TANK SYSTEMS REPORT US ECOLOGY NEVADA

March 2010

Revised October 2011

SECTION 10

TANK SYSTEMS REPORT

TABLE OF CONTENTS

10.1.0 Stabilization Tanks	1
10.1.1 Process Description	1
10.1.2 Tank Installation Certification	2
10.1.3 Diagram of Piping, Instrumentation and Process Flow	2
10.1.4 Description of Secondary Containment Structure	2
10.1.5 Description of Practices to Prevent Spills and Overflows	3
10.2.0 PCB Storage & Treatment	3
10.2.1 Tanks Description	3
10.2.2 Tank System Integrity Assessment	3
10.2.3 Description of Feed Systems and Safety Cut-Off Systems	4
10.2.4 Diagram of Piping, Instrumentation and Process Flow	4
10.2.5 Containment and Detection of Releases	4
10.2.6 Description of Practices to Prevent Spill and Overflows	4
10.3.0 Evaporation Tank	5
10.3.1 Evaporation Pad Description	5
10.3.2 Tank Integrity Assessment	5
10.3.3 Description of Feed and Cut-Off Systems	5
10.3.4 Diagram of Piping and Process Flow	5
10.3.5 Description of Secondary Containment Structure	5
10.3.6 Description of Practices to Prevent Spills and Overflows	6
10.4.0 LTTD Tanks – Removed from Service	
10.5.0 Leachate Storage Tank	6
10.5.1 Storage Tank Description	6
10.5.2 Tank System Integrity Assessment and Installation Certification	on 6
10.5.3 Description of Feed and Safety Cut-Off System	6
10.5.4 Diagram of Piping, Instrumentation, and Process Flow	6
10.5.5 Containment and Detection of Releases	6
10.5.6 Description of Practices to Prevent Spills and Overflows	6
10.6.0 Subpart AA, BB, and CC Standards	7
10.6.1 Subpart AA	7
10.6.2 Subpart BB	7
10.6.3 Subpart CC	7
	Tank Systems Report Version 2 10/14/11

10.7.0	Managing Incompatible, Ignitable or Reactive Wastes	7
	10.7.1 Precautions for the Management of Incompatible Materials.	8
	10.7.2 Precautions for Management of Ignitable or Reactive Wastes	8
10.8.0	Response to Leaks or Spills and Disposition of Unfit Tanks	8
10.9.0	Inspection of Tanks and compliance with 40 CFR §264.195	9
10.10.0	Closure of Tanks	10
10.11.0	One Year Storage	10

APPENDICES

Evaporation Pad Design Drawing
Evaporation Pad Volume Calculations
Evaporation Pad Construction Quality / Assurance and Integrity Assessment
Reports
Removed
Batch Stabilization Units Integrity Assessment Report
PCB Tanks Ultrasound Leak Test Results
PCB Processing System P & I D
PCB Tank Farm Liner System
PCB Tank Farm Secondary Containment Calculations
Leachate Storage Tank Diagram and Picture
Leachate Storage Tank Integrity Assessment
Tank Systems Location Diagram
Container Management Building

MANAGEMENT OF HAZARDOUS WASTES IN TANKS

US Ecology – Beatty, Nevada (USEN) manages hazardous waste¹ in tanks in five different scenarios:

- Waste Stabilization / Treatment Units
- Polychlorinated Biphenyl (PCB) Tank Farm
- Evaporation Pad & Associated Tank
- Leachate Collection Tank(s)

	Table 1 – Summary of Tank Management Units			
Tank	Common Name			Capacity
IGHK	Common Name	Status	Permit Required	[gallons]
#1	Stabilization Tank (Pan 1)	Existing	Yes	6,400
#2	Stabilization Tank (Pan 2)	Existing	Yes	35,500
#3	Stabilization Tank (Pan 3)	Existing	Yes	35,500
#4	PCB Storage & Treatment Tank	Existing	Yes	7,500
#5	PCB Storage & Treatment Tank	Existing	Yes	7,500
#6	PCB Storage & Treatment Tank	Existing	Yes	5,000
#7	PCB Storage & Treatment Tank	Existing	Yes	5,000
#8	PCB Storage & Treatment Tank	Existing	Yes	3,000
#9	PCB Storage & Treatment Tank	Future	Yes	12,500
#10	PCB Storage & Treatment Tank	Future	Yes	12,500
#11	Evaporation Tank	Existing	Yes	10,000
#15	Leachate Storage Tank	Existing	Yes	10,000
#18	Stabilization Tank (Pan 4)	Existing	Yes	17,250
#19	Stabilization Tank (Pan 5)	Existing	Yes	17,250

10.1.0 STABILIZATION TANKS

10.1.1 Process Description

USEN operates five stabilization tanks to solidify wastes containing free liquids, transfer wastes between containers, and to treat hazardous waste debris to comply with LDR standards or alternative treatment methods.

Stabilization Tanks 1-3 are capable of processing 75 tons/hour of waste and Tanks 4 and 5 are capable of processing 50 tons/hour. An excavator, backhoe, rotary mixing head, front-end loader, and/or other equipment may be used as mixing tools. Potential air emissions are minimized with the use of water sprays and/or fog systems.

10.1.1.1 Debris Treatment

Hazardous debris is treated by microencapsulation and macroencapsulation as discussed in the Section 11 Landfill Report and the Section 8 Waste Analysis Plan. Microencapsulation may be completed within stabilization tanks.

Here-in-after "waste" or "wastes."

10.1.1.2 Waste Stabilization Activities

Five (5) existing tanks stabilize wastes by mixing waste and stabilization reagents. A design drawing for the stabilization vessels is provided in the integrity assessment included in Appendix E.

Reagent selection is typically determined from the stabilization recipe developed in the laboratory, scaled up to the net weight of the load. In those cases where recipes are not predetermined, ² the treated waste is tested to ensure the appropriate treatment standard or method is achieved.

Once the operator determines the waste and reagents have been adequately mixed, the stabilized material is typically taken to the active cell for disposal, containerized and placed in the Dry Hazardous Waste Storage Area, or, as an alternative, staged in a segregated portion of the active landfill while being analyzed, but before being disposed.

Conformational testing is conducted on treated waste to verify compliance with applicable LDR treatment standards. As described in the WAP, samples are collected from treated waste streams to confirm the waste meets applicable LDR standards. Absence of free liquids is also confirmed on each treated waste stream using a visual inspection and/or the Paint Filter Liquids Test (PFLT), if the presence of free liquids is in question.

10.1.2 Tank Installation Certification

Appendix E contains integrity assessments certified by an independent professional engineer, registered in the State of Nevada, on the structural integrity of the stabilization tank systems and their suitability to manage the hazardous wastes intended. USEN also inspected the stabilization tanks prior to placing them in service to ensure proper installation.

10.1.3 Diagram of Piping, Instrumentation and Process Flow

Operation of the batch stabilization vessels does not require piping or instrumentation as these are batchoperated units.

10.1.4 Description of Secondary Containment Structure

The waste stabilization units are double-walled steel tanks. Two (2) of the tanks (Stabilization Tanks #2 & #3) are adjacent to each other, another tank (Stabilization Tank #1) is located in a near-by, but separate location. Two stabilization tanks 4 and 5 (Tanks 18 and 19) are located inside the Container Management Building. The primary tank holds the waste materials and the external secondary tank serves as a secondary containment system. Each secondary tank slopes to a collection sump. In addition, a steel pan covered with 12" of sacrificial soil is provided around the outdoor units. This secondary containment

As can be the case for commonly treated materials such as lead contaminated wastes.

device drains into the stabilization tanks and is surrounded by a concrete curb to prevent run-on and run-off. A tertiary, high-density, polyethylene (HDPE) liner is located under Stabilization Tank #1 and serves as further protection. Stabilization pan 4 and 5, located inside the Container Management Building, are surrounded by a concrete floor system to contain wastes managed around the tanks.

10.1.5 Preventing Spills and Overflows

Trained facility personnel oversee loading, unloading and treatment activities to ensure operations minimize spillage of waste outside the treatment units or containment systems. The outdoor units are equipped with a steel secondary containment pan covered with sacrificial soil to contain spillage. Spillage is promptly removed and placed in the treatment tanks or otherwise managed in accordance with the WAP. Pans 4 and 5 are surrounded by a concrete floor system. Waste spilled in the area can be washed into the pan system for management.

The quantity of waste in the vessel is limited to minimize spillage during mixing. Spillage or residue is contained within the containment structure and returned to the mixing vessel or managed in accordance with the WAP.

10.2.0 PCB STORAGE & TREATMENT TANKS

The tank processing system consists of the PCB Building, where storage, handling, draining and flushing of transformers and capacitors take place, and four (4) carbon steel tanks located outside the building for the temporary storage of drained liquid PCBs, rinsate, and other organic wastes until transported off-site. These tanks are to be used for TSCA regulated PCB contaminated liquids only.

10.2.1 Tank Description

The PCB treatment & storage tanks have a combined capacity of 25,000 gallons, consisting of two (2) 7,500-gallon tanks (Tanks #4 & #5), and two (2) 5,000-gallon tanks (Tanks #6 & #7). A 3,000-gallon tank (Tank #8) is used to transfer liquids from the original containers to the storage tanks. The 5,000-gallon tanks are 8' in diameter and 14' in length with four (4) supports, while the 7,500-gallon tanks are 8' in diameter and 20' long with six (6) supports. All tanks are carbon steel, with a nominal 1/4" shell thickness.

No internal corrosion protection measures are necessary for the tanks, since carbon steel is not subject to corrosion by PCB oil, transformer flush fluid, or other organic wastes.

The PCB storage tanks (Tanks #4 - #7) are vented through a carbon filtration system. The filtration system consists of 2 carbon canisters in series and connects to the storage tanks vents. When PCB liquids are being transferred to the storage tanks the air/vapors are pulled through the filtration system to prevent PCBs from possibly entering the atmosphere. Pictures of the system are included in Appendix G.

10.2.2 Tanks System Integrity Assessment

In accordance with 40 CFR §264.191, tank integrity assessments are required on tank systems in existence as of July 14, 1986, if the system is not provided with secondary containment. Since this tank

system is an existing system with secondary containment, no integrity assessment is provided for this unit. Ultrasound testing of the tanks will be conducted annually as a precautionary measure and reported in the Annual Report. These tests demonstrate that tank shell thickness exceeds the recommended minimum for horizontal carbon steel tanks. Results of the leak test, and an excerpt from UL 142 "Steel Aboveground Tanks for Flammable and Combustible Liquids" illustrating shell thickness requirements, are included in Appendix F.

10.2.3 Description of Feed Systems and Safety Cut-Off Systems

An automatic or emergency cut-off system is not required since the pumping of PCB liquid and other organic wastes is conducted as a batch operation rather than as continuous flow. The storage tanks are provided with overfill control equipment consisting of high-level alarms audible inside the PCB Building, which alert the operator when the tank level is approaching maximum capacity. Tank T-8, vacuum tank is not equipped with an alarm because PCBs are not stored in this tank. It is simply used as a transfer tank.

10.2.4 Diagram of Piping, Instrumentation, and Process Flow

Appendix G contains a diagram illustrating the piping; instrumentation and process flow for this system, and design drawings for each tank.

10.2.5 Containment and Detection of Releases

The storage tanks are located within a bermed containment area, elevated to allow leak detection during daily inspections. The containment area is underlain by an external liner system consisting of two (2) 30-mil liners protected by a polyester 125-mil filter fabric and 1-3" of sand. Drawings are included in Appendix H illustrate the configuration of the liner system.

Appendix I includes calculations demonstrating the ability of the system to contain twice the volume of the largest tank capacity (7,500 gallons), in addition to precipitation resulting from a 100-year, 24-hour storm event.

The liner system provides protection from vertical and lateral migration of waste as it surrounds the tank farm and covers all surrounding soil likely to be in contact with the waste in the event of a release. The 1-3" layer of sand covering the liner system serves as a containment media for a potential release. Because of the viscous nature of the PCB oils, the migration of any potential release from the storage tanks would be a slow process, allowing pumping of a great portion before seepage through the containment media occurs. Any spillage or contaminated portion of the containment media will be removed within 24 hours, or as soon as practicable, and the containment layer restored to its original thickness with clean sand.

10.2.6 Description of Practices to Prevent Spills and Overflows

Trained facility personnel oversee loading, unloading and treatment activities to minimize spillage of waste outside the treatment units or containment systems. Spillage is promptly removed and managed in accordance with the WAP.

10.3.0 EVAPORATION TANK

An Evaporation Tank (Tank #11) manages aqueous wastes (e.g.; wash water generated from vehicle decontamination, laboratory wastewaters, collected liquids from containment systems, and off-site generated wastes, etc.). The tank is 10,000 gallons and is provided with a pump and piping system that recirculates the water to break the liquid's surface tension and accelerate the evaporation process.

10.3.1 Evaporation Pad Description

The evaporation pad was constructed as a monolithic reinforced concrete unit, designed to resist cracking. The unit's bottom and walls are coated with a waterproofing coating.

Appendix A contains the design drawings for the evaporation pad. Volume calculations illustrating the net capacity of the tank are included as Appendix B. The unit's net volume accounts for the containment required for a 100-year, 24-hour storm event, and maintenance of a 6" freeboard at all times.

10.3.2 Tank Integrity Assessment

Appendix C contains a written assessment certified by an independent, qualified, professional engineer, on the structural integrity of the unit and its suitability to handle the hazardous wastes placed in the unit and the certification report on the quality assurance observed during unit installation.

10.3.3 Description of Feed and Cut-Off Systems

The evaporation tank is not equipped with any feed and cut-off systems. The unit receives wastes from several sources which are placed in the unit on a batch process.

10.3.4 Diagram of Piping and Process Flow

As described above, no piping or instrumentation is associated with the unit's waste feed mechanisms.

10.3.5 Description of Secondary Containment Structure

The evaporation tank is equipped with a liner and leak detection system consisting of a 4-millimeter-thick vapor barrier, followed by open graded sand underlain by a 40-millimeter, high-density polyethylene (HDPE) flexible membrane. The HDPE membrane covers the full height of the tank walls (up to the freeboard), and is sealed at the edges to prevent rainfall from entering the system.

The design of the evaporation pad secondary containment system satisfies the 40 CFR §264.193(d)(3) description of a doubled-walled tank, where the HDPE flexible membrane functions as the outer shell capable of containing any release from the inner tank. The system is equipped with an 8" steel pipe riser, which is inspected daily to allow detection of a release within 24 hours, or at the earliest practicable time.

10.3.6 Description of Practices to Prevent Spills and Overflows

Trained facility personnel oversee loading, unloading and treatment activities to minimize spillage of waste outside the treatment units or containment systems. Spillage is promptly removed and managed in accordance with the WAP.

Daily inspection of the pad ensures that a minimum 6" freeboard is maintained in the tank to prevent overtopping due to wind action

10.5.0 LEACHATE STORAGE TANK

10.5.1 Storage Tank Description

The leachate storage tank is a ten thousand (10,000) gallon fiberglass reinforced tank. The tank is currently managed as a <90-day storage unit. Collected leachate is stored in the tank pending treatment and/or disposal.

10.5.2 Tank System Integrity Assessment and Installation Certification

An integrity assessment report, reviewed and certified by an independent professional engineer registered in the State of Nevada is included as Appendix K.

10.5.3 Description of Feed and Safety Cut-off System

An automatic or emergency cut-off system is not required since the pumping of liquid is conducted as a batch operation rather than as continuous flow. The leachate level in the storage tank is visually inspected daily to ensure the tank is not nearing maximum capacity. The employee performing the inspection will compare leachate levels in the tank with a painted red line that indicates the high level mark. When the leachate level reaches the indicator mark no more liquid can be added to the tank.

10.5.4 Diagram of Piping, Instrumentation, and Process Flow

The tank integrity assessment and installation certification report included in Appendix K includes a diagram illustrating the piping; instrumentation and process flow for this tank system.

10.5.5 Containment and Detection of Releases

The storage tank is contained within a fiberglass reinforced secondary containment vessel. Daily inspections will detect any release from the tank to the secondary containment vessel. Any spillage is removed within 24 hours (or as soon as practicable).

10.5.6 Description of Practices to Prevent Spills and Overflows

Trained facility personnel oversee loading, unloading and treatment activities to minimize spillage of waste outside the treatment units or containment systems. Any spillage is promptly removed and managed in accordance with the WAP.

This is a manually operated tank not requiring any high level alarm.

10.6.0 SUBPART AA, BB AND CC STANDARDS

10.6.1 Subpart AA

The requirements of 40 CFR Part 264, Subpart AA are not applicable to the tanks discussed.

10.6.2 Subpart BB

The requirements of 40 CFR Part 264, Subpart BB are not applicable to the tanks discussed with the exception of Tanks T-4 through T-8 (PCB storage tanks). To comply with Subpart BB each piece of equipment has been identified and tagged with a unique number. Appendix G contains detailed schematics of this system. Per 40 CFR §264.1063 USEN will perform monthly Method 21 inspections using a portable Photo Ionization Detector (PID) to verify no equipment leaks. Any leaks detected will be fixed immediately and documented.

10.6.3 Subpart CC

The requirements of 40 CFR Part 264, Subpart CC are not applicable to the tanks discussed. The Subpart CC Air Emission Standards for the five stabilizations tanks (T-1, T-2, T-3, T-18, and T-19) will not apply because USEN will not accept for treatment hazardous waste with volatile organic compounds (VOC) concentrations greater than 500 ppm. All generator profiles are reviewed by USEN technical staff to ensure VOCs are below these limits. The five PCB storage tanks (T-4 through T-8) will not be subject to the Subpart CC regulations because concentrations of VOCs will not be greater than 500 ppm.

10.7.0 MANAGING INCOMPATIBLE, IGNITABLE OR REACTIVE WASTES

In accordance with the requirements of 40 CFR §264.17, USEN has developed a program to ensure that necessary precautions are taken to prevent the accidental commingling or reaction of incompatible and/or reactive wastes, or ignition of ignitable materials. The program encompasses the following elements:

- Identification of the hazardous characteristics of the waste streams during the approval process as described in the WAP;
- Segregation of reactive or incompatible materials according to USEN's segregation and classification system;
- Identification of the potential for incompatible reactions through the waste stream verification
 program described in the WAP. Verification testing of incoming shipments includes water
 reactivity tests and compatibility checks on waste streams intended for bulking or combined
 treatment. When the potential for inadvertent reactions is anticipated, precautions are taken as
 appropriate; and
- Identification of sources of ignition and necessary precautions.

10.7.1 Precautions for the Management of Incompatible Materials

Conducting compatibility testing between any loads intended for simultaneous treatment prevents inadvertent reactions in the batch stabilization units. No waste will be added to the treatment unit until all potentially incompatible waste or residues have been removed to the maximum extent possible.

Where the potential for incompatibility exists, USEN documents in the operating record the precautions observed to prevent violent reactions and/or generation of extreme heat, toxic mists, fumes or gases. Such documentation may consist of waste analysis results, results of compatibility tests, or the results from management of similar wastes under similar operating conditions.

10.7.2 Precautions for Management of Ignitable or Reactive Wastes

Ignitable or reactive wastes will only be placed in the tank system such that the waste is treated, rendered, or mixed before or immediately after placement in the tank so that:

- the resulting waste, mixture, or dissolved material no longer meets the definition of ignitable or reactive waste under 40 CFR §§261.21 or 261.23, and
- the waste is separated and protected from sources of ignition or reaction including but not limited to: open flames, smoking, cutting and welding, hot surfaces, frictional heat, sparks (static, electrical, or mechanical), spontaneous ignition (e.g., from heat-producing chemical reactions), and radiant heat. While ignitable or reactive waste is being handled, smoking and open flames will be confined to specially designated locations. "No Smoking" signs are conspicuously placed wherever there is a hazard from ignitable or reactive waste; or
- the waste is stored or treated in such a way that it is protected from any material or conditions that may cause the waste to ignite or react.

10.8.0 RESPONSE TO LEAKS OR SPILLS AND DISPOSITION OF UNFIT TANKS

The tank system or secondary containment system from which there has been a leak or spill, or that becomes unfit for use, will be removed from service. USEN will stop the flow of hazardous waste into the system and inspect it to determine the cause of the release. All material will be removed from the tank and associated secondary containment within 24 hours of becoming aware of the situation, or at the earliest practicable time, if removal is not possible within 24 hours. Since all hazardous waste tanks at the facility are provided with secondary containment, no release to the environment is anticipated. However, in the unlikely event of such a release, USEN will visually assess the extent of the release, and based on that assessment, determine the measures necessary to prevent further migration of the leak or spill to soils or surface water. Any visible contamination will be promptly removed and properly managed.

Notification of a reportable release will be provided to the NvDEP Administrator within 24 hours of detection. No notification will be provided if the release involves a waste quantity of one (1) pound or less, and it is immediately contained and cleaned up. Within 30 days of detection of the release to the environment, USEN will submit to the Administrator a written report containing the following information:

- Likely route of migration of the waste;
- Characteristics of the surrounding soil (soil composition, geology, hydrogeology, climate, etc.);
- Results of any monitoring or sampling conducted in connection with the release (if available);
- Proximity to down-gradient drinking water, surface water, and populated areas; and
- Descriptions of response actions taken or planned.

If the cause of the release was a spill that did not damage the containment system's integrity, the system will be returned to service once the released waste is removed and all necessary repairs are made. If major repairs of the tank system are required (e.g., installation of an internal liner, repair of a ruptured⁴ primary or secondary containment structure), a certification by an independent, qualified, registered, professional engineer will be obtained indicating that the repaired system is capable of handling hazardous waste without a release for the rest of the unit's service life. This certification will be obtained prior to returning the system to service, and will be submitted to the NDEP Administrator within seven (7) days of returning the system to use.

If the system cannot be repaired, the tank system will be closed according to procedures described in the approved Closure Plan.

10.9.0 INSPECTION OF TANKS AND COMPLIANCE WITH 40 CFR §264.194 AND §264.195

Treatment and storage tanks are inspected in accordance with the Section 5 Inspection Plan. All tanks will be inspected at least once per operating day with any deficiencies reported directly to the Facility Manage or designee. The following (if applicable) will be inspected:

- Overfill/spill control equipment to ensure it is in good working order.
- Above ground portions of the tank system to detect corrosion or releases of waste
- The construction materials and the area immediately surrounding the externally accessible porting of the tank system, including secondary containment.
- The level of waste in the tank to ensure adequate freeboard
- On a bi-monthly basis, the cathodic protection on Tanks 1, 2, and 3 will be inspected

All daily tank inspections will be turned into the Compliance Department and maintained as part of the facility operating record.

Ruptures do not include breaks in welds or in the tank shell due to normal wear & tear. Most tank repair events at USEN are due to excavator wear on the steel surface of the tank & are not "ruptures" as that term is used in 40 CFR §264.196 nor are the repairs typically "major tank repairs."

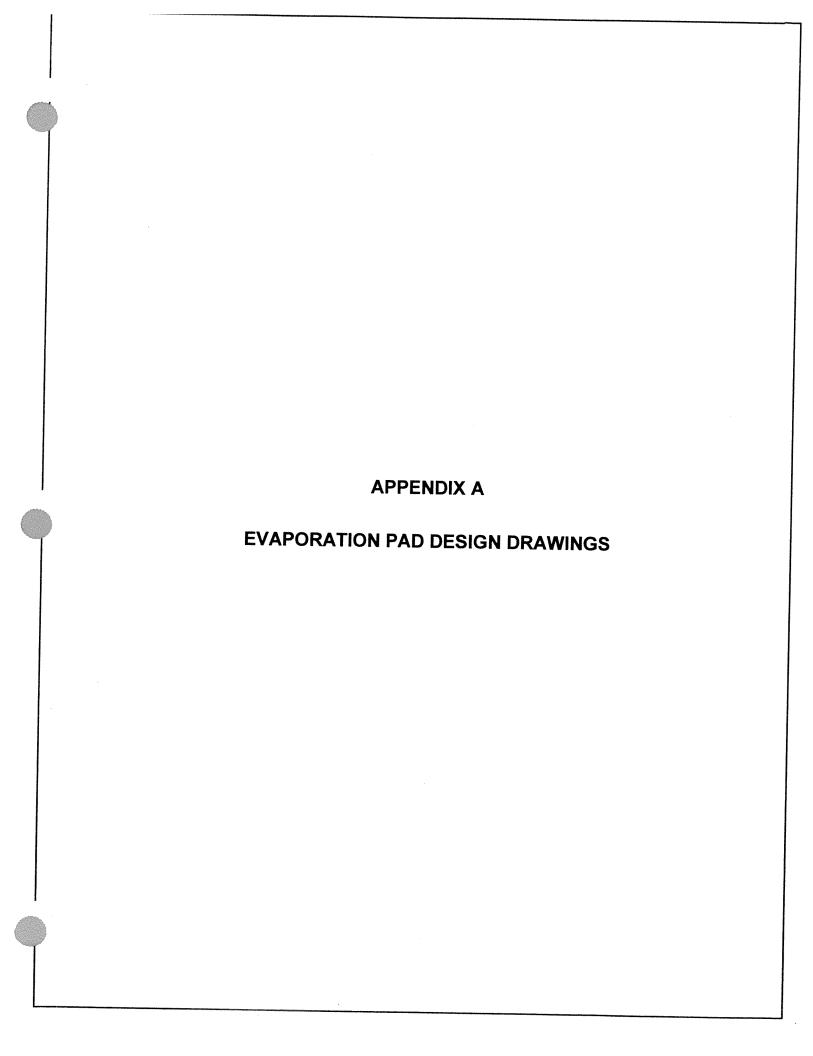
10.10.0 CLOSURE OF TANKS⁵

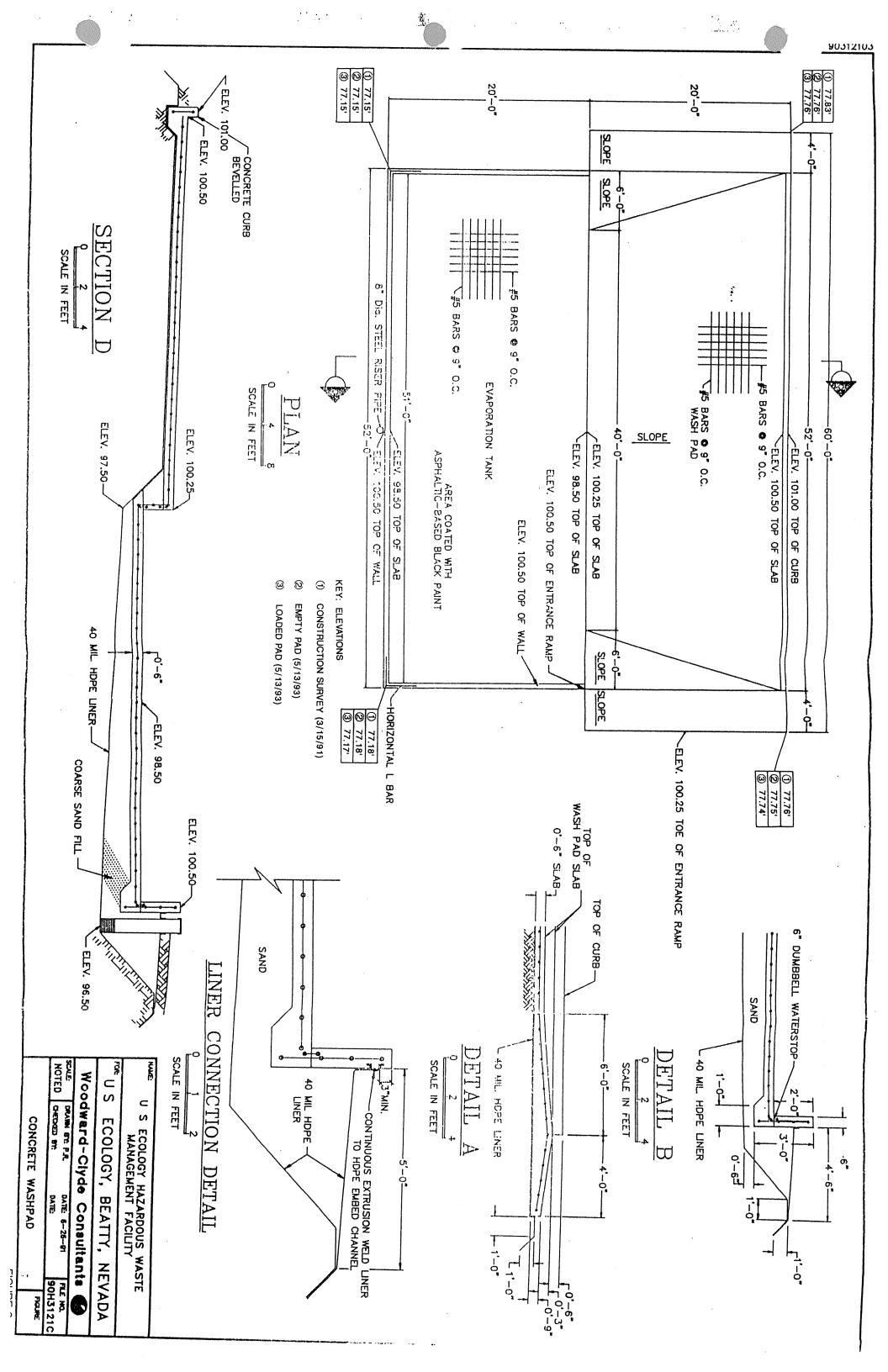
At closure, all hazardous waste and hazardous waste residue will be removed from the tanks or tank systems described in this section, treated and / or disposed of in the landfill, or sent to an off-site facility for treatment and / or disposal. All tank systems, including tank vessels, piping, ancillary equipment and contaminant structures will either be removed and properly managed (e.g.; disposed of in the on-site landfill), or decontaminated in accordance with procedures described in the Closure Plan.

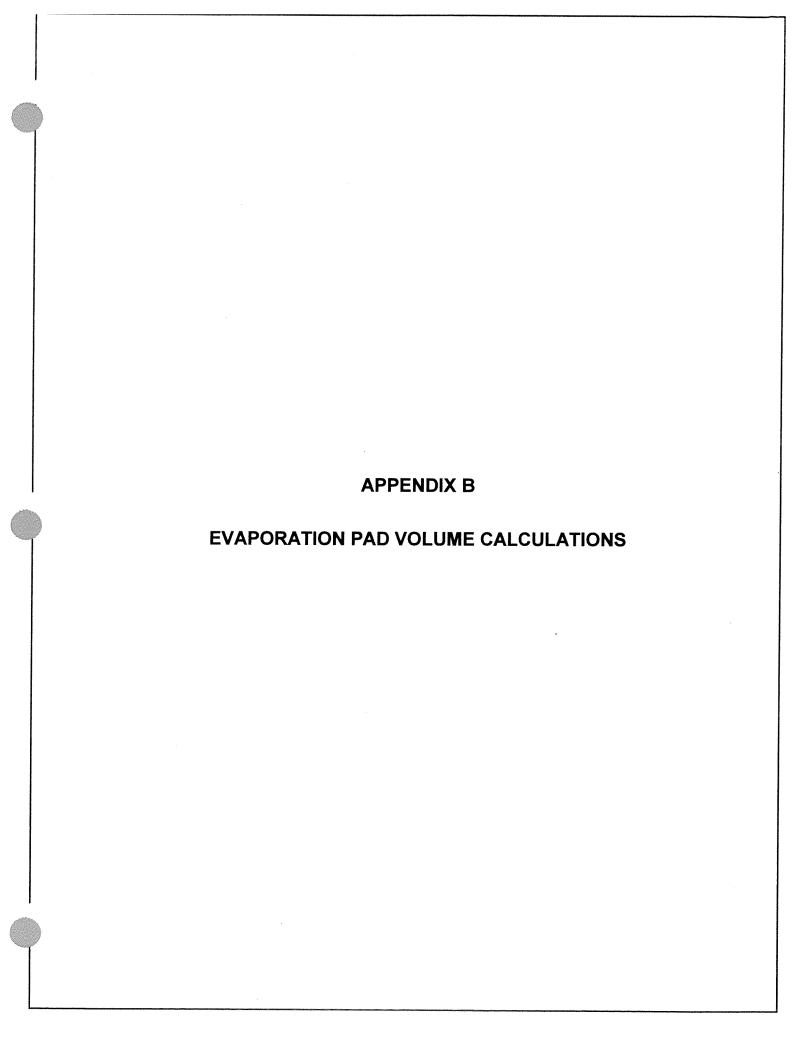
10.11.0 ONE YEAR STORAGE

Waste placed in a tank is not to exceed 1 year from the date of receipt. At a minimum frequency of once per month USEN will perform an inventory of waste being stored in tanks. Reports generated by AESOP (or NEWTON once released) will be utilized to ensure all received wastes are disposed of within 1 year of receipt.

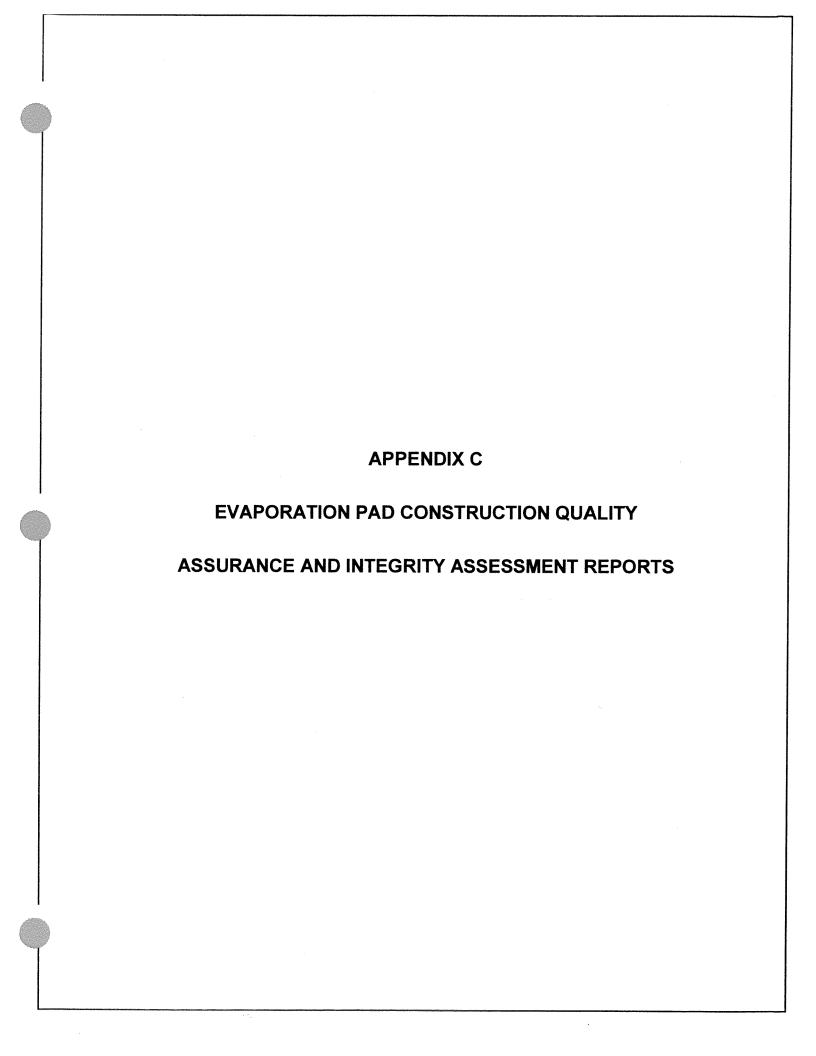
The Closure Plan governs any discrepancy between the general description of closure activities and this section since it is the authoritative document on closure issues.







American Ecology	SHEET NO OF
	CALC. NO. NV148 - 040
	DATE 6/27/95
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SUBJECT EIRPORATION PAD YOUME	CHECKED BY
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25 yr., 24 M. STORM = 2.0 In (.	the Widen U.S. VII VII-NEVADA
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APPENDIX C EVAPORATION PAD CONSTRUCTION QUALITY ASSURANCE AND INTEGRITY ASSESSMENT REPORTS

4735 1

June 14, 1991

U S Ecology, Inc. 9200 Shelbyville Road, Suite 300 P.O. Box 7246 Louisville, Kentucky 40257-0246

Attention:

Mr. Howard Althouse

Project Engineer

Subject:

Construction Quality Assurance Services For: Reinforced Concrete Washpad U S Ecology's

Hazardous Waste Management Facility

Beatty, Nevada

WCC File: 90H3121C

Dear Mr. Althouse:

This report summarizes the quality assurance monitoring services provided by Woodward-Clyde Consultants for the construction of a reinforced concrete washpad at the U S Ecology's Hazardous Waste Management Facility near Beatty, Nevada.

The report summarizes the monitoring activities and includes the conclusion of these activities.

Should you have any questions or if we can be of further service, please do not hesitate to contact us.

Sincerely,

Don. L. Colbourne Project Manager

DLC:llm

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Consulting Engineers, Geologists
and Environmental Scientists

Offices in Other Principal Cities

woodward. Ciyde Consultants

TABLE OF CONTENTS

2-1

Section	on	•	Page
1.0	INTRODU	JCTION	1-1
	1.2 DE 1.3 SCO 1.4 PR 1.5 CH 1.6 CO 1.7 CO	NERAL SCRIPTION OF PROJECT OPE OF WORK OJECT TEAM ORGANIZATION RONOLOGY OF CONSTRUCTION NSTRUCTION QUALITY ASSURANCE NSTRUCTION MEETINGS ELD IMPROVEMENTS/ADJUSTMENTS	1-1 1-2 1-3 1-4 1-5 1-6
2.0	CONCLU	SION	2-1
APP APP APP APP	ENDIX A ENDIX B ENDIX C ENDIX D ENDIX E	PRECONSTRUCTION MEETING IMPROVEMENTS/ADJUSTMENTS WOODWARD-CLYDE CONSULTANTS' REPORTS C1 - DAILY REPORTS C2 - SUMMARY OF SITE ACTIVITIES CONCRETE TESTING GEOMEMBRANE INSTALLATION E1 - CONTRACTOR'S DOCUMENTATION - DAILY REPORTS - SUBGRADE ACCEPTANCE - HDPE WELDING ROD QC REPORT E2 - WOODWARD-CLYDE CONSULTANTS' SITE DOCUMENTATION - PANEL PLACEMENT LOG - TRIAL SEAM LOG - SEAMING LOG RECORD DRAWING	•
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Woodward-Clyde Consultants

coarse sandfill leak detection layer on top of the HDPE liner under the area defined as the evaporation tank; and the construction of the reinforced concrete structure. Following the completion of the concrete structure the HDPE liner was carried up and mechanically fastened to the top of the outside perimeter of the concrete structure.

1.3 SCOPE OF WORK

WCC was retained by US Ecology to implement the CQA program for the construction of the washpad. WCC's services included the observation and documentation of construction activities including the preparation of the subbase, placement of the HDPE liner, coarse sandfill and reinforced concrete. WCC observed the field testing of the concrete by ETEC Testing Laboratory, Inc. (ETEC) of Las Vegas, Nevada. The off-site concrete testing was carried out by ETEC. WCC observed the HDPE liner Contractor's testing of the HDPE liner site seams. WCC reviewed the Contractors' quality control test results and provided on-site records management and system control.

The services provided by WCC were performed in accordance with our contract and the documentation provided by US Ecology, which included the following:

- Bid documents which included:
 - Request for Proposal letter dated November 13, 1990
 - Specification No. 167-C-001, Pages 1-13, For Structural Concrete US Ecology, November 16, 1990, Revision 0
 - Specification No. 140-C-001, Pages 1-79, US Ecology, October 23, 1990, Revision 5 (for HDPE liner reference)
 - Plan Sheet No. NV-105-CON-001, U.S. Ecology, November 3, 1991, Revision 1

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1.4 PROJECT TEAM ORGANIZATION

The project team consisted of the following firms and individuals:

	Entity/Individuals		Position
•	US Ecology, Inc. Louisville, Kentucky	-	Owner and Designer
	- H. Althouse, P.E. - D. Adrian		Project Engineer Project Manager
•	US Ecology, Inc. Beatty, Nevada		
	- R. Marchand - W. Marchand	•	Site Superintendent Construction Foreman
•	Woodward-Clyde Consultants Houston, Texas Oakland, California	-	Construction Quality Assurance
	Don L. ColbourneH. Richard Soennichsen, P.E.Scott DavisBill Snyder	٠.	Project Manager Project Certifying Engineer CQA Site Manager Senior Technician Soils/Geosynthetics
•	T & J Concrete Beatty, Nevada	-	Concrete Contractor
٠	- Tom Nickell	-	Superintendent
•	Poly-America, Inc. Dallas, Texas	•	Geomembrane Installation
	- M. Jett - C. Piper	•	Sales Manager Site Superintendent

Entity/Individuals

Position

- National Seal Company Palatine, Illinois
- Geomembrane Manufacturer
- ETEC Testing Laboratories Las Vegas, Nevada
- Concrete/Testing

1.5 CHRONOLOGY OF CONSTRUCTION

WCC's CQA manager arrived on site December 11, 1990. The preparation of the subbase was ready for the placement of the 40 mil HDPE liner December 12, 1990 and the construction activities were generally completed in the following sequence:

- December 17, 1990 placement of HDPE liner.
- December 21, 1990 placement of sand on top of HDPE liner as part of leak detection system. Placement of reinforcing steel and concrete form work in process.
- January 8, 1991 completion of concrete placement.
- January 18, 1991 hydrostatic testing of washpad and leak repairs;
 completion of attaching HDPE liner to outside perimeter of washpad.
- The surface of the concrete was coated while WCC's representative was not on site. The coating application was observed by WCC's representative upon return to the site. The evaporation tank area was coated with a two-component coating (Hi-Build Tneme Tar) manufactured by Tnemec Protective Coating of Kansas City, Missouri; the wash area was coated with a two-component coating (UI 7012) manufactured by Urethane Plastics, Inc. of Placentia, California.

1.6 CONSTRUCTION QUALITY ASSURANCE

The documentation provided by US Ecology for: a) Specification for Structural Concrete and b) Specification for Trench 11 provided the initial guidelines for the CQA procedures necessary to evaluate, with a reasonable degree of certainty, that the completed facility meets the design criteria through the contractors' conformance to the approved Design Drawings and Specifications. In addition a CQA Plan was submitted by WCC to US Ecology.

The CQA elements outlined in the Specifications and CQA Plan include: (1) defining the responsibility and authority of all organizations and key personnel involved, (2) presenting the qualifications of CQA personnel and construction Contractors, (3) summarizing the observation and testing activities to be used to monitor the construction and, (4) describing the documentation to be performed, collected and stored. Documentation summarizing the CQA monitoring activities are presented in the following appendices.

Appendix A: Preconstruction Meeting

Appendix B: Improvements/Adjustments

Appendix C: Woodward-Clyde Consultants' Reports

C1 - Daily Reports

C2 - Summary of Site Activities

Appendix D: Concrete Testing

Appendix E: Geomembrane Installation

E1 - Contractor's Documentation

- Daily Reports

- Subgrade Acceptance

- HDPE Welding Rod QC Report

E2 - Woodward-Clyde Consultants' Site Documentation

- Panel Placement Log

- Trial Seam Log

- Seaming Log

Appendix F: Record Drawing

1.7 CONSTRUCTION MEETINGS

A preconstruction meeting was held December 11, 1990 at US Ecology's, Beatty, Nevada site. The meeting was held to review the requirements for the construction of three projects which included the washpad. Minutes of the preconstruction meeting are presented in Appendix A. As a result of the limited construction activities formal daily/weekly meetings were not held, normal daily on-site discussions took place for review of progress and construction activities. Points discussed are noted in the CQA Site Manager's daily reports (Appendix C1). The progress of construction is outlined in the CQA Site Managers' weekly report (Appendix C2).

1.8 FIELD IMPROVEMENTS/ADJUSTMENTS

All design field improvements/adjustments were approved by US Ecology's Project Engineer. The improvements/adjustments are as follows:

- The mechanical connection of the HDPE liner to the outside perimeter of the washpad was replaced with Poly-America's product Poly-Lock, which is designed specifically for this task.
- A 6-inch waterstop was used in place of the minimum 4-inch waterstop specified. The latter product was not available.
- The 40 mil HDPE liner used was manufactured by the National Seal Company. This liner had been inventoried on site following the completion of an earlier project. Quality Control documentation for this liner was included in the Certification Report for the 1988 Trench 11 project. This documentation is not included in this report.
- The test results of the concrete indicated that the concrete strength did not meet the compressive strength of 4,000 psi required in the specification. The tests results indicated concrete strength of approximately 3,500 psi. Consideration was given to the specification requirements, set deliberately high to avoid unacceptably weak concrete, the use of rein-

Woodward-Clyde Consultant

forcing steel bars and the fact that washpads with concrete having similar compressive strengths as the new washpad had shown no structural weaknesses during use and no structural weaknesses were observed, by US Ecology, when the old washpad was demolished. As a result of these observations, the new washpad was approved. Documentation relating to the concrete laboratory testing is presented in Appendix D "Concrete Testing."

- The slopes of the concrete slab and ramps, in the equipment cleaning area, were adjusted to prevent low trailers and trucks from impacting the concrete as they entered and exited the area, as had been experienced with prior washpads.
- The concrete curb ends were beveled to avoid contact with (damaging) equipment tires.

Documentation outlining these improvements is presented in Appendix B "Improvements/Adjustments," and Appendix A "Preconstruction Meeting."

The services reported herein have been performed by WCC within the scope presented in the US Ecology's Quality Assurance requirements and in accordance with the current standards of practice and standard of care for the profession ordinarily exercised by other professions under similar circumstances.

Our conclusions are based upon observations performed at various locations and at specific times during the course of the work.

Test and sample locations were spaced in an attempt to obtain a representative measure of the in-place characteristics of each component of construction.

WCC's Quality Assurance monitoring of the construction of the washpad included visual observation of the work, observing collection of samples, laboratory testing of concrete and observation of field testing. The concrete laboratory and field testing were performed by ETEC Testing Laboratory to compare results with the approved Design Drawings and Specifications. In our opinion, WCC's CQA monitoring, confirmation of record drawing configurations and the results of the performance testing, indicate that the washpad was constructed in substantial conformance with the intent of the Design Drawings, Specifications and Quality Assurance requirements for this project.

The Professional Engineer's certification below represents a declaration of his professional judgment. Also, it should be understood that WCC's observations and monitoring of the work of other parties on a project shall not relieve such other parties from their responsibility for performing their work in accordance with applicable plans, specifications and safety requirements.

Don L. Colbourne Project Manager H.R. Soennichsen, P.E. Project Certifying Engineer

APPENDIX A

PRECONSTRUCTION MEETING

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SOUTHWEST GEOTECHNICAL CONSULTANTS

3280 WEST HACIENDA, SUITE 201 LAS VEGAS, NEVADA 89118 TELEPHONE (702) 795-7515

JUNDATION INVESTIGATIONS EXPLORATORY DRILLING STEEL ERECTION INSPECTIONS

SOILS, ASPIIALT, CONCRE QUALITY CONTROL FOR CONSTRUCTION

Concrete Hix Design for:

Project No .:

Issue Date:

T and J Construction

RLV-2090

January 30, 1990

Concrete Mix Design:

T&JD2

4000 psi at 28 days - Type V. Cement - 6.5 sack/yd.3

W/C =

0.443

Slump:

4" Maximum

Aggregate:

Lathrop Wells Pit

Hix Proportion for 1 cubic yard:

•		Ratch Weight (1bs)	Absolute Volume (Ft.3)
W.C. Sand	427	1150	7.650
Coarse Aggregate (No. 67)	58 %	1780	10.565
Water (5.0 gal/sack)		27 1	4.327
Coment (6.5 sack)		611	3.108
Entrained Air: 5% Haximum			1.350
		3812	27,000

Admixture:

Airin X - 4.0 fl.oz./100 lbs. cement

Master Builders Pozzolith 322N - 5.0 fl.oz./100 lbs. cement

Note:

For water in sand in excess of 5.0%, make weight corrections: for each 1.0% excess of water, deduct 12 lbs. (1.5 gallons)

mixing water and add 12 lbs. sand.

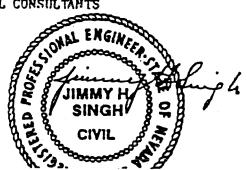
Theoretical Unit Weight = 141.2 lbs./cu.ft.

Information utilized for Mix Design Computations:

	Fine Aggregate	Coarse Aggregate
F.M.	2.89	-
S.G.	2.41	2.70
Absorption	2.51	2.27

Respectfully submitted,

SOUTHWEST GEOTECHNICAL CONSULTANTS



Recined 12-11-90 Goldon W.C.C.

FIELD/LABORATORY DATA - COMPRESSIVE STRENGTH TEST

	•
Client: US ECOLOGY	Job No.:
Address:	
Project: US ECOLOGY BEATTY	
Location in Structure: WASH PAD YAHK FLOOR	
Source of Sample: IVEST FUN OF TANK FLOOR	
Contractor: T&J	Ticket No:
Arch/Engineer:	Measured Slump. in.: 3
Material Supplier: T&J	Measured Air Content: 4.2*
Batch Size/CY: 10 CYS	Concrete Temp., °F: 53°
Mix Identification:	Ambient Air Temp, °F:
Design Strength PSI: 4000 / 28 Days	Plastic Unit Weight, pcf:
Nominal Size Aggregate: 3/4	No. of Cylinders Molded: 4
Time Sampled: 1145	Specimen Size: 6X7
ield Curing Conditions: CURE BOX	Area, sq.in.: 28,27
Sampled By: Sion 1402ME Date: 1.3.9	Time in Mixer: Hr M
Submitted By: SONTHORNE Date:	Water Added on Job: 4 Ga
Authorized By:Date:	Test Procedure: ASTM C39-
REMARKS: CONCRETE PLACED BY CHUTE	

	Specimen			Compressive Strength . Maximum Load		Type Fracture	Defects in Specimens/	Tested
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4150 W. Pioneer Ave., Suite A • Las Vegas, NV 89102 (702) 367-0100

LABORATORY REPORT COMPRESSIVE STRENGTH OF CYLINDRICAL CONCRETE SPECIMENS

CLIENT: Woodward - Clyde Consultants

7330 Westview Drive Houston, Texas 77055 JOB NO.: 12037- 1

DATE OF REPORT: 01-11-91

roject:	US ECOLOGY	- Beatty, Ne	evada (WC	C #90H3121C)		
ocation in Structure:	: Wash Pad T	ank Floor				
ource of Sample:	West End o	f Tank Floor				
ontractor:	T & J		Ticket	No:	NA	
rch/Engineer:	NA -		Measure	d Slump:	· 3	in
Material Supplier:	T & J		Measure	d Air Conten	t: 4.2%	
atch Size/CY:			Concret	e Temp:	53	
lix Identification:	6.0 Sacks		Ambient	Air Temp:	50	
esign Strength PSI:	4000	/ 28 Days	Plastic	Unit Weight	, pcf:	
Iominal Size Aggregate	≘: 3/4		No. of	Cylinders Mo	lded:	4
Sampled By: S.T	horne/ETEC	Date 101-03-	91 Time in	Mixer: N/	A Hr.	NA
Submitted By: S.T		Date 101-08-	91 Water A	dded on Job:	4	
uthorized By: S.D	avis/WCC		Test Pr x 12": Area	ocedure: = 28.27 sq. in.	ASTM unless oth	C39-8
REMARKS: Concrete pla		•				

Specimen	Date	Specimen	Compressive Strength Maximum Load		Type Fracture	Defects Specimens	Tes
-Marking If Any	Tested	Age In Days	Pounds Force	psi	if Other Than Cone	Caps If Any	
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18	01-31-91	· 28				j	
10	01-31-91	28					
10	01-31-91	HOLD					

CC: (1/M) Client; Don Colbourne

REVIEWED BY: A Sahi P



4150 W. Pioneer Ave., Suite A • Las Vegas, NV 89102 (702) 367-0100

LABORATORY REPORT COMPRESSIVE STRENGTH OF CYLINDRICAL CONCRETE SPECIMENS

CLIENT: Woodward - Clyde Consultants

7330 Westview Drive Houston, Texas 77055 JOB NO.: 12037- 1

DATE OF REPORT: 01-11-91

01-17-91

Project:	US ECOLOGY - Beatty, Ne	vada (WCC #90H3121C)	
Location in Structure:	Wash Pad Tank Floor		•
Source of Sample:	West End of Tank Floor		
Contractor:	T&J	Ticket No:	NA
Arch/Engineer:	NA	Measured Slump:	3 i
Material Supplier:	T & J	Measured Air Content:	4.2%
Batch Size/CY:	10	Concrete Temp:	53
Mix Identification:	6.0 Sacks	Ambient Air Temp:	50
Design Strength PSI:	4000 / 28 Days	Plastic Unit Weight, p	ocf:
Nominal Size Aggregate		No. of Cylinders Molde	ed: 4
Sampled By: S.Th	norne/ETEC Date 101-03-9	1 Time in Mixer: NA	Hr. NA
Submitted By: S.TI	norne/ETEC Date 101-08-9	1 Water Added on Job:	4
Authorized By: S.Da	vis/WCC Date:	Test Procedure: :12": Area = 28.27 sq. in. un	ASTM C39- less otherwise

REMARKS: Concrete placed by chute and vibrated into place

Specimen Date		Specimen	Compressive Maximum		Type Fracture	Defects Specimens Caps	Te
Marking If Any	Tested	Age In Days	Pounds Force	psi	i if Other Than Cone	If Any	
1A	01-10-91	7	64764	2290			
18	01-17-91	14	77134	2730		,	
1C	01-31-91	28					
10	01-31-91	28				:	

CC: (1/M) Client; Don Colbourne

REVIEWED BY: Kilwant & Sania

4150 W. Pioneer Ave., Suite A • Las Vegas, NV 89102 (702) 367-0100

LABORATORY REPORT COMPRESSIVE STRENGTH OF CYLINDRICAL CONCRETE SPECIMENS

CLIENT: Woodward - Clyde Consultants

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7330 Westview Drive Houston, Texas 77055 JOB NO.: 12037- 1

DATE OF REPORT: 01-11-91 01-17-91 02-04-91

Project:	US ECOLOGY	 Beatty, Nev 	ada (WCC #90H3121C)		
Location in Structure:	Wash Pad Ta	nk Floor		•	
Source of Sample:	West End of	Tank Floor			
Contractor:	Т&Ј .		Ticket No:	NA	
Arch/Engineer:			Measured Slump:	3	<u> </u>
Material Supplier:	T&J		Measured Air Content:_	4.2%	
Batch Size/CY:			Concrete Temp:	53	
Mix Identification:			Ambient Air Temp:	50	
Design Strength PSI:	4000	/ 28 Days	Plastic Unit Weight, p	cf: <u> </u>	
Nominal Size Aggregate	: 3/4		No. of Cylinders Molde	d:	4
			Time in Mixer: NA		
Submitted By: S.Th	orne/ETEC	Date <u>101-08-9</u> 1	Water Added on Job:	4	
Authorized By: S.Da	vie/WCC	Date:	Test Procedure: 12": Area = 28.27 sq. in. un	ASTM	C39-
REMARKS: Concrete place	ed by chute	and vibrated	into place		

Specimen	Date	Specimen	Compressive Maximum		Type Fracture	Defects Specimens Caps	Te
Marking If Any	Tested	Age In Days	Age In Pounds psi Days Force		if Other Than Cone	If Any	
1A	01-10-91	7	64764	2290			
1B	01-17-91	14	77134	2730		j	
1C	01-31-91	28	97420	3450			
1D	01-31-91	28	96316	3410			

CC: (1/M) Client; Don Colbourne

WILLIAMON ENGINEEDING CONCRETE AND MATERIAL CONSULANTS:

	1	•	F	IELD/LABORA	TORY DATA - COMPRESSIV	E STRENGTH T	ESTS .	
		Client: <u>U.S</u>	. ECOLOG	1		Job No.:_	12037-2	
	-	Address:						
	i	/roject: <u>U.</u>	ECOLO	GY BEAT	17			
	-	Location in S	Structure:_	WASH PA	0			
	ĺ	Source of Sam	mple: CEN	TER OF W	VASH PAD			
	ļ	Contractor:	T&J			Ticket No:_		
		Arch/Engineer	•			Measured S1	ump. in.: <u>4</u>	*
	į	Material Supp	olier: To	ZZ		Measured Ai	r Content: 4	.3%
	Ĺ	Batch Size/CY	r: 8 CY	<u>S</u>		Concrete Te	mp., °F: <u>5</u>	_0
	ļ.,	Mix Identific	ation:		Ambient Air Temp, °F: 52°			
	Ì	Design Streng	th PSI: 4	000	/28 Days	Plastic Uni	t Weight, pcf	:
	!	Nominal Size	Aggregate:	3/4		No. of Cyli	nders Molded:	4
		Time Sampled:				Specimen Si	ze: 6XIZ	
	1.	Field Curing	Conditions	: CUPE E	POX	Area, sq.in	.: <u>28.27</u>	
		ampled By:	Sion 140	2HE	Date: 1 · 8 · 91	Time in Mix	er: <u> </u>	Mi
		Submitted By:	SconTH	OPNE	Date:•	Water Added	on Job: 5	Gal
		Authorized By	/ :		Date:	Test Proced	ure: AS	TM C39-8
	i	REMARKS: CON	CRETED I	PLKED RY	CHUTE AND VIL	PATED IN	TO PLACE	
		•						
	i	•						
÷ :	: = -			T			<u> </u>	
. ż.	# 4 1	Specimen Marking	Date Tested	Specimen Age In	Compressive Strength Maximum Load	Type Fracture if Other	Defects in Specimens/ Caps	Tested By

	Specimen	_Date	Specimen	Compressive Strength Maximum Load		Type Fracture	Defects in Specimens/ Caps If Any	Tested By
	Marking Tested If Any	Age In Days	Pounds Force	psi	if Other Than Cone			
	25	1.15	7					
Ī	7B	2.2	78					
	26	2.5	Z8				·	
· [2D	2.5	HOLD					
	-						1-8-9/	



4150 W. Pioneer Ave., Suite A • Las Vegas, NV 89102 (702) 367-0100

LABORATORY REPORT COMPRESSIVE STRENGTH OF CYLINDRICAL CONCRETE SPECIMENS

CLIENT: Woodward - Clyde Consultants

7330 Westview Drive Houston, Texas 77055 JOB NO.: 12037- 2 DATE OF REPORT: 01-16-91

Project: US ECOLOGY - Beatty, Nevada (WCC #90H3121C) Location in Structure: Wash Pad Center of Wash Pad Source of Sample: Contractor: T & J Ticket No: NA Arch/Engineer: 4 NA Measured Slump: Material Supplier: T&J 4.3% Measured Air Content: 8 55 Batch Size/CY: Concrete Temp: NA Mix Identification: 52 Ambient Air Temp: Design Strength PSI: 4000 / 28 Days Plastic Unit Weight, pcf: ---Nominal Size Aggregate: 3/4 No. of Cylinders Molded: Sampled By: S.Thorne/ETEC Date: 01-08-91Time in Mixer: NA Hr. NA Submitted By: S.Thorne/ETEC Date: 01-10-91Water Added on Job: Authorized By: S.Davis/WCC Date: --- Test Procedure: NOTE: Cylinders are 6"x 12"; Area = 28.27 sq. in. unless otherwise REMARKS: Concrete placed by chute and vibrated into place

Specimen	Date	Specimen	Compressive Maximum		Type Fracture	Defects Specimens	Tes
Marking If Any	Tested	Age In Days	Pounds Force	psi	if Other Than Cone	Caps If Any	E
2A	01-15-91	7	70796	2500			
2B	02-05-91	28			••	j	
20	02-05-91	28					
20	02-05-91	HOLD					
							l

CC: (1/M) Client; Don Colbourne

REVIEWED BY: Kulwart S. Sahi, P



4150 W. Pioneer Ave., Suite A • Las Vegas, NV 89102 (702) 367-0100

LABORATORY REPORT COMPRESSIVE STRENGTH OF CYLINDRICAL CONCRETE SPECIMENS

CLIENT: Woodward - Clyde Consultants

7330 Westview Drive Houston, Texas 77055 JOB NO.: 12037- 2

DATE OF REPORT: 01-16-91 02-06-91

Project:	US ECOLOGY	' – Beatty, Ne	vada (WCC #90H3121C)		
Location in Structure	: Wash Pad				Mile Mile and a second
Source of Sample:	Center of	Wash Pad			
Contractor:	T&J		Ticket No:	NA	
Arch/Engineer:	NA NA		Measured Slump:		inc
Material Supplier:	T&J		Measured Air Content:	4.3%	
Batch Size/CY:	8		Concrete Temp:	55	
Mix Identification:	NA		Ambient Air Temp:	52	
Design Strength PSI:_	4000	/ 28 Days	Plastic Unit Weight, p	ocf:	
Nominal Size Aggregate	e: <u>3/4</u>		No. of Cylinders Molde	ed: 4	
Sampled By: S.T	horne/ETEC	Date: <u>01-08-</u> 9	91Time in Mixer: N	A Hr. NA	
Submitted By: S.T	horne/ETEC	Date: <u>01-10-</u> 9	Mater Added on Job:	5	(
Authorized By: S.D			Test Procedure:		
REMARKS: Concrete pl	•	Cylinders are 6"x e and vibrated	12": Area = 28.27 sq. in. un i into place	less otherwi	se i

Specimen Date -Marking Tested If Any		Specimen	Compressive Maximum		Type Defects Fracture Specimens		Test B:
		Age In Days	Pounds Force	psi	if Other Caps Than Cone If Any		
2A	01-15-91	7	70796	2500	•		С
28	02-05-91	28	95515	3380	•	j	F
20	02-05-91	28	95769	3390			F
2D	03-05-91	56					

CC: (1/M) Client; Don Colbourne



4150 W. Pioneer Ave., Suite A . Las Vegas, NV 89102 (702) 367-0100

LABORATORY REPORT COMPRESSIVE STRENGTH OF CYLINDRICAL CONCRETE SPECIMENS

CLIENT: Woodward - Clyde Consultants

7330 Westview Drive Houston, Texas 77055 JOB NO.: 12037- 2

DATE OF REPORT: 01-16-91 02-06-91 03-06-91

Project:	US ECOLOGY -	Beatty, Nev	rada (WCC	#90H3121C)		
Location in Structure:						
Source of Sample:	Center of Wa	sh Pad			•	
Contractor:	T&J		Ticket No	:	NA	
Arch/Engineer:	NA			Slump:	4	in
Material Supplier:	T&J		Measured	Air Content:	4.3%	
Batch Size/CY:	8		Concrete	Temp:	55	
Mix Identification:	NA			ir Temp:		
Design Strength PSI:	4000 /			nit Weight, pc		
Nominal Size Aggregate:				linders Molded		·
Sampled By: S.Tho	orne/ETEC D			ixer: NA		-
Submitted By: S.Tho			•	ed on Job:		-
Authorized By: S.Dav	ris/WCC D	ate:	Test Proce	edure:	ASTM C3	9-8
REMARKS: Concrete plac	NOTE: Cyli ed by chute a			28.27 sq. in. unle	ss otherw	ise i

Specimen Marking			Compressive Strength Maximum Load		Type Fracture	Defects Specimens	Test
If Any	Tested.	Age In Days	Pounds Force	psi	if Other Than Cone	Caps . If Any	B)
2A	01-15-91	7	70796	2500	æ		0
28	02-05-91	28	95515	3380	•		R
2C	02-05-91	28	95769	3390		,	R
20	03-05-91	.56	101840	3600			R

CC: (1/M) Client; Don Colbourne

(::

SOILS INVESTIGATION AND FOUNDATION ENGINEERING; CONCRETE AND MATERIAL CONSULTANTS; TEE. TEETING EEDINGES, TOOLIBI ESHOCTING CONSULTANTS: NON-DESTRUCTIVE STEEL AND WELDING CERTIFICATIO

E1 - CONTRACTOR'S DOCUMENTATION

#DAILY REPORTS.

SUBGRADE ACCEPTANCE

HDPE WELDING ROD OC REPORT

POLY-FLEX, INC.

construction management services

project no.	date //18/91
project name	115 Ecology weather Marc
project location	BEATTY NEV contract days remaining
contractor's equipment	
contractor's personnel	
observations	West to week @ 7:00 AM. Finished REPAIRS AND TESTING
	Finished Depails AND TESTING TRuch loss of faboic ARDINED Washed on wash pad Laid to panels of faboic 450' lang 32,400 59 ft
· ·	Jara / To Dare Fabric - 3 40,600 59 Liner - 219, 200 59
	photo meeting change order problem sheet conversation
time anived	7:00 time 5:00 Signature

1/19/200

POLY.FLEX, INC.

daily field report construction management services

	date ///2/9/
project no.	date
project name	U.S. Ecology contract days remaining
project location	US Ecology weather Mean Y Linny contract days remaining
contractor's equipment	
contractor's personnel	
observations	West is a 7:00 1 M
	West is 0 7:00 d M. Wester the chieran on The wash per Total to Date Fabric 305, 200 Linea-219, 200
	photo meeting change order problem sheet conversation
tim anive	7:00 time 5:00 figures

JEKU11

POLY-FLEX, INC.

daily field report construction management services

		/-5-71
project no	G-1075	date <u>-/2/3/90</u>
project name	1/5 F12/05V	weather //ordy
project name	BEATTY NEV	contract days remaining
location		
equipment	PO 20200 20 000 000 000 000 000 000 000 0	
and the state		
personnel	***************************************	è .
•		
observations	- Inder APPI	VED this morning
	- They STAPTED	DOURING WAS DADA
	- lule Trimmio	back ELPOSED INTE ON CAP.
	- Sine Tricks	home @ 2:00p because
		A DEA PEADU FOR US
	- T 1000 - TO	Las Vages To pick up Alfonse
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	CNA 194371A	

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	to not to the court of the cour	
	\$	
		nonhem sheet conversation
	photo meeting	change order problem sheet conversation
ý m	7:00 Am	2:00 pm
arrive	. و الماريخ	-

POLY-FLEX, INC. daily field report construction management services

project no.		date 12/14/90
project name	U.S. Ecology	weather //c//
project location	BEATTY NEVADA	contract days remaining
contractor's equipment		
contractor's personnel		
observations	MADE SURE = // E	Suigment was in work
	VAC TESTED DE PA	RS ON WASh PBD.
	P+++++	
		,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,
-		< <u>\</u>
	photo meeting dang	pe order problem sheet conversation
tim anive	ne 700 time 5'00 departed	11 Police
		•

A STATE OF THE STA

778

POLY-FLEX, INC.

daily field report construction management services

	date 12/13/90	
project no.	date /2/13/90	*****
project name	U.S. Ecology weather //eae Contract days remaining	•••••
project location	CEASTY NEVADA contract days remaining	*****
contractor's equipment		
contractor's personnel		*****
observations	West to work at 7:00 A.M. Unknown Touch less of 50 mil gad Welding Rod Has "PEW hau! bass out of TRENTH!! for Cap Repaired Seams on wash gas Filled Sand bass for REST of The day Wireken when	
	photo meeting change order problem sheet conversal	bor
tim anive	departed departed departed	Ammente 1 mmente 1 mmente 1 mmente 2 mment

POLY-FLEX, INC.

daily field report construction management services

	10/10/00
project no.	date 12 12 90
project name	Uin James and or of Journal of the state of
project location	Beairy Nevaga contract days remaining
contractor's equipment	
contractor's personnel	
	- WENT IN AT TEA AM -BACKALE APRILED FROM HEATE
	- 11 hans wift TRATIED and CUGANIZED
	- Dit to take and 40 mil on wash DAR
	slimational was U.S. Ecologis
	- Wings Welden and A. e. TESTED Ill good
	- Upliance Truck lass of 50 mil 5hest
	10 ml- 2400 Sq JASTALID IN WISH PAD
	1410c 24:0 59
-	***************************************
·	
	M 100 100 100 100 100 100 100 100 100 10
	photo meeting change order problem sheet conversation
tin arriv	7:00 A.M. time 5:00 P.M. signature

POLY-FLEX, INC. geomembrane air/vacuum test record

		projec	t name U.	5. Ecolog	7
project no.	1-12/1/1/210	and	•		/
project location	BESITY NEVADA model				
vacuum box no.	make	Illoder			
air testing			_	a a a Mari	data
seam interval tested	tester's name	time	psi	pass/fail	date
WASh Pap 1/2	1 J Bose	3:30	30 psi .	455	12/12/9
Wash Pac 2/3					
Wash PAD 3/4				******************	*****************
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	***************************************				*****************
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va-v-0 12 12 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2		*********************		**********************	*************
	tester's name	test failure location	test failure no.	repair date	retest approval
Mark Pen 1/2	Danny Polis	NONE	NANE	12/13/50	
Liash Pan 2/3	//	. *		,,,	
	>		54 20200 00020 00020 00 00 00		
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	50 000 FR 2000FR 00 200 CR 00 000 000 000 000 000 000 000	*****************		**************	
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inspected b	v 1. J. Piper	·· ·· · · · · · · · · · · · · · · · ·	d	ate	1/90

PF-006-5-90

12-15-90

Attachme

POLY-FLEX, INC.

certificate of acceptance of soil subgrade

• •	U.S.E. n.ksy		
project no.			•••••
location	Prairy Neyara PJ. Pape		
installation contractor representative	1. J. PIPIE	:	
area to	Wash Pap		
be accepted			······
·	I, the undersigned, duly authorized represent subgrade surface conditions and shall be res in accordance with the specifications. I do no character of the subsurface soil, or any effect	ponsible for maintaining in accept any responsibility	for the conditions or
	11 figur	Superatudas	12/12/90
	aignature	úde	· date

POLY-AMERICA Inc.

2000 W. Marshall Drive

Grand Prairie. Texas 75051

800-527-3322

214-647-4374

Telex 79-2851

FAX 214-988-833:

January 4, 1991

Ms. Jeanette Lear U.S. Ecology, Inc. 9200 Shelbyville Rd. Suite 300 Louisville, KY 40222

Re: HDPE Welding Rod QC Report
US Ecology Trench 10 & 11 Construction
Beatty, NV

Dear Ms. Lear:

The following Welding rod rolls were shipped to Beatty, NV for the above referenced project.

5mm Rod Roll No.	5mm Rod Roll No.	4mm Rod Roll No.
284 285 286 287 291 292 293 295 296 302 307 308 312 313	317 318 328 329 331 332 336 337 338 339 388 389 414 424	218 382 385 431
J 1. J	767	

All 5mm rods were manufactured of Railcar RAIX 60671, Lot 431933 All 4mm rods were manufactured of Railcar CCBX 55230, Lot 431183 The resin QC and QA reports are attached.

Sincerely,

:==

George M. Hall Plant Manager

PATICAL RESIN REPORT

•					
P. O. # 4770		•		Weight / Resim .Cod	851000
Date Recaived 10-41-90			•	KE2T# 'POC	. = ===================================
BUY INFORMATION RELICES # RAIX 60671	### # # # # # # # # # # # # # # # # #	4.5.0	CHB	50.0 J .	
Vendor IC		<u> </u>	Cin	Slip Azzáblock	
Lot i	Density ,			Antioxida	
Type: IDPE HDPE	Comments	aco. Poly- 7	Her		EVA
Pressure: Eigh Low				01751	
•			•	•	
CAR CAPACTITI	·	nular	Can Pome	5050	
			Car lyps	7700	•
Measurements:	Z_ CA_	14 CB 11	3	12 I	CTAL
Actibet T	cr _	G	3	Ī	CTAL /5/
Release Information:	Daze	The L	441574		
Released to Production					+10
Released to 2111 road					
Comments					
LABORATORY TESTING REPORT	,12 -		i "ı	#	. R=
Resin Eveluation: Mal: index	: A .13 :	15 13	3	_ Å⊽8· _4	
- Deasity:	A . 947	म नित्र ८३ नि	नि ३ ंवेर	3 A78	947
Film Evaluation: Ganga: Ru		· -	281		
Edab:	·	Dart Impact: C-BlQ(k Content:	5 .10		
: CO?	50		2.4%		
IR Analysis: 'Slip	₹	_ =4		¥0	
$\frac{4}{C_{1}}$	17A	Other	(specify)		
Comence: Pal.,-Flex					
Film Das: Pala-flex		Approved By:	ON	10/11	
Film Ose:		,		707-7	
FUMPING INFORMATION			7		10°
Released for Papies:		·			
(हा	nate)	(Data)	د د ـــرو	Severect)	J
_		Time Started	Time Tim	72066	
	mpermen: A				

JAH- 4-91 FRI 10:17

	RAILCAR RESIN REPORT	
•	2.0. # 1914	Weight 18075 Resin Coce +
	Date Received 11-2-85	
<u> </u>	RUY INFORMATION	/m/
	Vendor UC Melt Index 0.13 Lot i Density .950	Slip Antiblock Antioxidant VA EVA
	Type: LDPE LLDPE Comments Rale Dest Other HOPE Pressure: High Low Slate	EA Other
	•	
	CAR CAPACTITY Pallets Granular Car Type	5250
	Measurements: inches: A 15 CA 32 CB 13 B	10 TOTAL
	weight: A CA CB B	
	Release Information: Date Time Initials	•
	Released to Production	-19
1	Released to Reilroad 11-9-89 4:30pm 100	
	Comments	
		•
_	LABORATORY TESTING REPORT A JUST Sure Sura A D. 20 CA 0.18 CA 0.21 15 0.1	19 R=
	Resin Evaluation: Male index: Wh 1947 CA 144 CB 1948 B. 95	AV8. 0-20
	Density: 2017 14/9 CA -450 CB -947 B-941	Avg. 0.797
	Film Evaluation: Gauge: Range Average	
•	Width: Dart Impact:	
•	COF C.8/K.Ask Content: A 2.2, CA	
:	IR Analysis: Slip VA EA	•
	AB EVA Other (specify)	
	Comments: Phy Flux MI Elichtly higher	normal
	Film Use: Poly-Flex Approved By: N	11/2
	PUMPING INFORMATION	
	Released for Pumping: SIL: FP //->- SI	(Approved)
	Time Started Time Fi	
		14 to 14
	Compartment A	

Compartment CA

FRODUCT OWALLTY REFORT

FAX NO. 214-647-4574 EXI. 233 - DR NO. 214-647-8061 POLY AMERICA INC. GRAND PRAIRE, TX 75051

UNION CARBIDE CORPORAT FOLYOLEFINS DIVISION F.O. BOX 186 FORT LAVACA. TEXAS 779

OCTOBER 24, 1989

PRODUCT NAME

. L

258D-1525 BK

SLEND NUMBERS 445668 431183
GUANTITY, LBS. 90,350 90.350
CONTAINER CODX55230 CODX55230
CUSTUMER ORDER NO. UBL

UCC DRDER NO. 440762 SHIPPING DATE 10/24

SHIPPED TO: GRAND PRAIRIE, TX

THE FOLLOWING TEST DATA WAS GREAT VED:

•	445668	431183
" INDEX	0.15	0.16
iY ASTM	0.9500	0.9495
inl : ime 200 c min	117.	110.
CARRON BLACK	2.4	2.3
•		

ANALYSIS NO. 1041020 601022

P.O. 1914

GUALITY CONTROL REPARTMENT SEADRIFT FLANT LABORATORY

PRODUCT QUALITY REPORT

431014

Lax No. 214-647-8061 x 208 POLY AMERICA INC. AND PRAIRE, TX 75051 TN: SHAWNEE DORADO

UNION CARBIDE CHEMICALS AND PLASTICS COMPANY INC. POLYOLEFINS DIVISION P.O. BOX 185 PORT LAVACA, TEXAS 77979

OCTOBER 9, 1990

PRODUCT NAME DEGD-1525 BK

A END NUMBERS 431933 431934 QUANTITY, LBS. 92,800 , 92,800 CONTAINER RAIX606717 RAIX60671

431033

G STOMER ORDER NO. 4770 . ' U.J ORDER NO. 447476 SHIPPING DATE 10/03

S : PPED TO: GRAND PRAIRIE, TX

THE FOLLOWING TEST DATA WAS OBTAINED: L

47777	427234
* * *	
0.15	0.11
16.	14.
0.9485	0.9490
2.2	2,4
113.	116.
741003	1761003
	0.15 16. 0.9485 2.2 113.

DEPARTMENT SEADRIST PLANT LABORATORY .

E2 - WOODWARD-CLYDE CONSULTANTS

DOCUMENTATION

PANEL PLACEMENT LOG

TRIAL SEAM LOG

SEAMING LOG

PROJECT NAME

Woodward-Clyde Consultants

PANEL PLACEMENT LOG

PROJECT NAME: BEAH INJ - USE, WASH PAD

PROJECT NO .: 9043121C

LOT # DATE REPAIRS AREA ROLL / PAHEL # TIME YES / HO REPAIRED TESTED L/W ± \$Q. FT. 870 60/14.5 NO \geq 60. 3 60 4 60 TOTAL 340. COMMENTS: FR. SHT. # ACCUM. TOTAL 348 THICKNESS SIGNATURE: SHL CHK'D BY:

PROJECT NAME: U.S. Ecology - Beathny. PAO

PROJECT NO .: GOH 3121C

3	SAMPLE TRIAL SEAM INFORMATION TEST RESULTS														
	4		TRI	AL SE	AM IN			-			TEST RESULTS ME PEEL SHEAR				
-	DATE	EQUIP	TECH	TIME			EMP IN	. F		TIME			SHE	AR .	اللا ال
k	1				AMS	SHEET	-				F/BRK	P/F	F/BRK	P/F	
. -	12-12	634F	エフ	P.4	47	52	300			PM	1100	P	105	7	40
F	12-13	24505	エノ	AM	52	55	420	450		AM		P	100	4	90
k	12-17	04 E	I7	AM	43	52	400	500		A.M	95	P	125	4	40
L	1.17.71	Z 330 <u>6</u>	エノ	P.4	55	دع	4,-5	500		Pun	1100	7	135/120	4	40
L	1-18-91	23305	<u>L</u> J	Any	47	52	450	مح		AM		2	125	ک	40
	2/-16	23306	エコ	Pay	55	62	450	ూం		PM		7	136	P	40
	1-19	2330 €	上上	Am	<u>4</u> 2	51	405	500		AM	95/100	7	125	7	40
	2/-19	2336 E	エン	PM	5E	65	4 25	500		PM	105/0	P	146/	P	40
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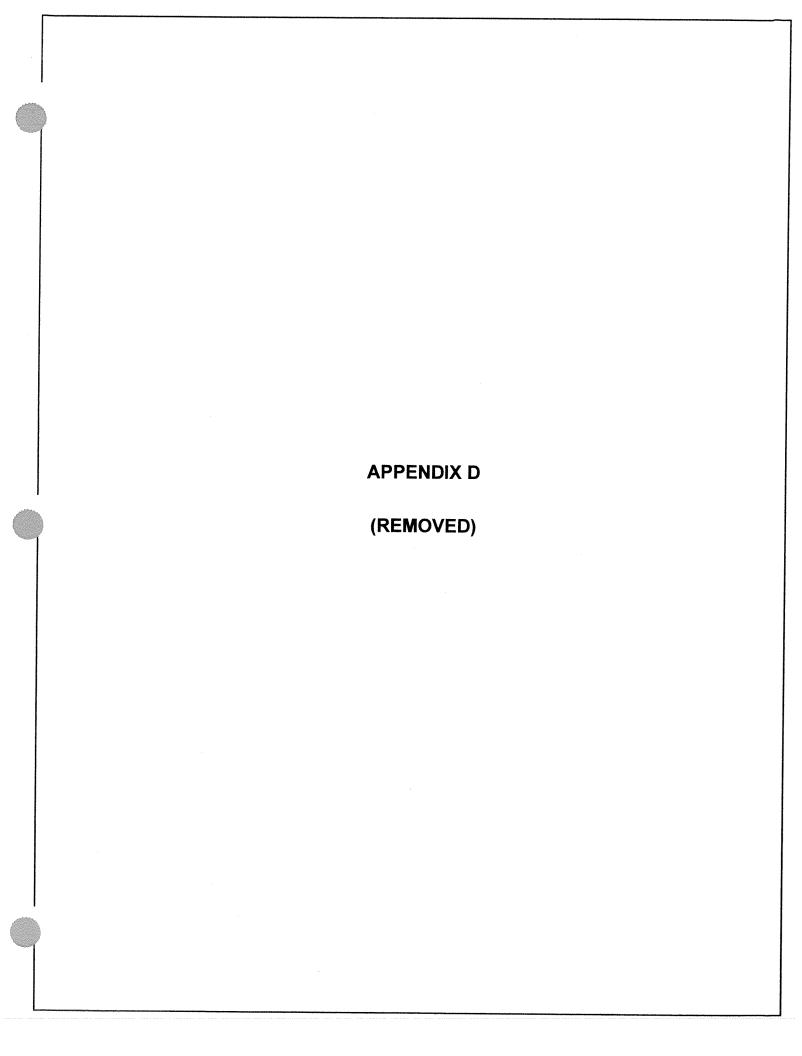
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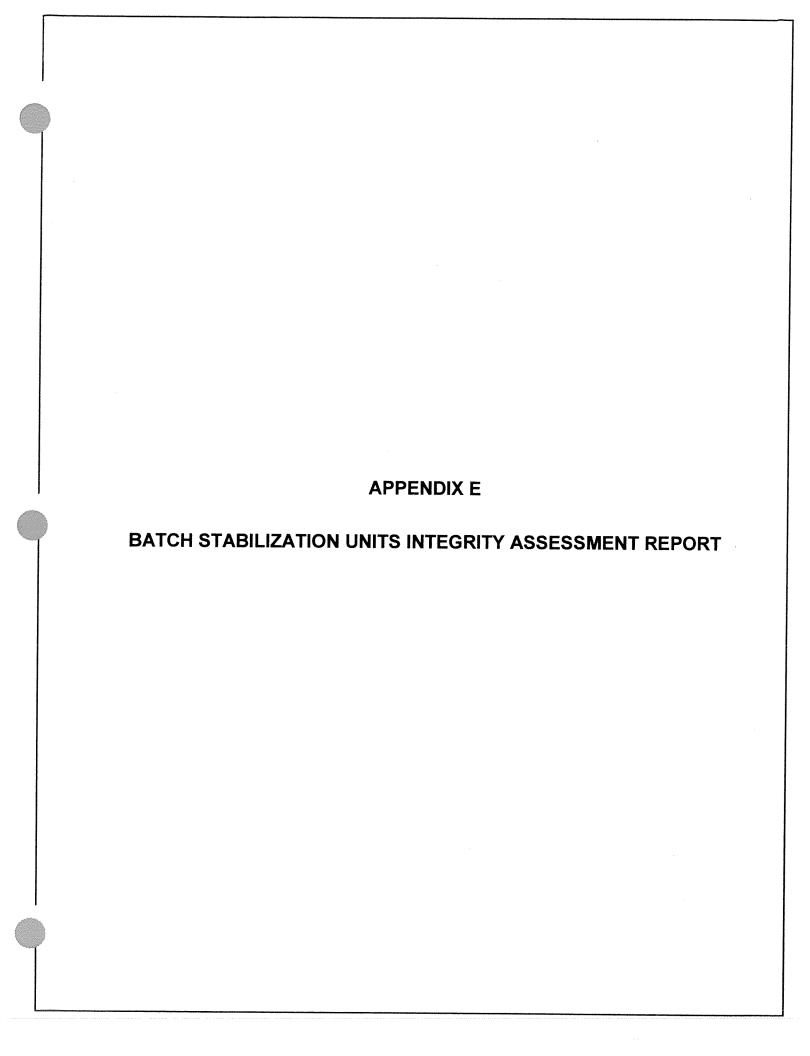
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UPGRADE OF EXISTING BATCH STABILIZATION UNIT

U.S. ECOLOGY, INC. BEATTY, NEVADA NDEP Permit HW0011 Revision 0

March 1998

GRANT A. OF JACKSON CIVIL No ho299

Prepared By

NAISMITH ENGINEERING, INC. ENGINEERING • ENVIRONMENTAL • SURVEYING CORPUS CHRISTI, TEXAS

NEI PROJECT NO: 4856

TABLE OF CONTENTS

1. GENERAL:		1
2. FACILITY DE	ESCRIPTION:	1
3. DESCRIPTIO	N OF BATCH STABILIZATION UNIT MODIFICATION	1
3.1. Reaso	n for Modification:	1
3.2. Modif	ication Procedure:	1
3.3. Person	nnel Making Modification:	2
3.4. Const	ruction Quality Assurance for the Modification:	2
3.5. CQA	Personnel:	2
4. REFERENCE	S	3
APPENDICES		
Appendix A Appendix B Appendix C	As-Built Drawings and Revised Calculations Construction Quality Assurance Documentation Certification Letter	

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1. GENERAL:

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Naismith Engineering, Inc., (NEI) was retained by U.S. Ecology, Inc., (USE) to perform the construction quality assurance (CQA) for the upgrade of the existing bulk stabilization unit (BSU), located at their Beatty, Nevada facility. Golder Construction Services, Inc. (GCS) was retained by NEI to perform third party certification for the BSU. Facility operations are governed by two (2) separate authorizations. The facility is authorized to manage hazardous wastes regulated by the Resource Conservation and Recovery Act (RCRA) under a permit (Permit No. NEV-HW0011) [Ref. 1] issued by the Nevada Department of Conservation and Natural Resources, Division of Environmental Protection (NDEP). The facility is also authorized to manage toxic substances regulated by the Toxic Substances Control Act (TSCA) under an approval issued by the U.S. Environmental Protection Agency, Region IX.

2. FACILITY DESCRIPTION:

The facility is located in Nye County, near Beatty, Nevada. It is authorized to treat, store and dispose of certain types of hazardous and toxic wastes. The bulk storage unit is designed for the mechanical solidification and/or stabilization of hazardous wastes and for debris treatment. The existing BSU was converted into secondary containment for the new primary containment unit. The converted secondary containment unit is approximately fifty (50) feet long and approximately thirteen (13) feet wide. The new primary containment unit is a welded steel tank fabricated from one (1) inch thick steel plates and standard structural steel members. The primary containment unit is approximately forty-nine (49) feet long and approximately twelve (12) feet wide. A sump is provided on the east end of the secondary containment unit. There are two (2) four (4) inch diameter steel pipes in the sump for liquid removal from the secondary containment unit. The bottom of the secondary containment unit was sloped to drain to the sumps. A (1/4) inch thick steel pan surrounds the BSU on the north and east sides to provide containment for loading/unloading and support activities. The steel pan is sloped to drain liquids to the sump in the northeast corner. Gravel and sand separated by a geotextile was placed above the containment pan and graded to prevent the runoff of liquids. The as-built drawings and revised calculations are in Appendix A.

3. DESCRIPTION OF BATCH STABILIZATION UNIT MODIFICATION

3.1. Reason for Modification:

The previous batch stabilization tank was modified as per requirements of Permit No. NEV-HW0011, Section V.B.3.a.

3.2. Modification Procedure:

The existing unit was initially cleaned out, walls straightened, and "touch-up" welding was performed. The unit was visually inspected after the welding was complete and then hydrostatically tested. The hydrostatic testing results of the secondary containment unit on January 21, 1998 are presented in Appendix B.

The north and south walls of the existing BSU were squared up with new (1/2) inch steel plating supported by (1/2) inch steel plating. The gap between the existing steel walls and the new (1/2) inch steel plating was filled with a cement mixture. Two (4) inch steel pipes were placed on the east side of the secondary containment unit for liquid removal.

The primary containment unit was prefabricated in sections and then constructed inside the modified secondary containment unit. Below the floor and on the east 9.3 feet of the 1 inch thick steel primary tank is 3" x 3" x 1/2" steel angles on 5 inch centers for reinforcement. The rest of the new 1 inch thick primary tank was reinforced with 3" x 3" x 1/2" steel angles on 8 inch centers. The unit was visually inspected and hydrostatically tested. The hydrostatic testing results of the primary containment unit on January 27, 1998 is in Appendix B.

3.3. Personnel Making Modification:

The modification to the Batch Stabilization Unit was completed by U.S. Ecology, Inc., site maintenance personnel.

3.4. Construction Quality Assurance for the Modification:

CQA personnel inspected and tested the modifications to the secondary containment system following fabrication. Inspections were made to ensure that the fabrication was performed properly. In addition, a hydrostatic test was performed on the completed installation of the primary and secondary system. An inspection report and the results of the hydrostatic test are included in Appendix B. All inspections and test indicated that the lining system was functioning properly and was acceptable. Ms. Laurie Sanders of the Nevada Division of Environmental Protection (NDEP) was on site January 26, 1998 to observe the construction of the modified batch stabilization unit.

A letter certifying the proper construction of the Batch Stabilization Unit has been included in Appendix C.

3.5. CQA Personnel:

On-site CQA activities and CQA oversight were provided by Mr. Richard E. Kiel, P.E. of Golder Construction Services. Mr. Kiel is a registered professional engineer in the state of Nevada and is experienced in CQA activities for hazardous waste management facilities.

4. REFERENCES

- 1. "Nevada Division of Environmental Protection Permit for Hazardous Waste Treatment, Storage and Disposal", Nevada Division of Environmental Protection, Carson City, Nevada, July, 1988.
- 2. "Part B Renewal for Hazardous Waste Management Facility U.S. Ecology, Inc., Beatty, Nevada", Volumes I through VI, U.S. Ecology, Inc., Houston, Texas, April, 1997, Revision 0.

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APPENDIX A

AS-BUILT DRAWINGS AND REVISED CALCULATIONS

REVISED CALCULATIONS

March 6, 1998

NAISMITH ENGINEERING, INC. CALCULATIONS - BATCH STABILIZATION UNIT REVISED DESIGN FOR DOUBLE WALLED STEEL

SHEET NO. 1 DATE: 2/23/98

OBJECTIVE: To determine, through established and structural steel design procedures, the required structural steel dimensions/member sizes of the several proposed batch stabilization unit (BSU) system components.

APPROACH:

- 1. Perform analysis and design according to established structural and foundation engineering standards, ACI 318-89.
- 2. Where applicable, static and dynamic loads have been combined to develop "worst case scenerio" loading conditions.

GIVEN:

- 1. The site is located in a seismic zone 3, according to the 1994 Uniform Building Code.
- 2. The proposed BSU as shown in the design drawings given in Appendix A of this report.

ASSUMPTIONS:

1. All structural steel will have a minimum yield strength, f_y, of 36,000 psi [A36 carbon steel].

CALCULATIONS:

Step 1. Structural steel mixing tank

The tank will rest inside a containment tank constructed with 1/2 inch steel plate which rests on grade.

A. Size Wall Stiffeners - The governing loading condition is created by earth pressure on the walls.

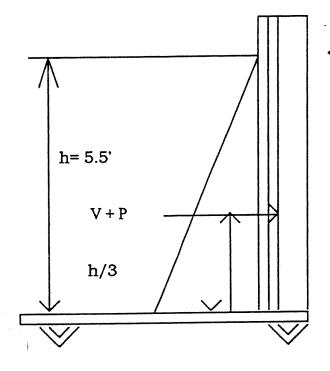
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NAISMITH ENGINEERING, INC. CALCULATIONS - BATCH STABILIZATION UNIT REVISED DESIGN FOR DOUBLE WALLED STEEL

SHEET NO. 2 DATE: 2/23/98



← L 3" x 3" x ½" @ 8" O.C.

(Assume $\emptyset = 45^{\circ}$ for Substrate) WALL DESIGN

P = FORCE DUE TO DEAD LOAD OF SUBSTRATE $P = \frac{1}{2} \gamma h^2 tan^2 (45 - \frac{1}{2}) = \frac{1}{2} (100 \text{ pcf}) 5.5 tan^2 (45 - \frac{45}{2}) = 259 \frac{1}{10} t_{ft}$

INFLUENCE FROM ZONE III SEISMIC (PER UBC 1994)

$$V = (ZIC) P = [(0.30)(1.25)(8.2)] 259 = 133 lb/ft < P$$

 $RW 6$

- Z = 0.30 (Table 16 I UBC 94)
- I = 1.25 (Table 16-K UBC 94)
 C = 1.25 S/T ^{2/3} = 1.25 (1.0)/(0.06) ^{2/3} = 8.2

Rw = 6 (Table 16-N UBC 1994)

MOMENT AT BASE

$$M_1 = (259 + 133)^{16} / {10} \frac{5.5}{3} = 719 \text{ lb.ft } (0.719 \text{ k.ft})$$

NAISMITH ENGINEERING, INC. CALCULATIONS - BATCH STABILIZATION UNIT REVISED DESIGN FOR DOUBLE WALLED STEEL

SHEET NO. 3 DATE: 2/23/98

 M_{allow} . = fb5x = (24ksi)(4.87 in³) 1/12 = 9.74 k.ft> M_1 ok

- $fb = 24 \text{ ksi (AISC } 9^{th})$
- $Sx = I/y = 18.9 \text{ in } ^4/(5.0 1.12) = 4.87 \text{ in}^3$

BASE (FLAT PLATE) DESIGN

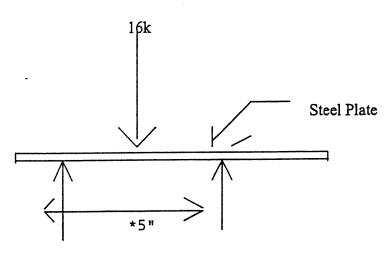
1" STEEL PLATE WITH A 1/16" LOSS ON INTERIOR (ONE SIDE) DUE TO CORROSION

• $Sx = 1/6 \text{ bh}^2 = 1/6(5\text{"})(15/16\text{"})^2 = 0.73 \text{ in}^3$

 $M_{\text{allow}} = (24 \text{ ksi})(.73 \text{ in}^3) 1/12 = 1.46 \text{ k.ft} > M_1 \text{ OK}$

MOMENT IN STEEL PLATE DUE TO HS20 TRUCK LOADING

HS 20 WHEEL LOAD = 16 klps



Continuity Factor
$$A = PL/4 = (16k)(5/12*0.80)/4 = 1.33k.ft < M_{allow} OK$$

*This analysis is extremely conservative since a typical tire will bear on at least three 3"x3"x1/2" steel angles.

NAISMITH ENGINEERING, INC. CALCULATIONS - STABILIZATION UNIT SECONDARY CONTAINMENT VOLUME

SHEET NO. 1 DATE: JANUARY 1998

OBJECTIVE:

To show that the containment volume within the confines of the secondary containment tank will meet the requirements from 40 CFR §264.193.

APPROACH:

Determine the required volume of containment according to 40 CFR §264.193, which requires that the secondary containment be able to contain one hundred percent (100%) of the capacity of the largest tank within its boundary, plus the precipitation resulting from a 25-year, 24-hour rainfall event.

ASSUMPTION:

The secondary containment will be sealed to prevent the collection of precipitation. Therefore, the secondary containment needs only to be sized to contain the volume of the primary tank.

CALCULATIONS:

Step 1 Calculate the maximum capacity of each steel mixing tank.

The maximum capacity of each tank, V_{tank} , is the sum of the volume above the flat bottomed area, V_{fb} , and the volume above the ramped area, V_r .

$$V_{tank} = V_{fb} + V_r = 29.3 \text{ ft } (12.1 \text{ ft})(1.8 \text{ft}) + .5(20 \text{ ft})(12.1 \text{ ft})(1.8 \text{ ft})$$

 $= 856 \, ft^3$

Step 2 Calculate the volume of the secondary containment unit. It is approximately 2-1/2" deeper and 7" wider than the primary containment unit.

$$V_{tank} = V_{fb} + V_r = (29.5 \text{ft})(12.7 \text{ft})(1.8 \text{ft}) + .5(20 \text{ft})(12.7 \text{ft})(1.8 \text{ft})$$

 $= 903 \, \text{ft}^3$

Therefore, the secondary containment is adequate for containing 100% of the primary containment unit. Since the sides of the units are at the same elevation, this intuitively checks.

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APPENDIX B

CONSTRUCTION QUALITY ASSURANCE DOCUMENTATION

NAISMITH ENGINEERING, INC. PROJECT INSPECTION REPORT

Owner: U.S. Ecology, Tric Reatly, NV (American Ecology) Owner's Project No.: NEI Project No.: 4856 Date: 1-21-98 Time: 0700 Page I of	Project rille. Upgrade of Ex	cisting	BSU				
Date: 1-21-98 Time: 0700 Page I of	Owner: U.S. Ecology, I	nc E	Beatly, NV (Amer	ican Ecology)			
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NAISMITH ÉNGINEERING, INC.

TEST REPORT-U.S. Ecology, Inc.

SHEET NO. 1 DATE: 02/23/1998

Batch Stabilization Secondary Containment Unit

Test Parameters

The Batch Stabilization Secondary Containment Unit is filled with water in a hydrostatic test. A plastic pan is also filled with water, to allow the test to account for water loss due to evaporation. Water level measurements are made in both units throughout the test period. Dimensions of the secondary containment unit are 49'-4" long, by 13'-7" wide, by approximately 5'-8" deep. The diameter of the plastic control pan is 11". All times are Pacific Standard Time. An initial mark was made on both units and all level measurements were made from this mark. This test was performed on January 21, 1998.

WATER LEVEL MEASUREMENTS OVER TIME							
Time	Pan Level (In.)	Wash Pad Level (In.)	Comments				
12:20	1.0	1.0	Initial				
12:35	1.0	1.0	No Loss				
12:50	1.0	1.0	st.				
1:20	1.0	1.0	и				
1:50	1.0	1.0	st				
2:50	1.0	1.0	st .				
	١						
	_						
			:				
			•				

Pan Calculations

Area:

 $(\pi/4) \times (11 \text{ in})^2 = 95.0 \text{ in}^2 \times (1 \text{ ft}^2/144 \text{ in}^2) = 0.65 \text{ ft}^2$

Volume lost:

 $0.0 \text{ in } \times 95.0 \text{ in}^2 = 0.0 \text{ in}^3 \times (1 \text{ ft}^3/1,728 \text{ in}^3) = 0.00 \text{ ft}^3$

Evaporation Rate: $0.00 \text{ ft}^3/0.65 \text{ ft}^2 = 0.00 \text{ ft}^3/\text{ft}^2$

Secondary Batch Stabilization Unit Calculations

Area: (filled to middle of ramp)

 $39.3 \text{ ft} \times 13.6 \text{ ft} = 534.5 \text{ ft}^2$

Actual Loss:

 $534.5 \text{ ft}^2 \times 0.0 \text{ in } \times (1 \text{ ft/}12 \text{ in}) = 0.0 \text{ ft}^3$

CONCLUSION: Since there was no recordable loss in the existing batch stabilization unit, the system did not leak and passed hydrostatic test

NAISMITH ENGINEERING, INC. PROJECT INSPECTION REPORT

Project Title: Upavade of Exist	ing BSU				
	Beatty, NV (American Ecology)				
Owner's Project No.:	NEÍ Project No.: 4856				
·					
Date: 1-26-98 Time:	0800 Page <u></u> of				
Contractor: N/A	Type of inspection: □ daily □ periodic				
Inspector(s): David ME Cormick (NEI	Persons contacted on-site:				
Rick Kiel, P.E.	Lori Taquehi - Tachnical Reviewer				
Weather: Law 50's, clear, calm	Testing in progress:				
Contractor: ☐ working ☐ delayed (weather ☐ delayed due toN/A	Inspection - Hydrostatic Test				
Work in progress: Preparation for hydrotest of the primary mixing tank.					
Work completed since last inspection: Medified existing tank, sealed pre Equipment/materials received on-site since	uious secondary system, constructed exterior par last inspection:				
N/A					
Summary: 0800 Arrived on site with Rick Kiel, P.E. 0830 Rick Kiel went through Health and Safety orientation. 0900 Performed inspection of BSU and exticy pan while US. Ecology was performing modifications. 04.15 Laurie Sanders DUCR) - End. Management Specialist II 1500 Departed site, US Ecology expects to complete BSU by late afternoon or early next modum (Attach additional sheets as required) Signature of inspector(s):					
	البو				
Distribution:					

REVISED 08-30-94

NAISMITH ENGINEERING, INC. PROJECT INSPECTION REPORT

Project litle: Upgrade of	Exis	ting BSU		
Owner: U.S. Ecology, I	nc, - E	Zeatty, NV (An	nevican Ecology)	
Owner: U.S. Ecology, I Owner's Project No.:	NEI Project No.: 48	356		
Date: 1-27-98	Time:	0800	Page <u></u> of <u>2</u>	
Contractor: N/A		Type of inspection: □	daily 🗆 periodic	
Inspector(s): David Mª Cormick (Persons contacted or	n-site:	
Rick Kel, P.E. (Lori Taquehi - Tech	nical Reviewer	
Weather: Low 50's, clear, call	2/	Testing in progress:		
Contractor: ロ working ロ delayed (v ロ delayed due to <u>ル/み</u>		Inspection - Hydros	static Test	
Work in progress:				
Preparation for hydrotes	+ of	the primary n	mixing tank.	
Work completed since last inspection				
Continue construction of Prin			pan	
Equipment/materials received on-site	e since la	st inspection:	;	
N/A				
Summary: 0800 Arrived on site with Rick kiel, R.E. (informed U.S. Ecology ran out of welding rod last night and drove to Las Vegas to purchase more). 2:30 pm Completed primary unit, began visual insp. and then performe the hydrotest. (Loss of 1/4"/15 min. in Secondary Sump). 3:30 pm Began pumping water out of primary tank in order to perform repairs on leaks. (Attach additional sheets as required) Signature of inspector(s):				
Distribution:	100			

E:\PROJMAN\INSP.FRM

REVISED 08-30-94

NAISMITH ENGINEERING, INC. PROJECT INSPECTION REPORT

Owner: U.S. Ecology, Inc Beatty, NV (American Ecology) Owner's Project No: NEL Project No:				
Owner: U.S. Ecology, I.	16	Beatly, NV (Am	evican Ecology)	
Owner's Project No.:	NEI Project No.: 4	856		
Date: 1-27-98	Time:	0800	Page <u>2</u> of <u>2</u>	
Contractor: N/A		Type of inspection: □	daily 🗆 periodic	
Inspector(s): David McCovmick, P.E		Persons contacted or	n-site:	
Pick Kiel, P.E. Cocs	;)	Lovi Taquehi-	Technical Paricy	
Weather: Low 50's, clear, co	1m	Testing in progress:		
Contractor: ☐ working ☐ delayed (v ☐ delayed due to//A	veather)	Inspection-Hydr	rostatic Test	
Work in progress:				
Prepavation for hydrot	est o	f the primary	mixing tank,	
Work completed since last inspection	า:			
Continue construction of f			r pan.	
Equipment/materials received on-site	e since la	st inspection:		
N/A	•			
Summary: (Confidence from P.	1)			
9:45pm finished repairs and	d begar	hydrotest (filled	secondary)	
10:00 pm Found 3 pinhole 1				
10:20 pm began hydrotest (filled s	secondary)		
No leaks found in Primary				
11:50 pm No loss in secondary. (Attach additional sheets as required)				
Signature of inspector(s):	Me C	i.l		
Distribution:				

E:\PROJMAN\INSP.FRM

REVISED 08-30-94

NAISMITH ÉNGINEERING, INC.

TEST REPORT-U.S. Ecology, Inc.

Batch Stabilization Primary Containment Unit

SHEET NO. 1 DATE: 02/23/1998

Test Parameters

The Batch Stabilization Primary Containment Unit is filled with water in a hydrostatic test. Water level measurements were made in the secondary sump throughout the test period. All times are Pacific Standard Time. A rod was used to measure the depth of water in the secondary sump pipe located in the northeast corner. This test was performed on January 27, 1998.

	WATER LEVEL MEASUREMENTS OVER TIME					
Time	Secondary Sump (In.)	Comments				
2:30 pm	0	Initial .				
2:45 pm	.25	Gain in Secondary				
3:00 pm	.25	"Gain in Secondary				
		Drained, Dried, Locating Leaks				
	·	u				
10:00 pm	19-7/8	Filled Secondary Sump				
		Found 3 pinhole leaks on West Side				
		·				
10:20 pm	19-7/8	Filled Secondary Sump after repairs				
10:40 pm	19-7/8	No Loss				
11:00 pm	19-7/8	No Loss				
11:50 pm	19-7/8	No Loss				

CONCLUSION: Since there was no recordable loss in the secondary sump and no visible losses in the batch stabilization primary unit, the system did not leak after final repairs to the primary and passed hydrostatic test

D:\4856\HYDROTEST2.DOC

APPENDIX C CERTIFICATION LETTER

Golder Construction Services, Inc. Ouality Assurance and Construction Management

February 6, 1998

Our Reference: 987-5124

Mr. Jeffrey C. Denison, P.E. RCRA Facilities Branch Supervisor Nevada Division of Environmental Protection 333 W. Nye Lane Carson City, NV 89706

Re: CERTIFICATION OF THE MODIFICATION TO THE BATCH STABILIZATION UNIT AT THE US ECOLOGY FACILITY NEAR BEATTY, NEVADA, UNDER NEVADA DIVISION OF ENVIRONMENTAL PROTECTION PERMIT NO. NEV-HW0011

Dear Mr. Denison:

This letter is submitted to certify that the construction of the Batch Stabilization Tank has been completed and conforms with the tank system standards of 40 CFR Subpart J, including 40 CFR 264.192, as required by Section V.B.3.a of the Facility Permit (Nevada Division of Environmental Protection Permit No. NEV-HW0011). This certification applies to the facility only at the time of completion of the construction.

Mr. Rick Kiel, with Golder Construction Services, Inc. (GCS) and Mr. Dave McCormick, with Naismith Engineering, Inc. (Naismith) performed a site inspection on January 26 and 27, 1998, to provide an assessment of the integrity of the Batch Stabilization Unit (BSU) or Batch Stabilization Tank. In addition, a leak test was performed on January 27, 1998, to aid in this assessment in accordance with 40 CFR Subpart J - Tank Systems; Section 264.191 (b) (5).

The BSU was modified according to the "Revised Design for Double Walled Steel Batch Stabilization Unit," Revision 2, dated January 1998, by Naismith Engineering, Inc. and in accordance with additional field modifications deemed necessary. The modifications consisted of constructing a new primary containment unit inside the existing BSU, and converting the existing BSU to provide secondary containment. These modifications make the system capable of handling the hazardous wastes for which it was designed, without release for the intended life of the system.

I certify under penalty of law that this document and all attachments were prepared under my direction or supervision in accordance with a system designed to assure that qualified personnel properly gather and evaluate the information submitted. Based on my inquiry of the person or persons who manage the system, or those persons directly responsible for gathering the information, the information submitted is, to the best of my knowledge and belief, true, accurate, and complete. I am aware that there are significant penalties for submitting false information, including the possibility of fine and imprisonment for knowing violations.

This certification will be followed by a report from Naismith (the Design Engineer) outlining the details of the work, and will include a complete set of as-built drawings.

If you should have any questions or need additional information, please feel free to contact us.

Sincerely,

GOLDER CONSTRUCTION SERVICES, INC.

Rick Kiel, P.E.

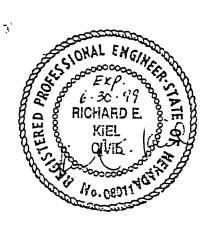
Senior Engineer

Rick Kul

cc: Mr. Grant Jackson, P.E., Naismith Engineering, Inc., Corpus Christi, Texas

Mr. Zaki Naser, General Manager, US Ecology, Inc., Beatty, Nevada

Ms. Lori Taguchi, Engineering Manager, US Ecology, Inc., Beatty, Nevada



DOUBLE-WALLED STEEL BATCH STABILIZATION UNIT AND REAGENT SILOS

US Ecology, Inc.

Hazardous Waste Management Facility

Beatty, Nevada

Prepared by

AquAeTer, Inc.

Englewood, CO

October 9, 2001

Each off the two bays of the BSU ("pans") will be constructed in a similar fashion. Pan construction will have a primary and secondary containment system, constructed of one-inch thick welded steel plate with standard structural steel members. The slope of the floor of the primary containment of the pans will be toward the mixing unit; this will facilitate the mixing process, and prevent waste materials and precipitation that falls on the pans from migrating beyond the limits of the pans.

Separate sumps will be located inside the secondary containment structure of each pan, near the mixing unit. The slope of each secondary containment structure will be toward the respective sump. The sumps will be inspected daily for the presence of liquid within the secondary containment structure. A steel pipe will extend into the sump to allow the inspection and extraction of any liquid that accumulates within the secondary containment sump. The primary and secondary containment structures will be sealed (welded) to prevent the migration of surface liquid from outside of the primary or secondary containment structures into the sump. Both containment structures are constructed of one-inch thick welded steel plate.

The areas beneath the truck load out and mixing area surrounding the pans will be underlain with 1/4-inch thick steel plate covered with six inches of sacrificial soil and 12 inches of gravel. For a distance extending outwards 12 feet from the edge of the pans, a concrete layer will be placed over the soil to facilitate operations near the pan. For an additional 12 feet beyond that, the sacrificial soil will form the top layer. The entire 24-feet wide concrete and sacrificial soil areas will be underlain by ¼-inch thick steel plates sloped to drain to separate collection sumps.

The load out area is where the stabilized waste will be transferred from the pan to the transport truck that will transfer the stabilized waste to the landfill. The steel plate of the load-out pans will be sloped to two separate sumps for the removal of any liquid that may accumulate within the gravel above the steel plate. A surface berm of soil will be placed around the area to prevent the run-on of precipitation from entering the truck load out area. A drawing of the BSU is included in Appendix A.

4.0 BSU CONSTRUCTION

4.1 Construction Standards

The BSU will be used for the mixing of hazardous waste and debris with reagents and stabilizing material to allow the disposal of the mixed material in the landfill. The BSU is planned for use under atmosphereic pressure conditions to accommodate the mixing activities, including both the distributed load of the waste and reagents and the small impact loads anticipated from the mixing head. Experience gathered from the single pan BSU already located on site was incorporated into the design.

The secondary containment structures are designed to collect and drain liquids that pass through the primary walls of the pans into two separate sumps. Additionally, the steel pan underlying the surrounding load-out area includes two sumps installed to capture precipitation and surface water that may penetrate the sacrificial soil layer.

4.2 Tank Integrity Assessment

The integrity of the secondary containment structure was tested by filling each side of the BSU secondary containment structure with water and observing the pan interior for the presence of leaks. Water level in the two secondary containment structures was observed for level declines that could be caused by leaks that were not visible. The tank integrity test was performed before backfill was placed around the tank. As a result of the initial test, minor leaks were detected. These leaks were re-welded and re-

tested to demonstrate integrity. Notes documenting the integrity of the secondary containment structure is included in Appendix B.

The secondary containment structures for the BSU consists of a redundant one-inch thick welded-steel plate tank surrounding the primary (interior) tanks. The secondary containment structure tank is attached to the primary tank, with separation provided by structural steel angles. The secondary containment structure is completely sealed to prevent the influx of surface water or precipitation. Therefore, the secondary containment structure only has to hold 100 percent of the contents of the primary (interior) tank. The spacing between the two tanks is about 4 inches on all sides, along the dividing wall, and beneath the tanks. Since the two tanks are joined at the top (same elevation), the space formed by the structural steel angles ensures the containment is sufficient, and no additional calculations are required to demonstrate containment volume.

4.3 Structural Strength

The steel BSU tanks and the concrete reagent silo foundation will be designed to withstand the governing loads imposed by the design seismic loading criteria for a seismic zone 3. The BSU tanks are buried in level ground, and are not subject to sliding or overturning by seismic activity.

A mixing head will be used to perform the stabilization process. If used carelessly or improperly, the mixing head may be capable of damaging the floor or walls of the tanks. However, routine inspection and prompt repair of damage should prevent failure of the unit from punctures. Additionally, the BSU has been reinforced, as compared to the existing on-site BSU by the use of thicker steel plate, which should also contribute to the durability of the unit.

4.4 Corrosion Protection

The steel components of the BSU are cathodically protected against corrosion by the use of one pound aluminum sacrificial anodes installed on the tank walls. One aluminum anode will be bolted to each wall of the exterior of the secondary containment structure. The primary containment unit is welded to the secondary containment unit, and is therefore, also protected. The aluminum anodes will be monitored for corrosion and replaxed as necessary.

4.5 Compatibility with Waste

The BSU could potentially be exposed to any of the waste streams handled at the facility, including inorganic aquaeous liquids, organic liquids, water-based sludges, organic sludges, inorganic and organic solids. The primary wastes received for stabilization at the facility will be organic and inorganic solids and sludges.

Highly reactive materials, and materials with a high pH or low pH represent the greatest potential for incompatibility with the steel tanks. The likelihood of chemical incompatibility between reactive, acidic, or alkaline wastes and the steel tanks is considered small due to the treatment reagents' tendance to quickly combine with the most reactive constituents in the waste, limiting their ability to further react with the tank material.

To further prevent the failure of the unit from incompatibility with the wastes, the BSU will be inspected routinely for signs of corrosion and structural failure. Any problems detected will be corrected prior to continuing stabilization operations. Routine cleaning operations between different waste types will remove waste residues remaining in the unit.

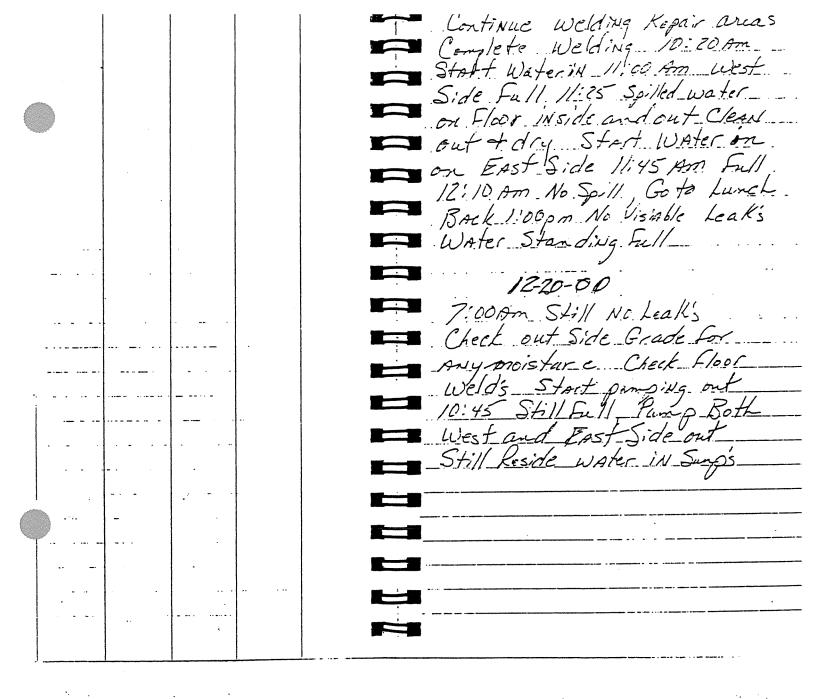
APPENDIX A

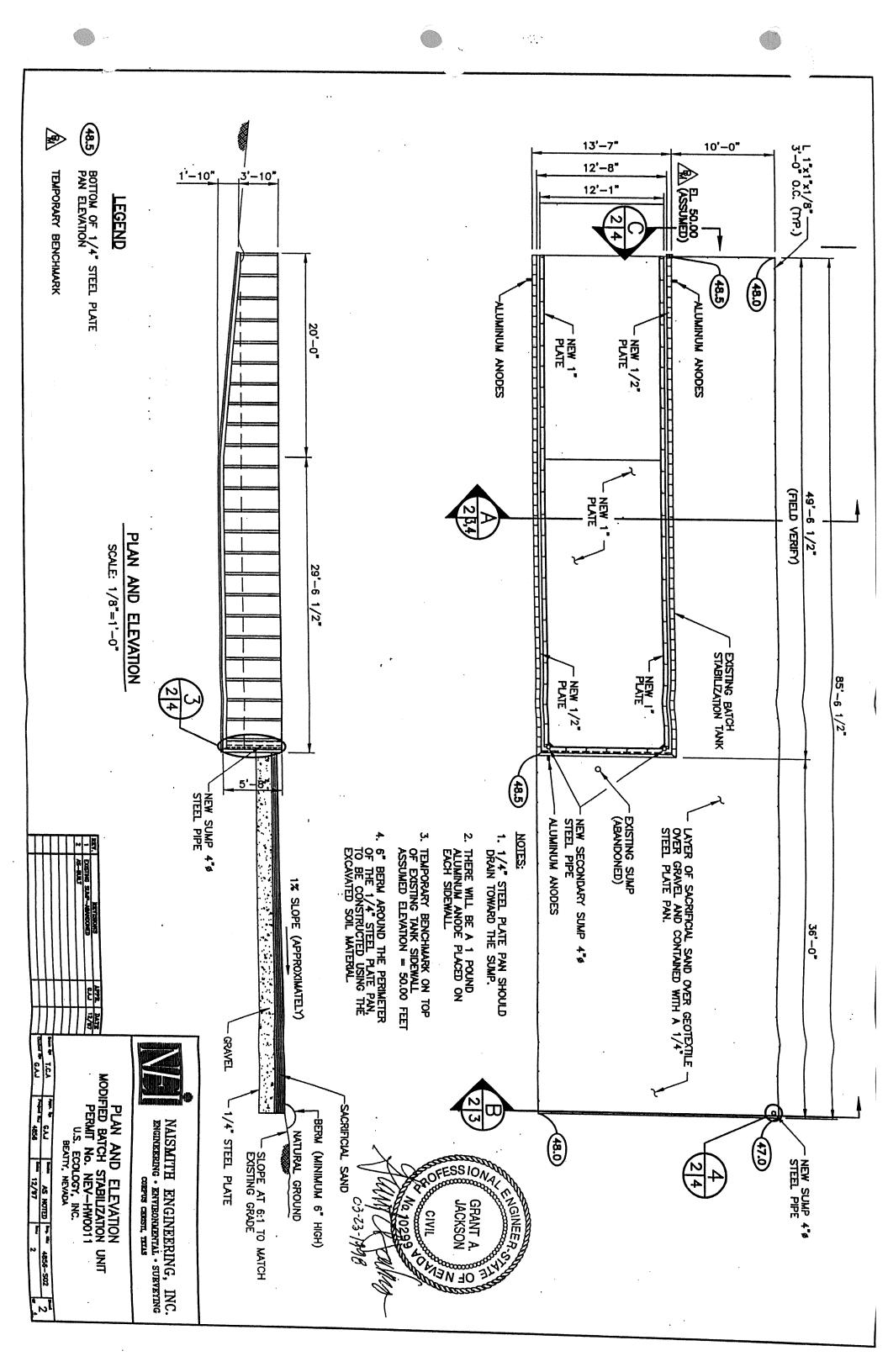
Batch Stabilization Diagram

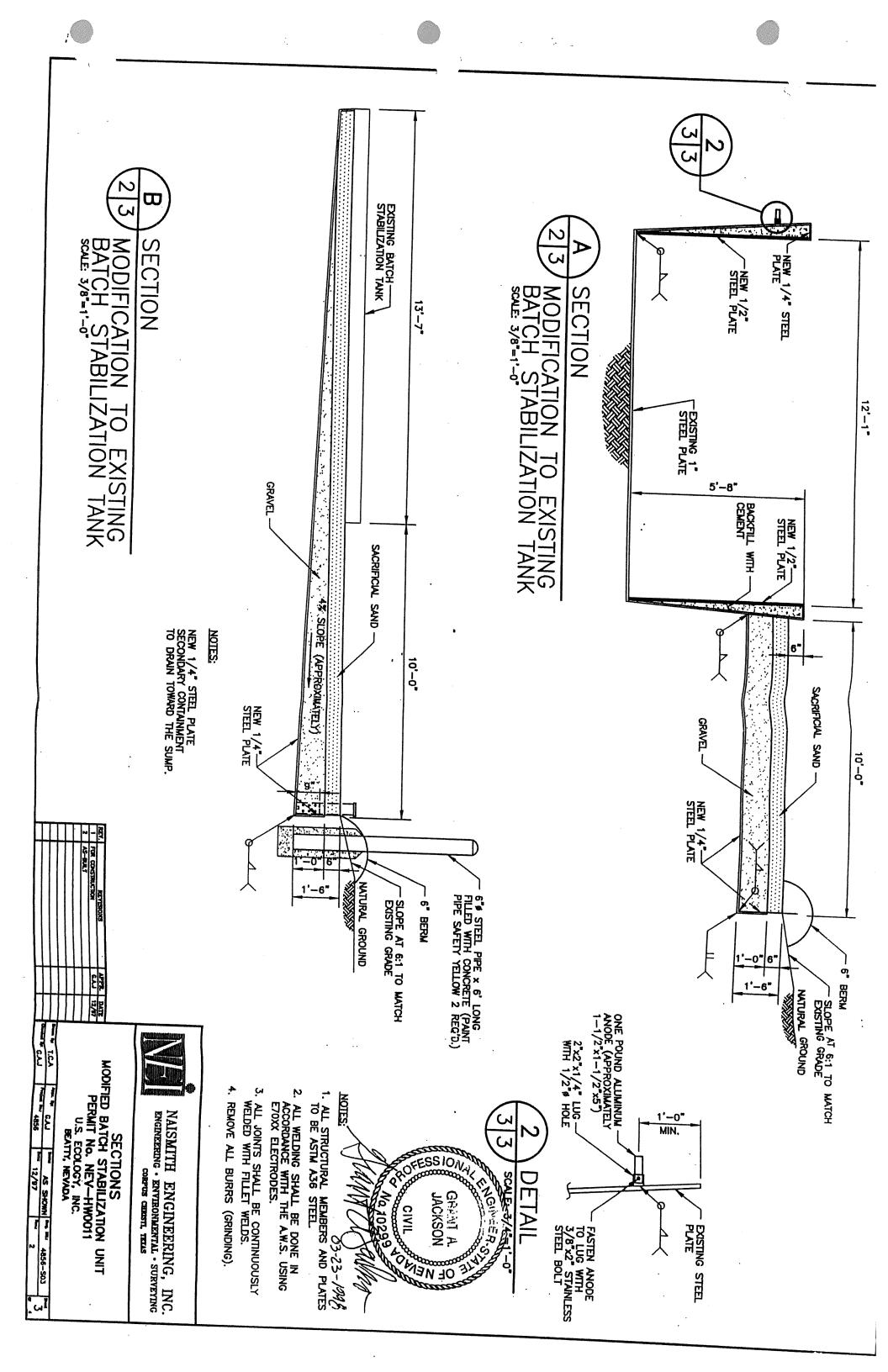
APPENDIX B

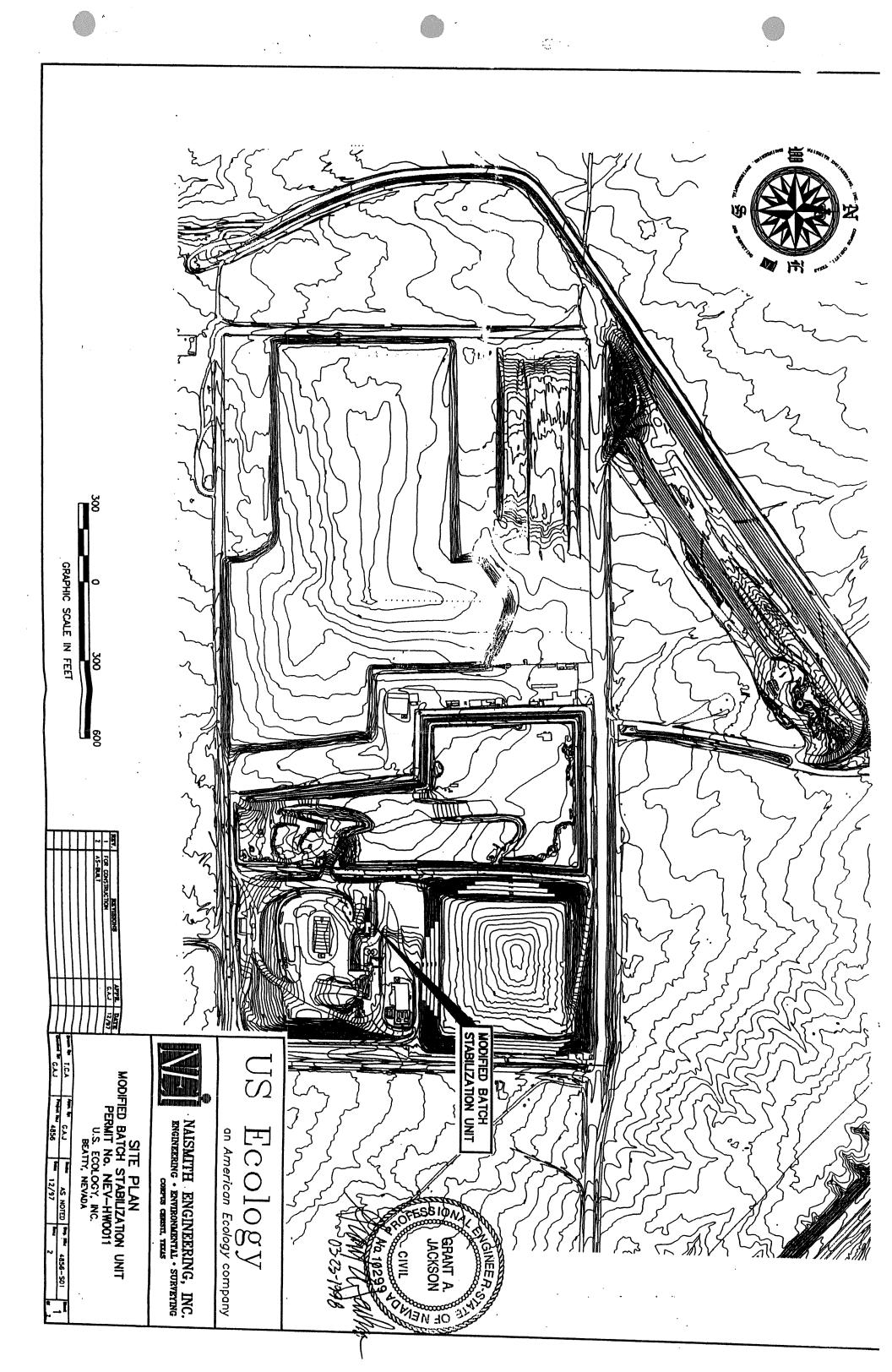
Leak Integrity Assessment Notes

12-18-00 1 Hydro Test New PAN's Start WAter IN 7:40 Am Water Started in West Side 7:55 West Side Full Visual Check Found Leak IN Cop MARK For Repair - Found Leak's IN Center WAll Tie IN Check IN Side Small scapen Top Cap - Started Purping Start Water IN East Side 8:40 East Sid Full 09:00 Checking for Leak's Small Seep Mark For repair One Small Seep South west Corner mark for Repair Stort Purping out 10:20Am water out 10:45-Start grinding out Repair Welding Repair









DOUBLE-WALLED STEEL BATCH STABILIZATION UNIT TANK INTEGRITY ASSESSMENT

US Ecology, Inc.

Hazardous Waste Management Facility

Beatty, Nevada

Prepared by

AquAeTer, Inc.

Englewood, CO

January 15, 2002

TABLE OF CONTENTS

1.	Introd	uction	1			
2.	Facility Information					
3.	BSU Operations					
4.	BSU	Construction	1			
	4.1	Construction Standards	1			
	4.2	Construction	2			
	4.3	Description of Secondary Containment Structure	3			
	4.4	Structural Strength	3			
	4.5	Corrosion Protection				
	4.6	Compatibility with Waste	4			
5.	Certif	ication	5			

1. INTRODUCTION

US Ecology, Inc. has requested that AquAeTer assist with the tank integrity assessment for the new Batch Stabilization Unit (BSU) constructed at the Hazardous Waste Management Facility (HWMF) near Beatty, Nevada. This tank integrity assessment conforms to the requirements of 40 CFR Part 264, Subpart J, Tank Systems.

2. FACILITY INFORMATION

The BSU will be used to stabilize and/or solidify hazardous wastes at the HWMF and treat hazardous debris prior to landfilling. Waste stabilization will be conducted in the BSUs, where waste and stabilization reagents (e.g., cement, kiln dust, lime, etc.) will be thoroughly mixed until a relatively homogeneous mixture is achieved. Water will be added to promote mixing and control air emissions, as necessary.

3. BSU OPERATIONS

The design of the double bay BSU (BSU 2) allows two separate wastes to be treated sequentially. The addition of a second mixing head would allow simultaneous stabilization and mixing activities to be performed on different wastes in each BSU bay. The BSU is constructed with truck load-out aprons on the north side of each BSU bay. Reagent silos are located near the BSU. The mixing unit is located at the center point on the south side of the two bays, allowing it to reach into each mixing bay.

4. BSU CONSTRUCTION

4.1 Construction Standards

The BSU is used for the mixing of hazardous waste and debris with reagents and stabilizing material to prepare the mixed material for disposal in the landfill. The BSU is used under atmospheric pressure conditions to accommodate the mixing activities, including both the distributed load of the waste and reagents and the small impact loads

anticipated from the mixing head. Experience gathered from the single pan BSU, already located on site, was incorporated into the design of the new units.

A secondary containment structure is an integral part of the design to collect and drain liquids that pass through the primary walls of the two separate mixing bays. The secondary containment structures are accessed by two separate sumps. Additionally, the steel pan underlying the surrounding truck load-out apron area includes two sumps installed to capture precipitation and surface water that may penetrate the sacrificial soil layer.

4.2 Construction

Each of the two bays ("pans") of the new double-bay BSU is constructed in a similar fashion. Pan construction incorporates a primary and secondary containment system; each constructed of one-inch thick welded steel plate with standard structural steel members. The slope of the floor of the primary containment of the pans is toward the mixing unit; this facilitates the mixing process.

Separate sumps are located inside the secondary containment structure of each pan, near the mixing unit. The slope of each secondary containment structure is towards the respective sump. A steel pipe extends into the sump to allow the inspection and extraction of any liquid that accumulates within the secondary containment sump. The primary and secondary containment structures are sealed (welded) to prevent the migration of surface liquid from outside of the primary or secondary containment structures into the sump.

The load-out apron area is where the stabilized waste is transferred from haul trucks to the pan or from the pan to transport vehicles that transfers the stabilized waste to the landfill. The areas beneath the truck-load out apron area surrounding the pans are underlain with 1/4-inch thick steel plate sloped to drain to separate collection sumps, and covered with gravel and sacrificial soil.

4.3 Description of Secondary Containment Structure

In each double-walled tank system, the primary tank holds the waste materials and the secondary tank serves as secondary containment. Each secondary tank slopes to a collection sump. Each secondary containment structure is completely sealed to prevent the influx of surface water or precipitation. The secondary containment structure holds slightly more than 100 percent of the contents of the primary (interior) tank. The spacing between the two tanks is about four inches on all sides, along the dividing wall, and beneath the tanks. Since the two tanks are joined at the top (same elevation), the space formed by the structural steel angles ensures the containment is sufficient, and no additional calculations are required to demonstrate containment volume.

The integrity of the secondary containment structure was tested by filling each side of the BSU secondary containment structure with water and observing for the presence of leaks to the interior (i.e., into the pan) or to the exterior (i.e., outside the outer secondary containment wall). The tank integrity test was performed before backfill was placed around the tank. As a result of the initial test, minor leaks in the tanks were detected. These leaks were re-welded. The integrity of the secondary containment structure was retested by filling each side of the BSU secondary containment structure with water, and observing the fluid level for six hours for declines that could be caused by leaks that were not visible. A control test tank open to the atmosphere also was observed for evaporation losses. No leaks were detected in the integrity test of the secondary containment tanks. Notes documenting the results of the hydrostatic tests are included in facility records. The integrity of the welded steel aprons also was tested prior to the placement of the gravel and sacrificial soil.

4.4 Structural Strength

The BSU tanks are buried in level ground, and are not subject to sliding or overturning by seismic activity.

A mixing head will be used to perform the stabilization process. If used carelessly or improperly, the mixing head may be capable of damaging the floor or walls of the tanks. However, routine inspection and prompt repair of damage should prevent failure of the unit from such damage. Additionally, the BSU has been strengthened, as compared to the existing on-site BSU, by the use of thicker steel plate, which should also contribute to the durability of the unit.

4.5 Corrosion Protection

The steel components of the BSU are cathodically protected against corrosion by the use of one pound aluminum sacrificial anodes installed on the tank walls. One aluminum anode will be bolted to each side of the exterior of the secondary containment structure. The primary containment unit is welded to the secondary containment unit, and is therefore, also protected. The aluminum anodes will be monitored for corrosion and replaced as necessary.

4.6 Compatibility with Waste

The BSU could potentially be exposed to any of the waste streams handled at the facility, including inorganic aqueous liquids, organic liquids, water-based sludges, organic sludges, inorganic and organic solids. The primary wastes received for stabilization at the facility will be organic and inorganic solids and sludges.

Highly reactive materials, and materials with a high pH or low pH represent the greatest potential for incompatibility with the steel tanks. The likelihood of chemical incompatibility between reactive, acidic, or alkaline wastes and the steel tanks is considered small because of the treatment reagents' tendency to quickly combine with the most reactive constituents in the waste, limiting their ability to further react with the tank material. Routine cleaning operations between different waste types will remove waste residues remaining in the unit.

5. CERTIFICATION

AquAeTer, Inc. services relating to certification of Batch Stabilization Unit 2 at the Beatty, Nevada facility were provided in a manner that is consistent with current standards of practice and the degree of care and skill ordinarily exercised under similar conditions by reputable members of the same profession in similar localities. The conclusions presented in this certification are based upon observations made by AquAeTer representatives at selected locations and times during construction and testing of Batch Stabilization Unit 2.

The signature and seal provided below is a declaration by the Professional Engineer that, in his professional judgment, the subject project was designed, constructed, and tested in manner consistent with the referenced design document and applicable State and Federal regulations.

This certification was prepared under the Professional Engineer's direction or supervision in accordance with a system designed to assure that qualified personnel properly gather and evaluate the information submitted. The information submitted is, to the best of the Professional Engineer's knowledge and belief, true, accurate, and complete.

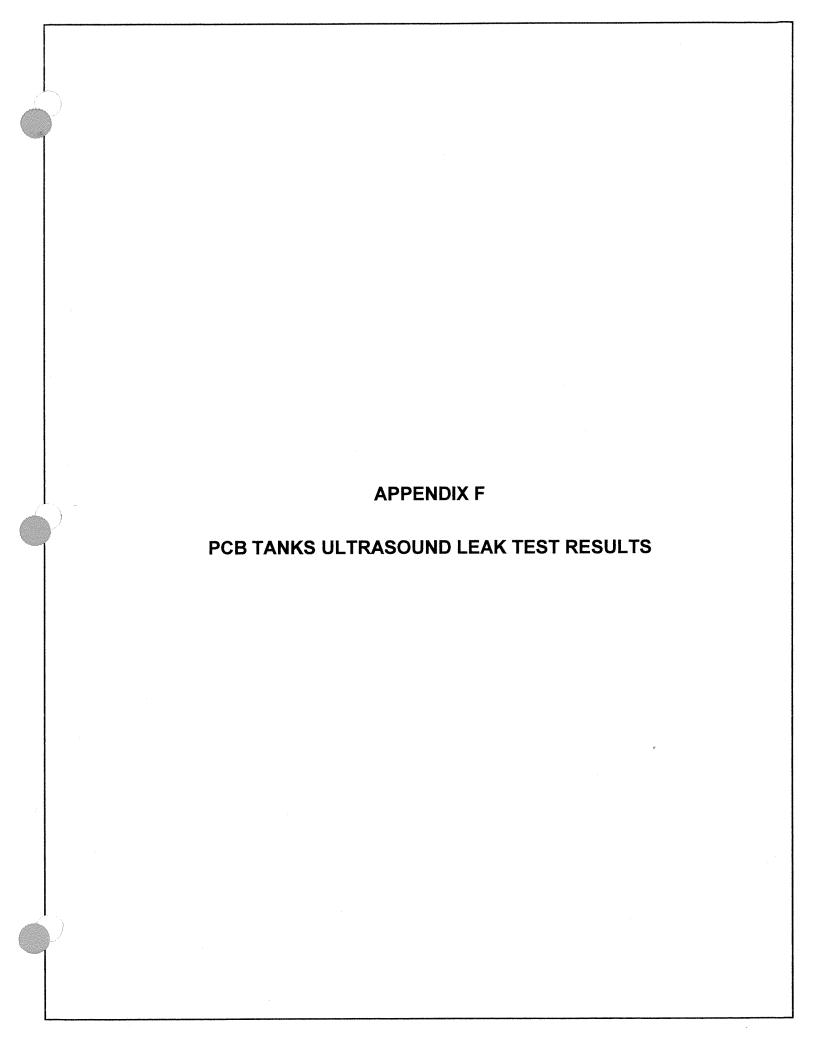
AquAeTer, Inc.

By:

•

Stephen II. Wampler,

STEPHEN L
WAMPLER
NO. 1364





3611 West Tompkins Avenue Las Vegas, Nevada 89103 -5618 (702) 798-8050 • fax 798-7664

REPORT ON ULTRASONIC THICKNESS TESTING

Page 1 of 2

CLIENT

US ECOLOGY PO BOX 578

BEATTY, NV 89003

Job No:

4168JK014

Event/Invoice No:

01

Authorized By:

MARK JOHN

Observation Made By:

D. ALDERSON

Date of Report:

1/15/09

Project

PCB LIQUID STORAGE TANKS (5 each)

Date of Testing

1/15/09

Location

US Ecology's Landfill and Hazmat disposal; US 95, 11 miles south of Beatty, NV

Per client request, WTI performed ultrasonic thickness testing on PCB LIQUID STORAGE TANKS identified as WMU tanks T-4, T-5, T-6, T-7 and T-8 (formerly identified as A, B, C, D and on Vacuum tank E).

Test equipment: KB, USN-58L with FH2E dual transducer. Calibrated on 1018 steel step wedge. Echo technique was used to preclude the need to remove the new paint at the test spots.

There are no significant deviations in material thickness measurements compared to previous year's readings.

Tanks exterior paint is in good condition except the new paint does not extend to the tank center bottoms.

(T-top, B-bottom, N-north, S-south, E-east, W-west, C-center)

Thickness Test Results in inches

Tank A (T-4): horizontal I	E-W orientation			The state of the s	
East End: T-B-N-S-C	0.260	0.263	0.267	0.263	0.274
West End: T-B-N-S-C	0.250	0.258	0.261	0.265	0.260
Top: East to West	0.255	0.265	0.265	0.265	0.265
Bottom: East to West	0.255	0.260	0.272	0.265	0.258
North: East to West	0.262	0.262	0.265	0.269	0.257
South: East to West	0.260	0.262	0.259	0.267	0.258
Observations:					

Tank B (T-5): horizontal N-S	orientation				
North End: T-B-E-W-C	0.237	0.229	0.237	0.239	0.237
South End: T-B-E-W-C	0.246	0.236	0.234	0.236	0.238
Top: North to South	0.253	0.244	0.265	0.246	0.246
Bottom: North to South	0.248	0.267	0.260	0.247	0.251
East: North to South	0.258	0.262	0.260	0.255	0.253
West: North to South	0.257	0.265	0.246	0.251	0.245
Observations:		,		İ	



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CONTINUATION **ULTRASONIC THICKNESS TESTING**

Page 2 of 2

Tank C (T-6): horizontal N-S	orientation				
North End: T-B-E-W-C	0.271	0.277	0.265	0.265	0.275
South End: T-B-E-W-C	0.232	0.244	0.229	0.234	0.246
Top: North to South	0.267	0.274	0.273	0.234	0.229
Bottom: North to South	0.265	0.272	0.255	0.241	0.234
East: North to South	0.272	0.277	0.269	0.246	0.243
West: North to South	0.265	0.274	0.244	0.241	0.236
Observations:					

Tank D (T-7): horizonta	I E-W orientation				
East End: T-B-N-S-C	0.276	0.277	0.276	0.279	0.284
West End: T-B-N-S-C	0.268	0.270	0.270	0.260	0.274
Top: East to West	0.265	0.273	0.265	0.245	0.281
Bottom: East to West	0.262	0.260	0.246	0.286	0.272
North: East to West	0.265	0.267	0.246	0.274	0.274
South: East to West	0.265	0.255	0.246	0.267	0.271
Observations:					

Tank E (T-8): horizontal E	-W orientation		. 1		
East End: T-B-N-S-C	0.244	0.241	0.248	0.249	0.229
West End: T-B-N-S-C	0.255	0.241	0.251	0.251	0.234
Top: East to West	0.232	0.234	0.243	0.243	0.230
Bottom: East to West	0.234	0.232	0.246	0.242	0.237
North: East to West	0.234	0.229	0.250	0.230	0.231
South: East to West	0.232	0.243	0.244	0.229	0.232
Observations:					

If there are any questions, or if we can be of further assistance, please call us.

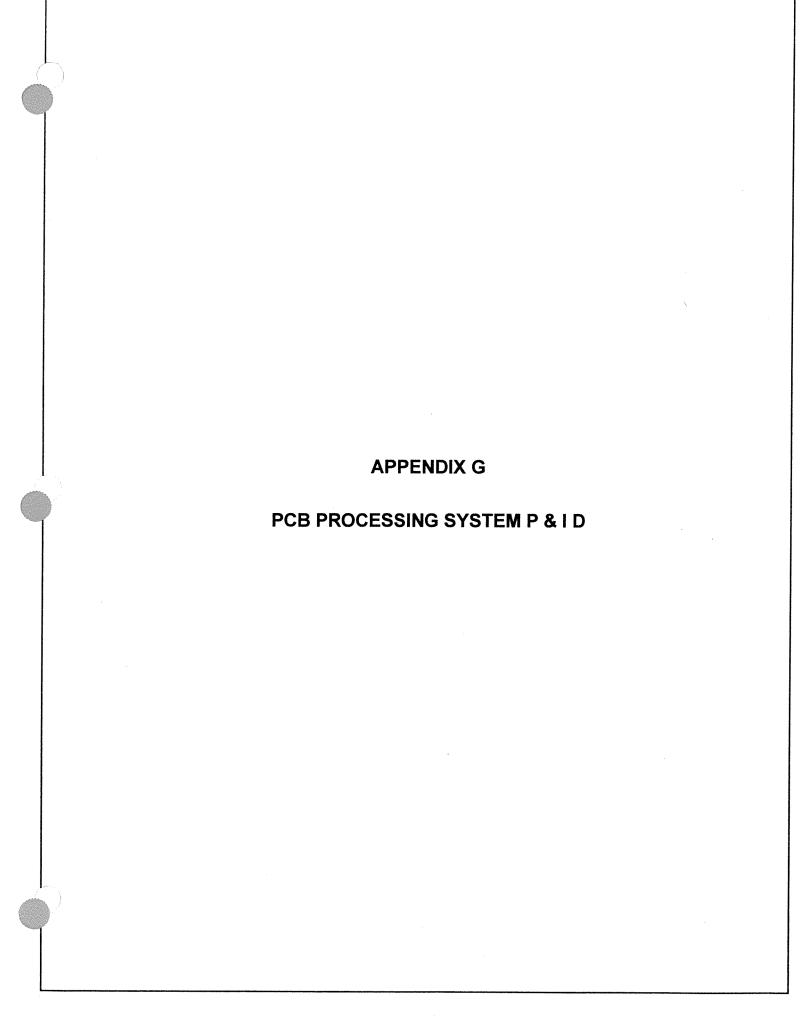
Respectfully submitted, WESTERN TECHNOLOGIES INC.

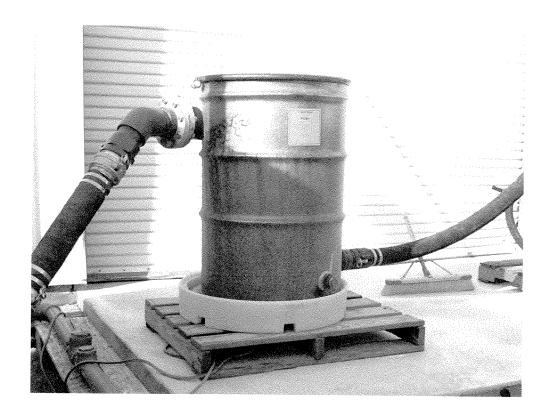
David B. Alderson, CWI, ASNT Level III

Alderson

Director of Non-Destructive Testing

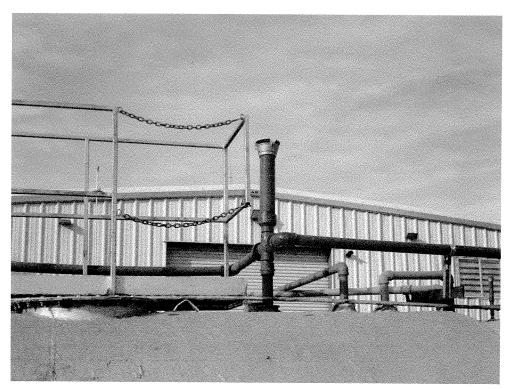
Observations reported herein are indicative of conditions found at the exact location and time of observation only. The above services and report were performed pursuant to the terms and conditions of the contract between WT and client. WT warrants that this was performed under the appropriate standard of care, including the skill and judgment that is reasonably expected from similarly situated professionals. No other warranty, guaranty, or representation, either expressed or implied is included or intended.

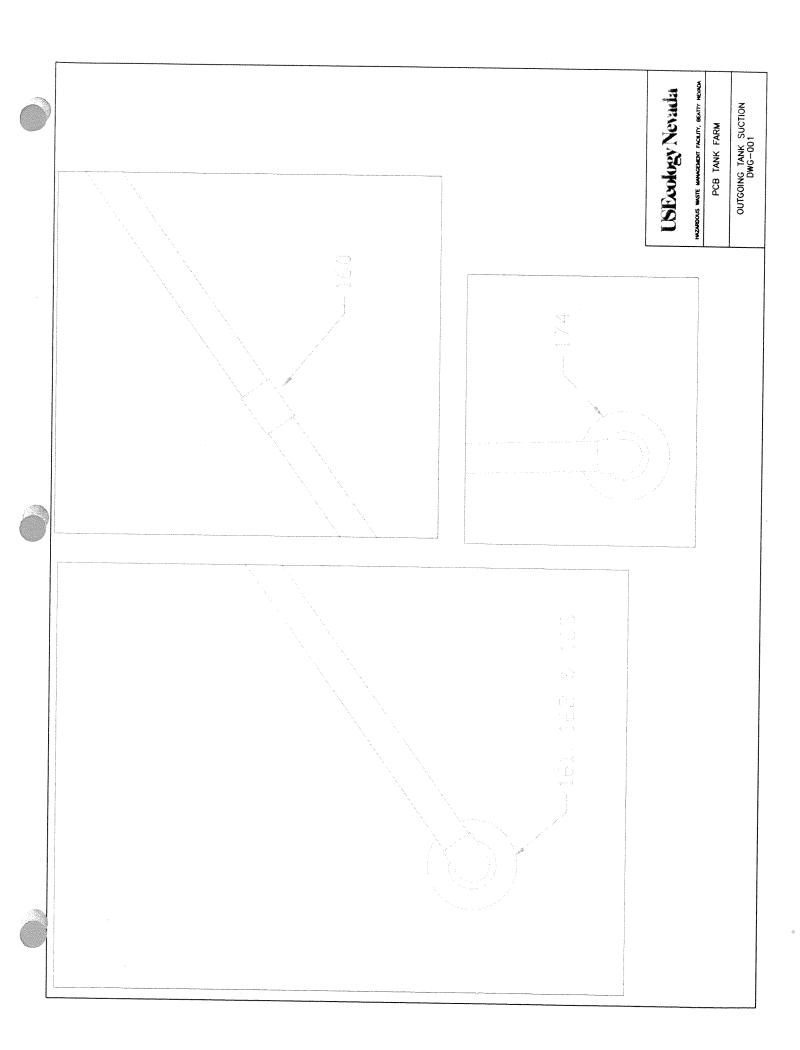




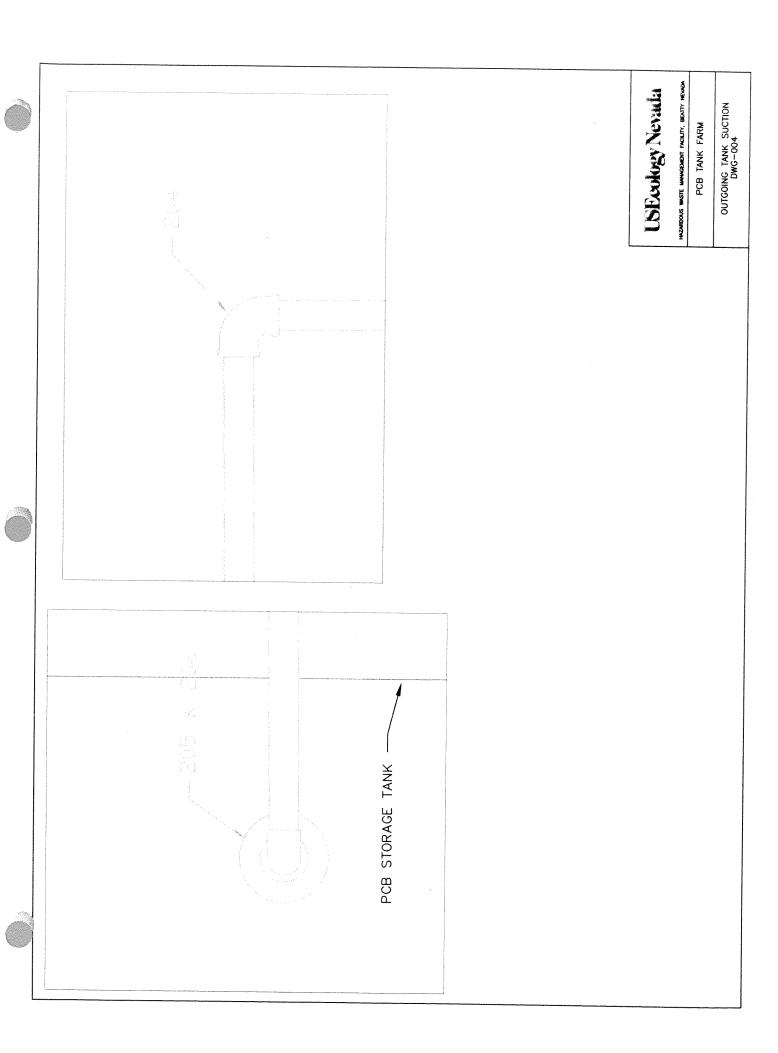


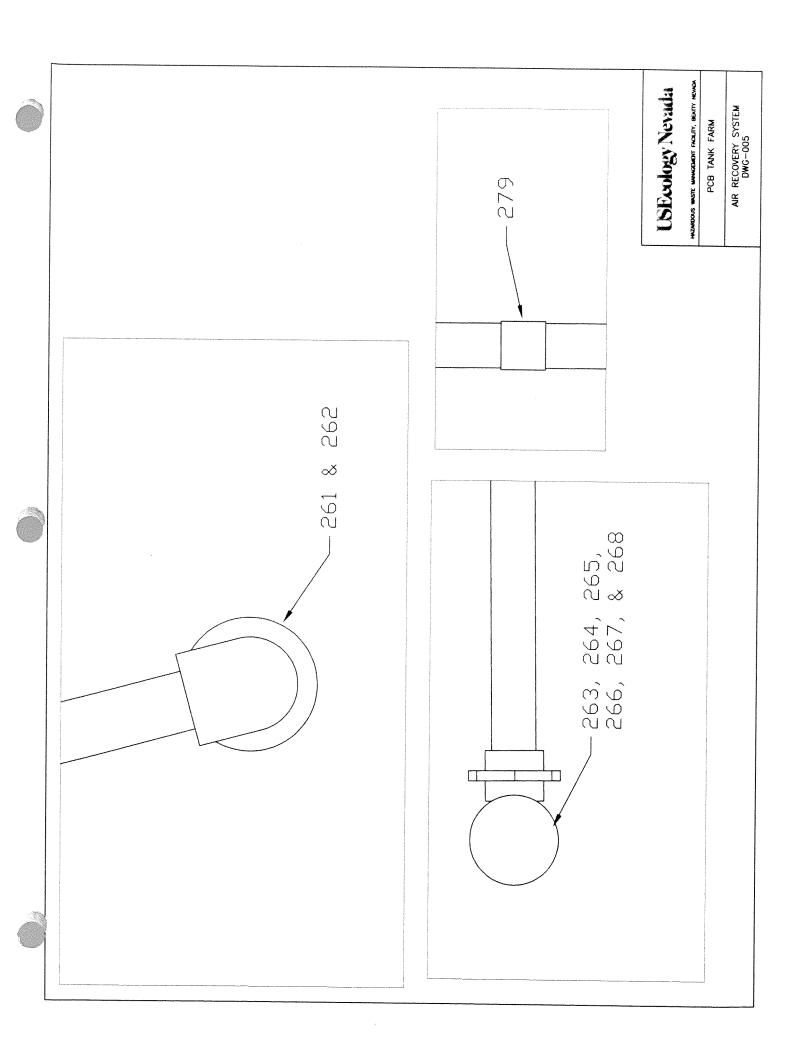


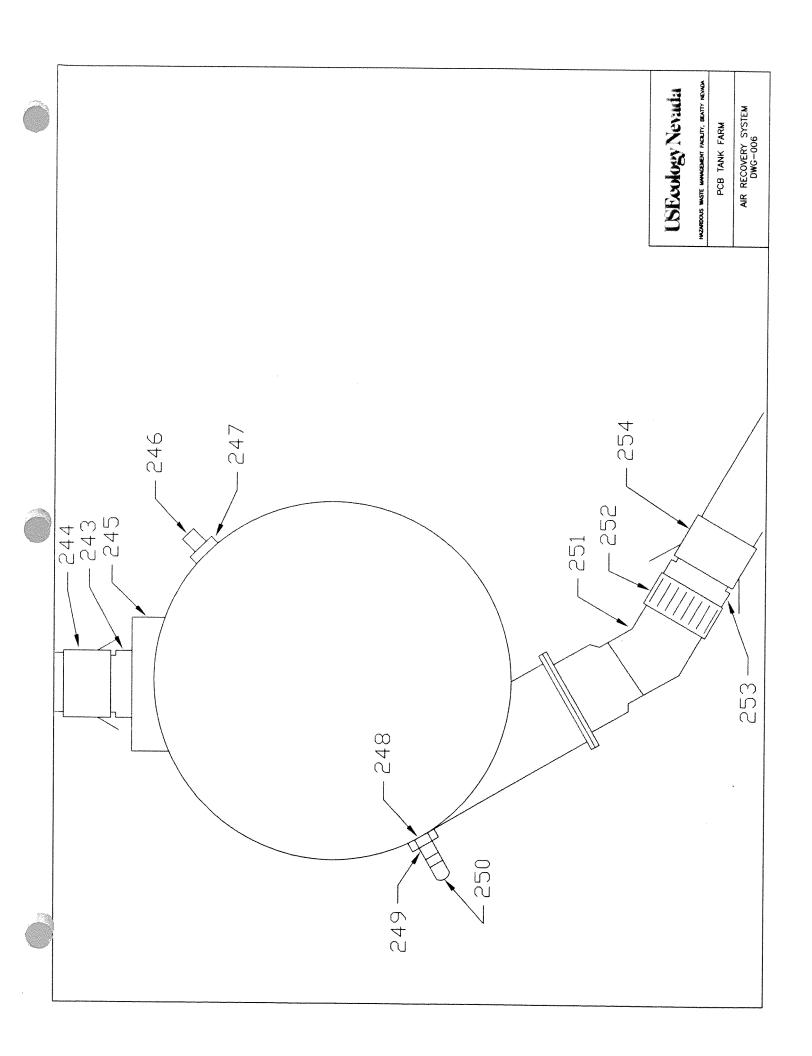


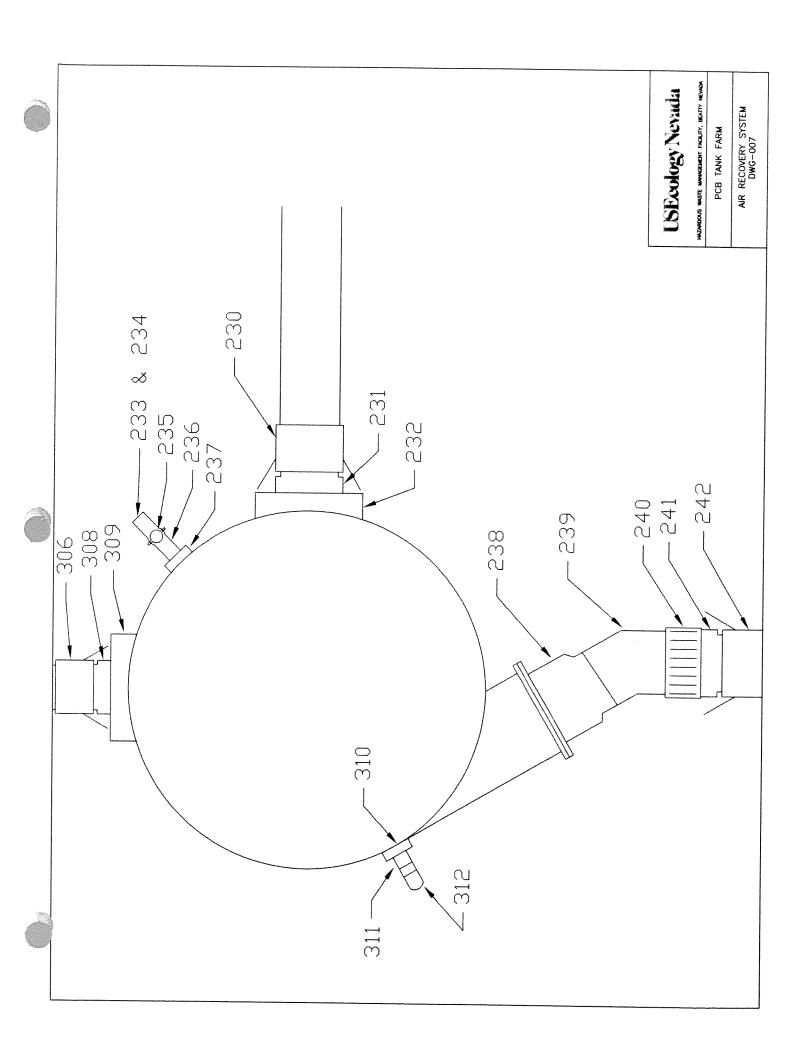


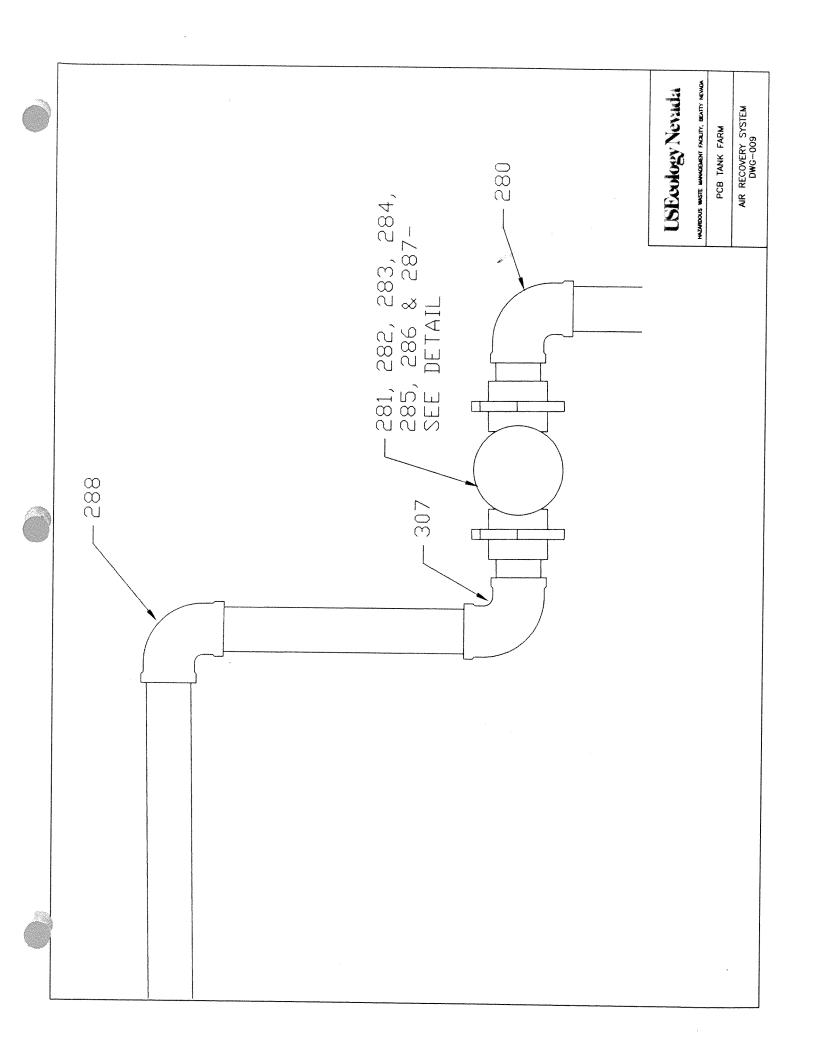
HAZARDOUS WASTE MANAGEMENT FACULTY, BEATTY NEVADA USEcology Nevada OUTGOING TANK SUCTION DWG-002 PCB STORAGE TANK PCB TANK FARM

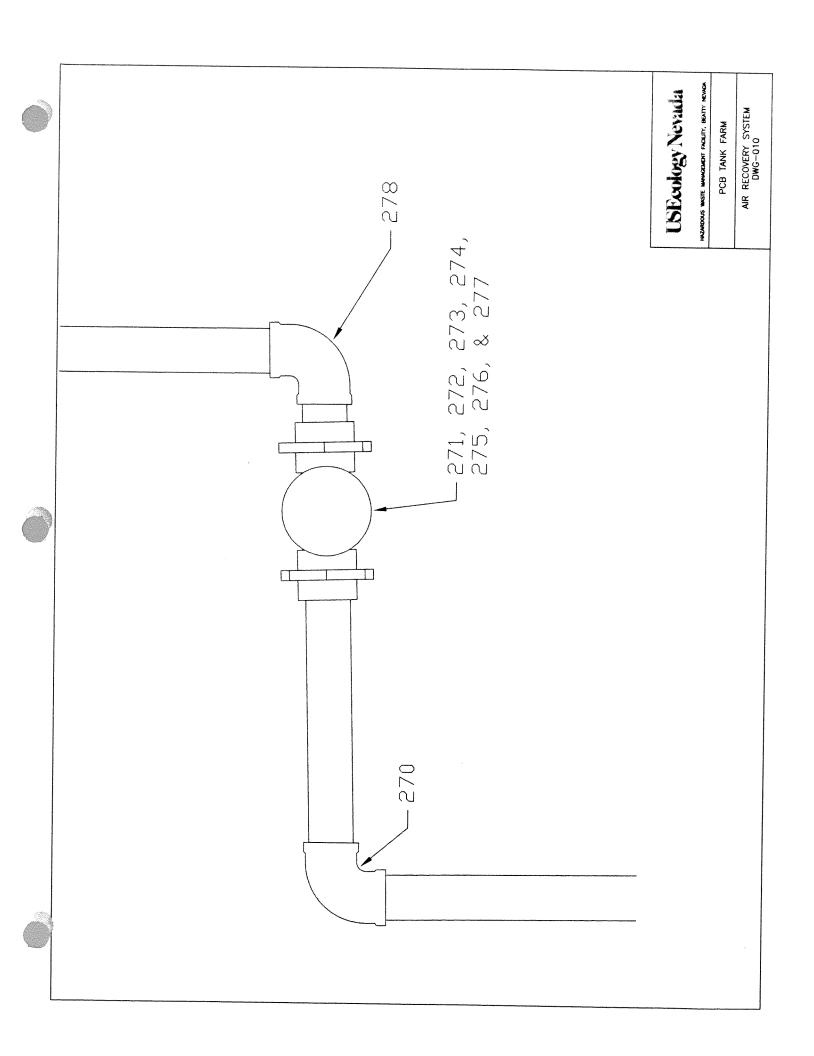


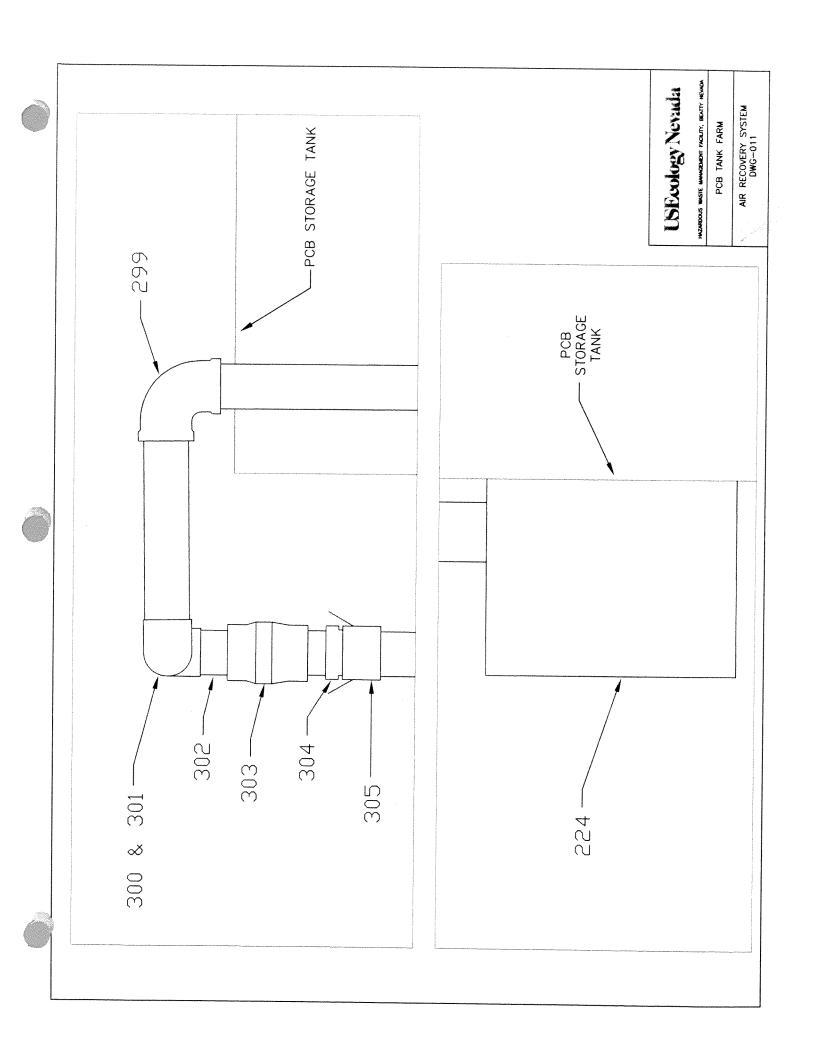


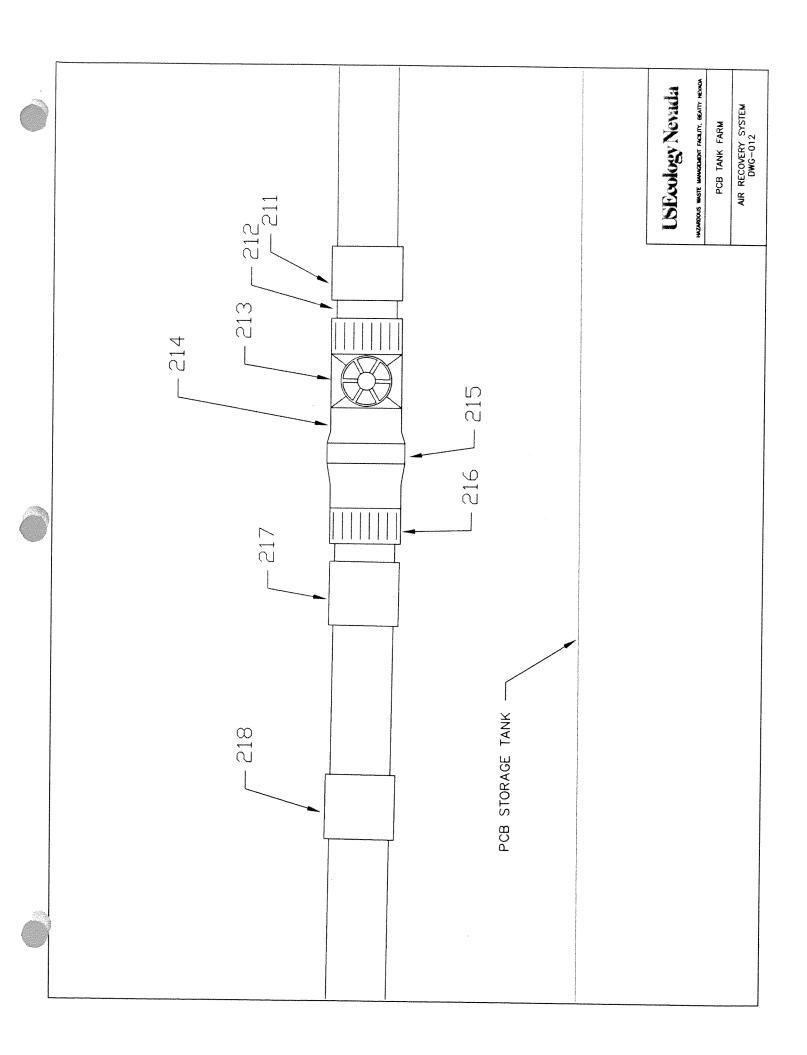


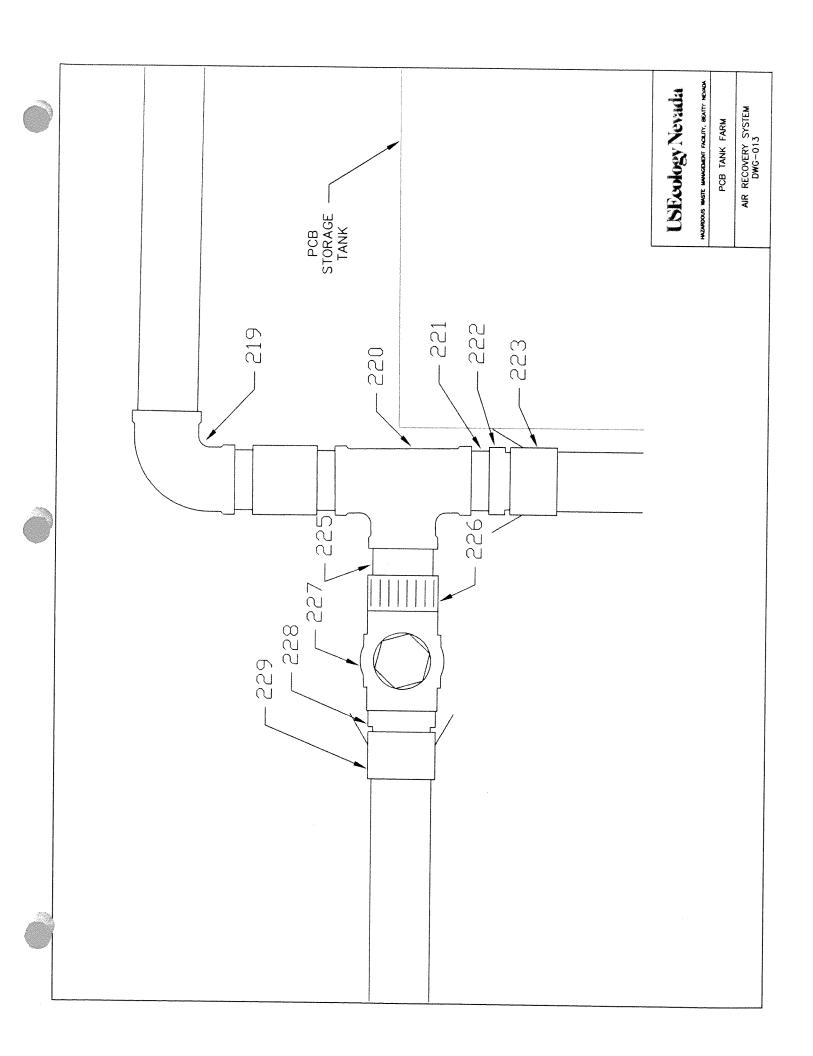


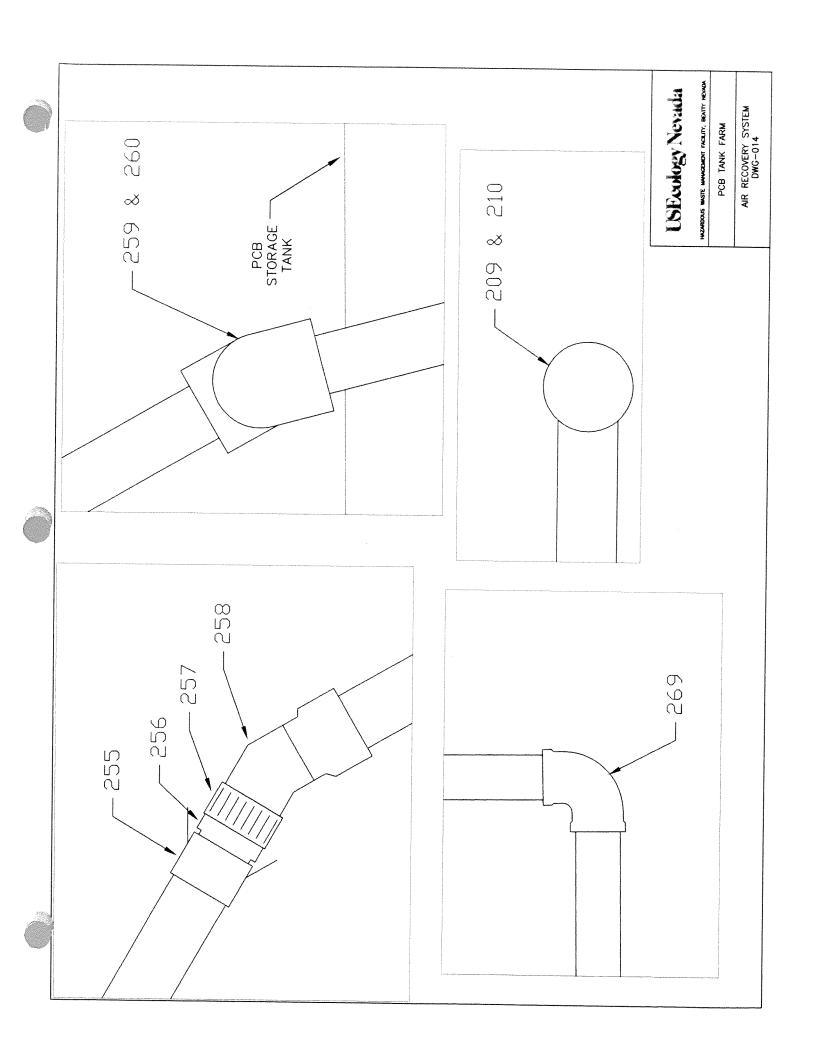


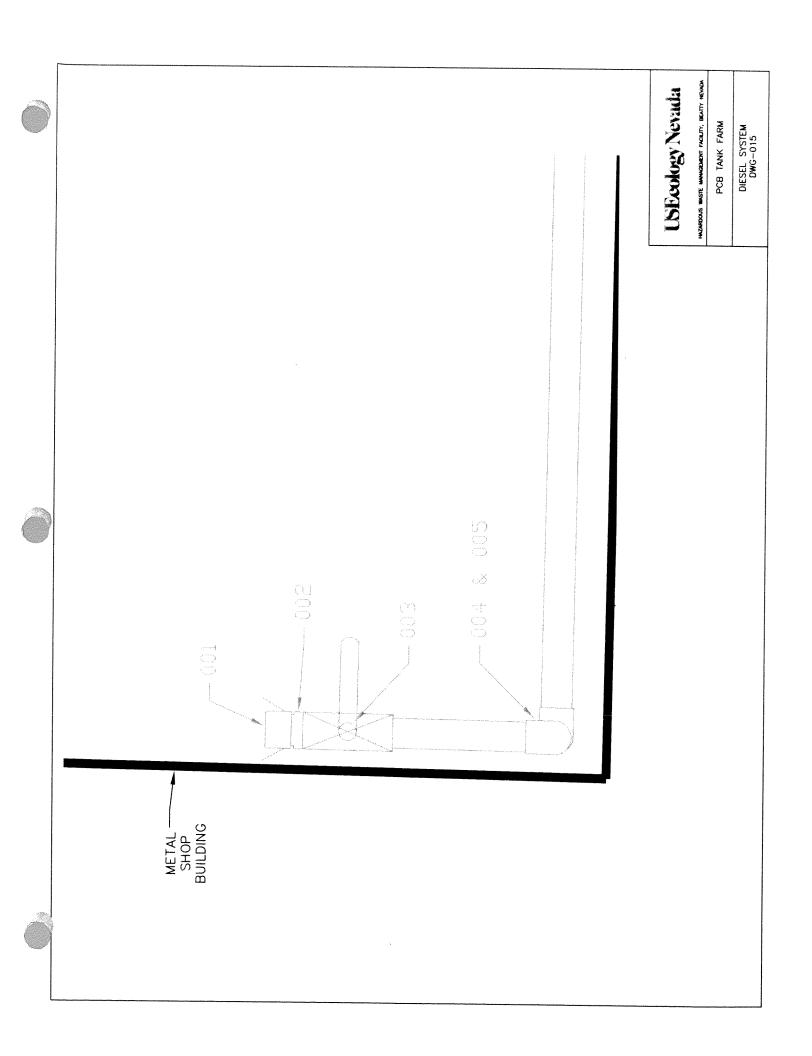


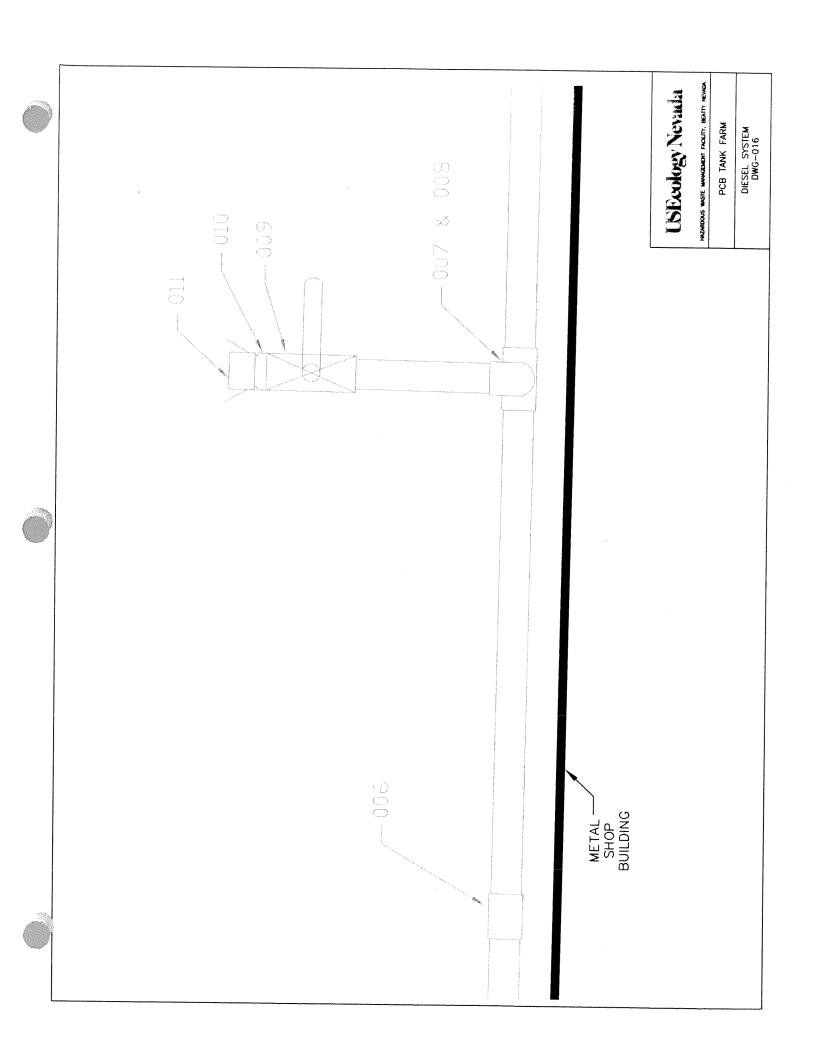


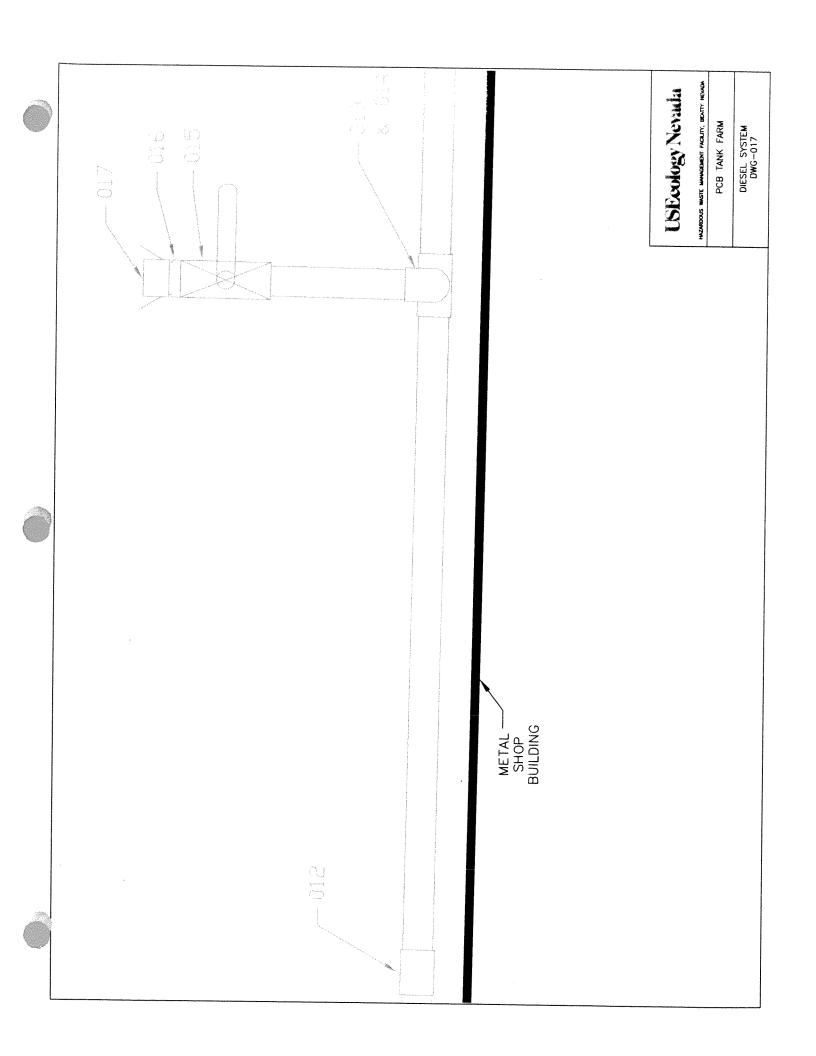


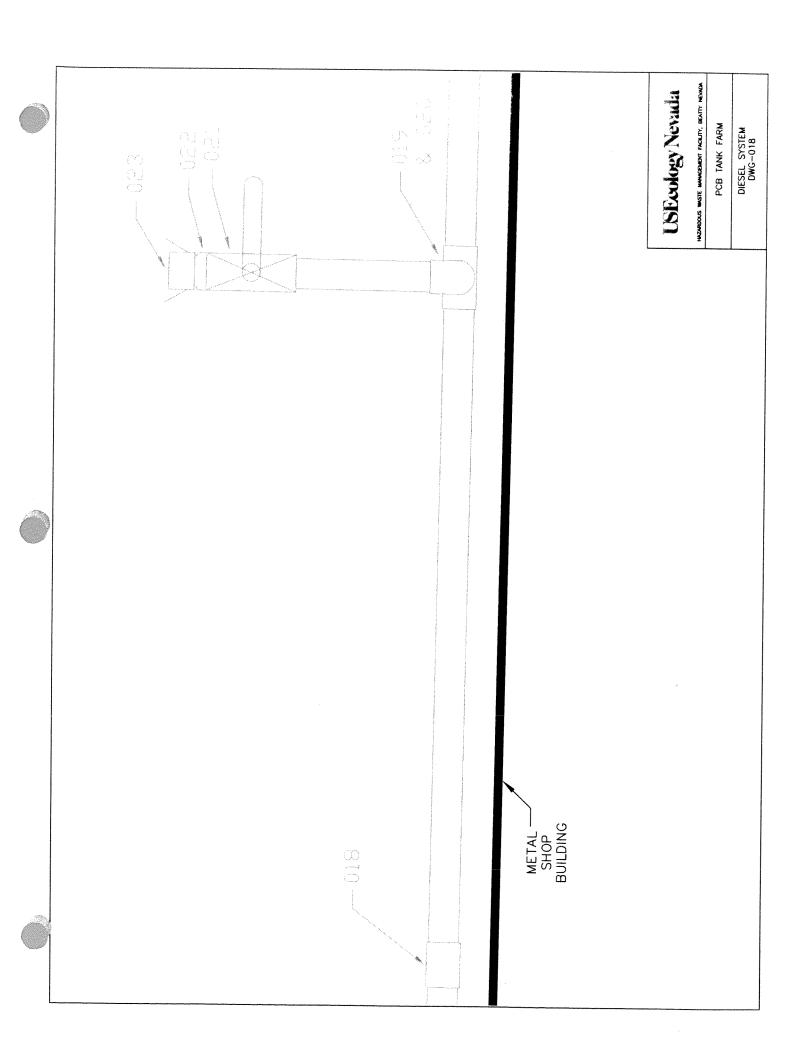


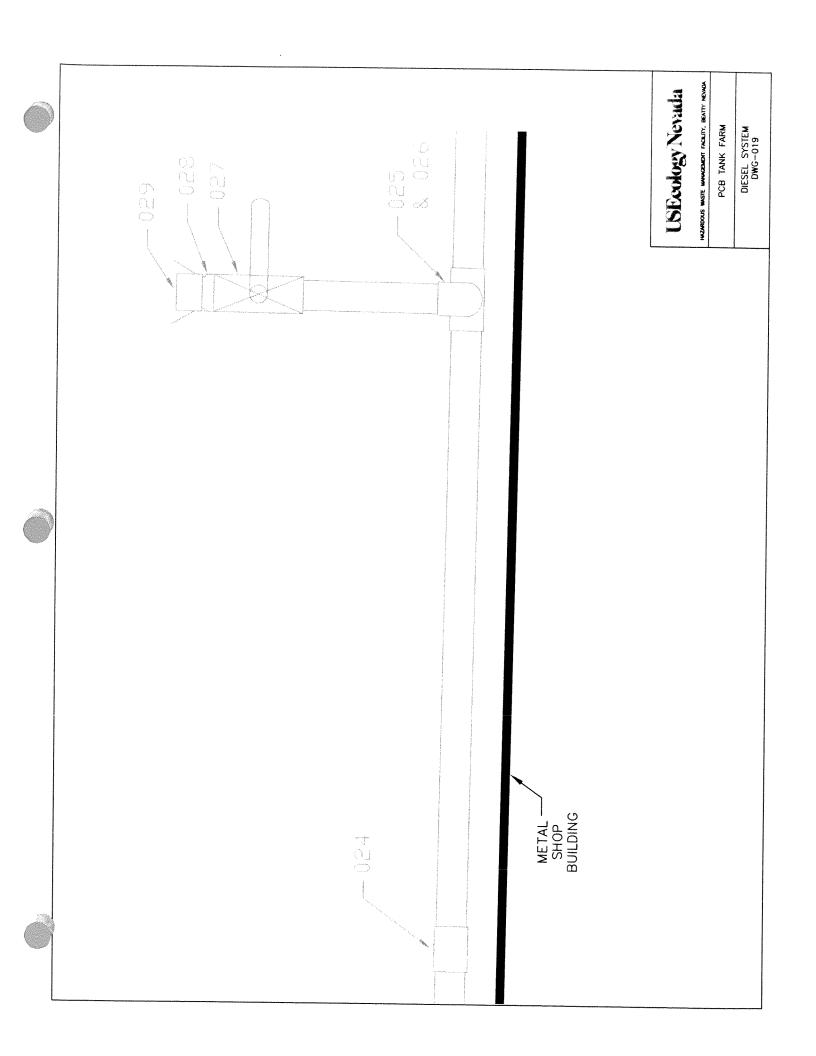


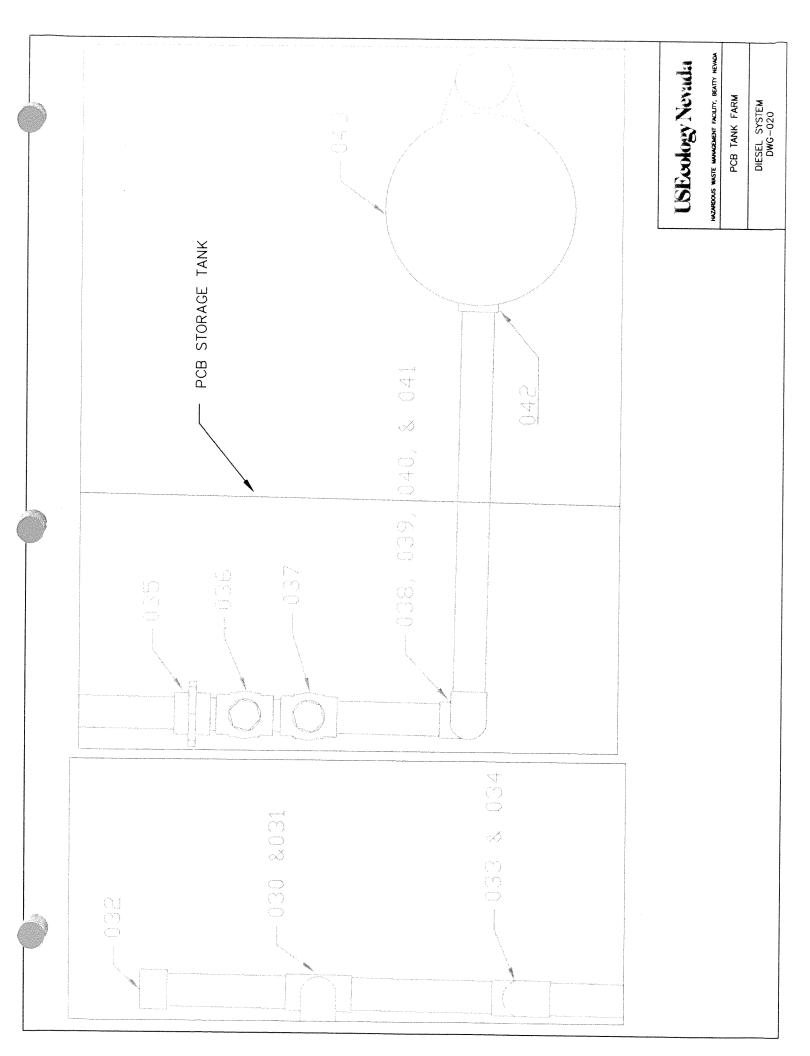


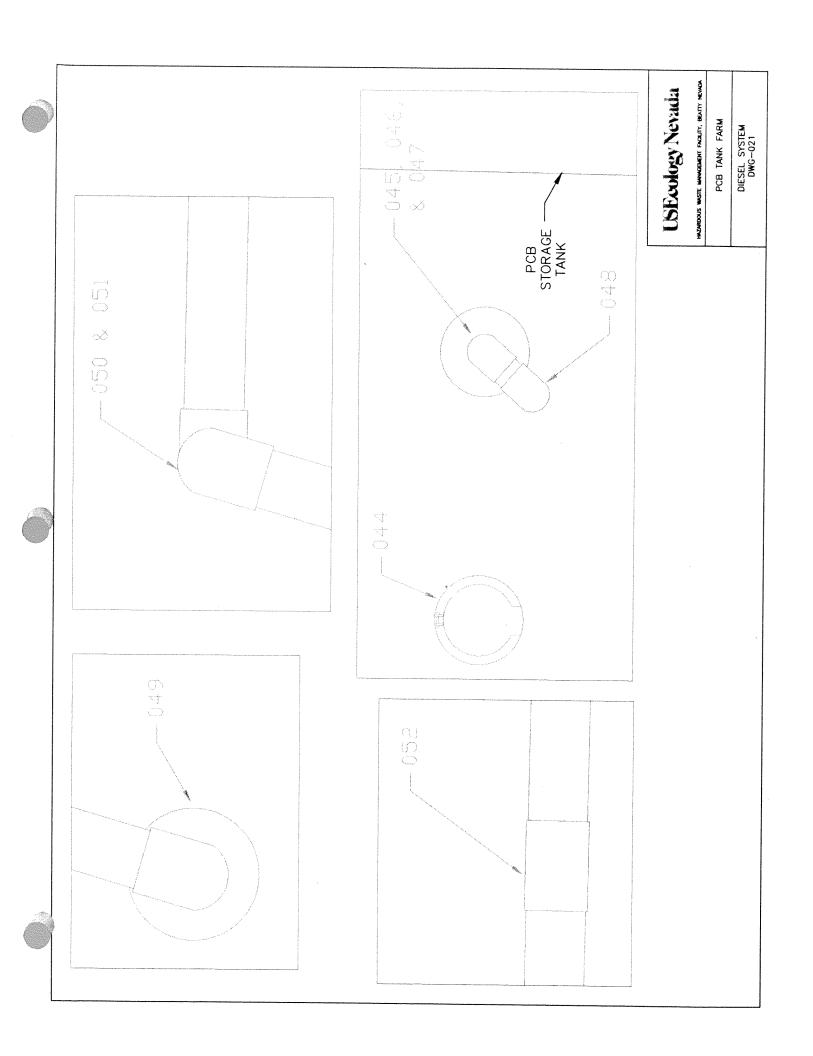


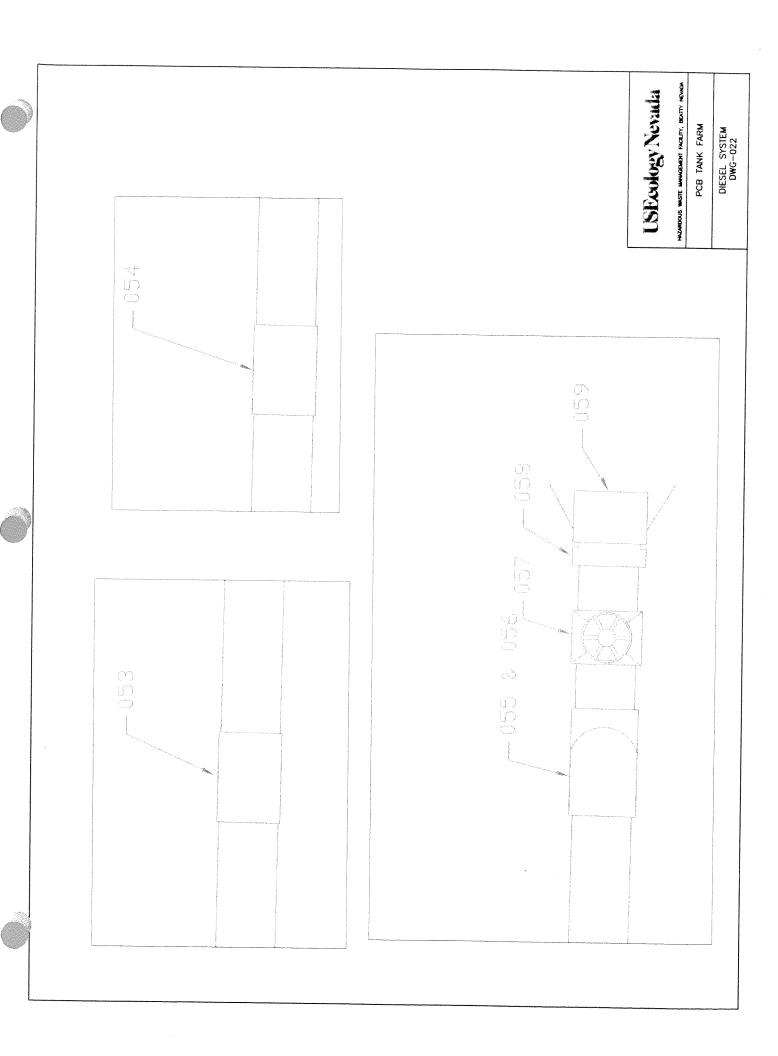


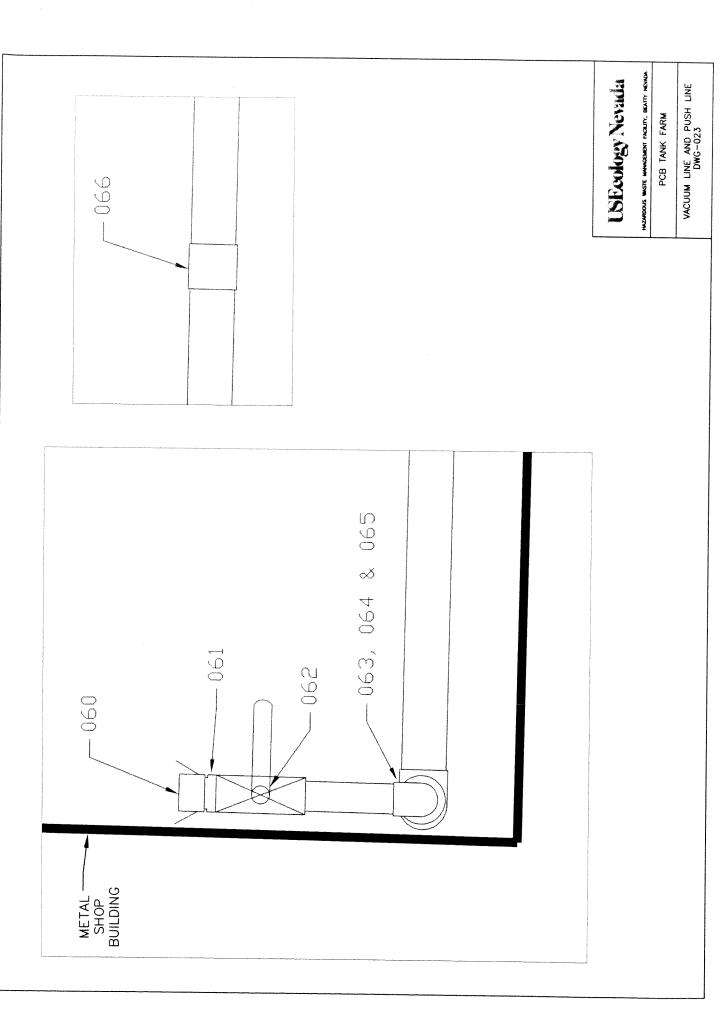


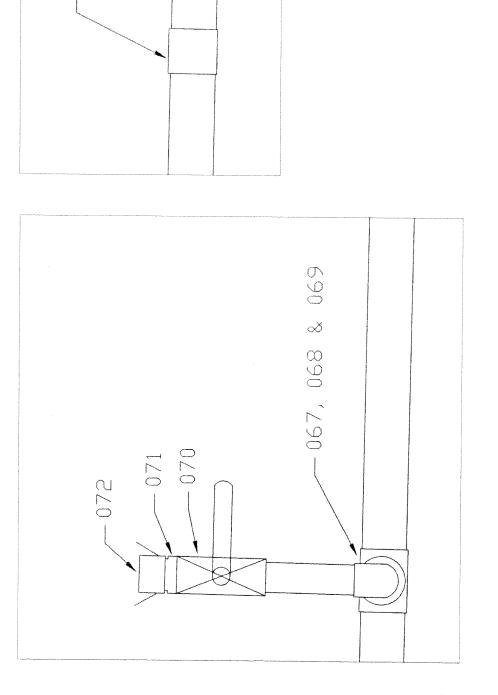








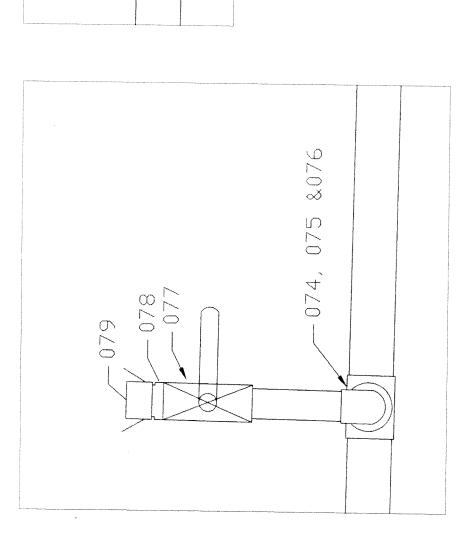




USEcology Nevada

INCHEDOUS WISTE MANACEMENT FACULY, BEATTY NEWAN PCB TANK FARM

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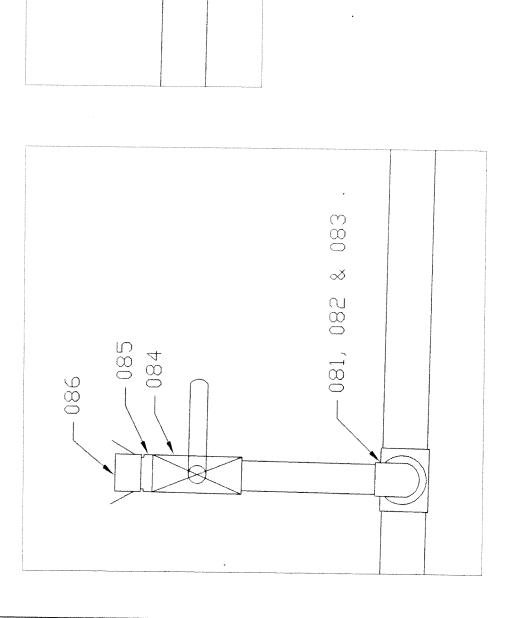


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USEcology Nevada

HAZHOOUS WISTE MANABARRI FACUTY, BEATTY MENABARRI PCB TANK FARM

VACUUM LINE AND PUSH LINE DWG-025

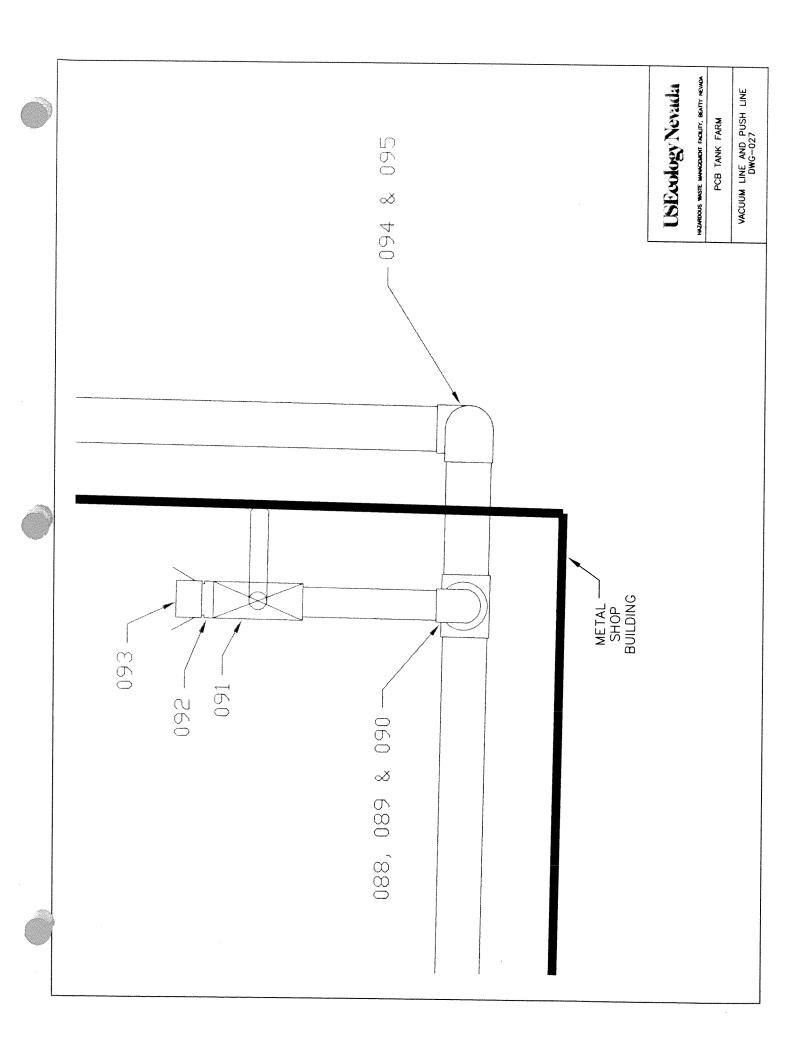


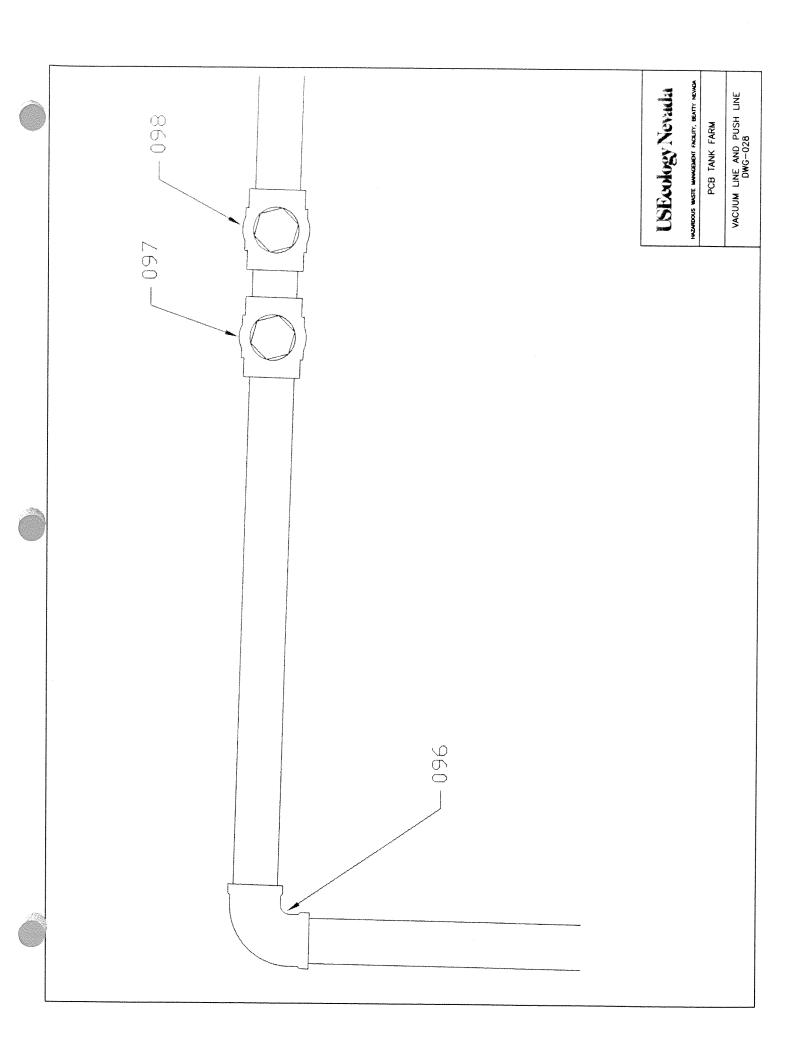
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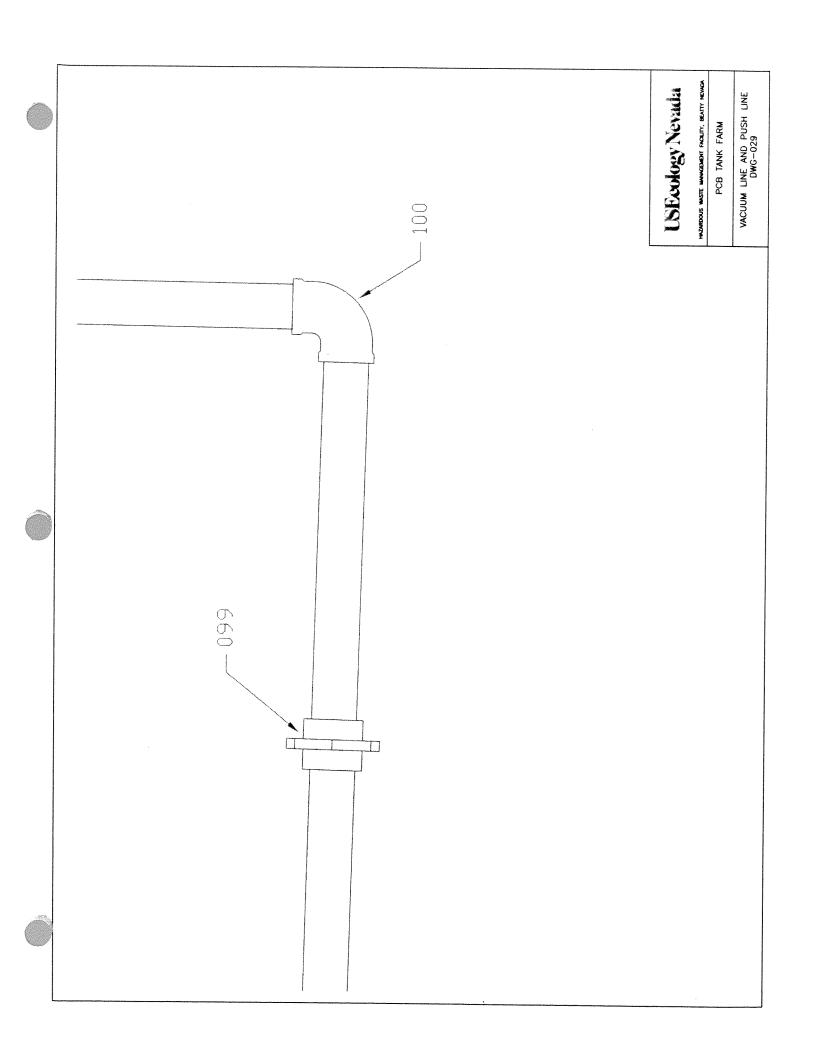
USEcology Nevanta

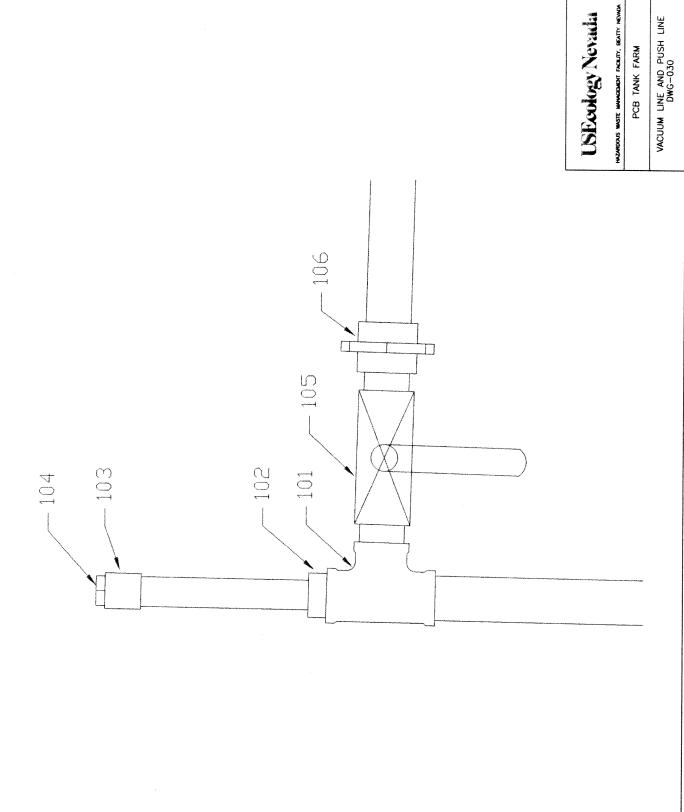
MAZARDOUS WISTE WANAZARDIT FACULIY, BEATITY NEWON PCB TANK FARM

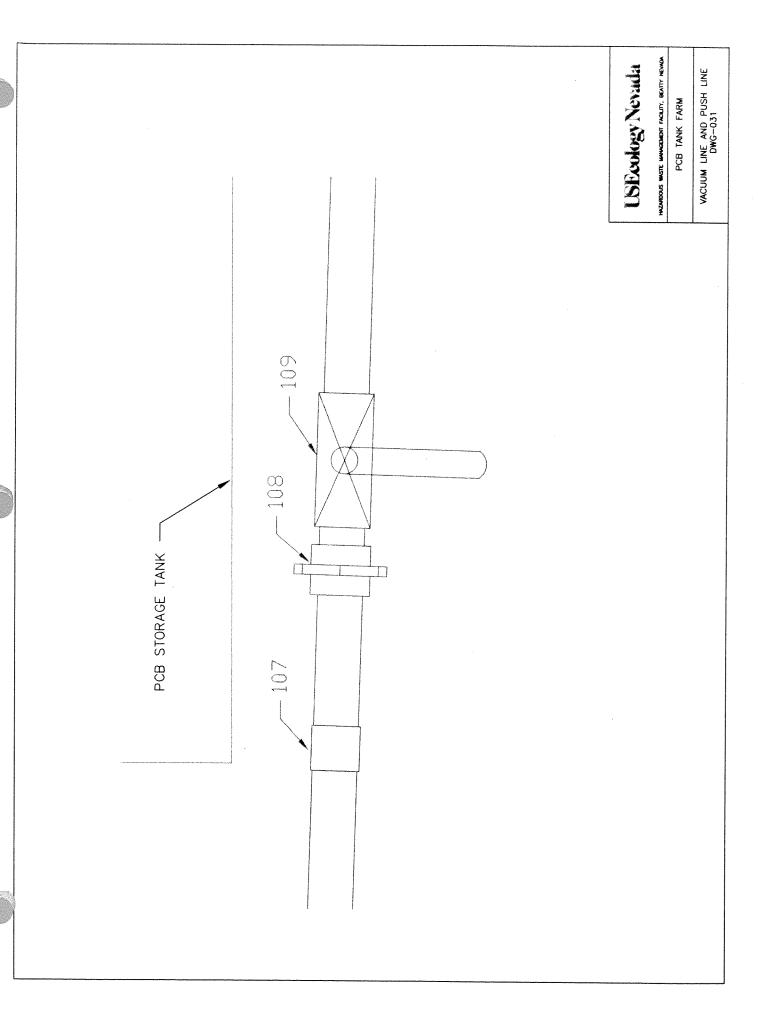
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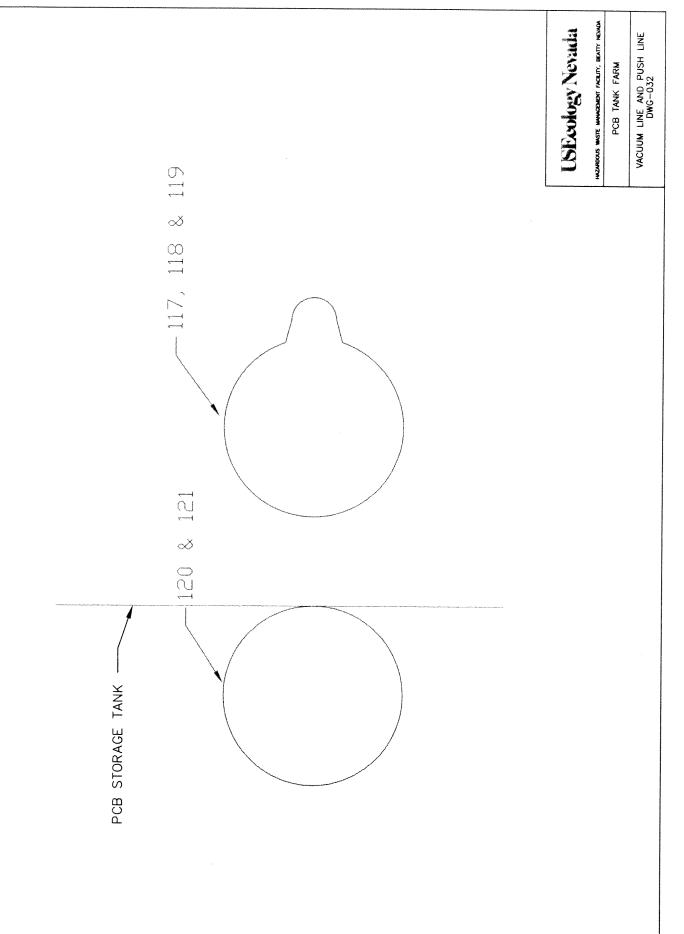


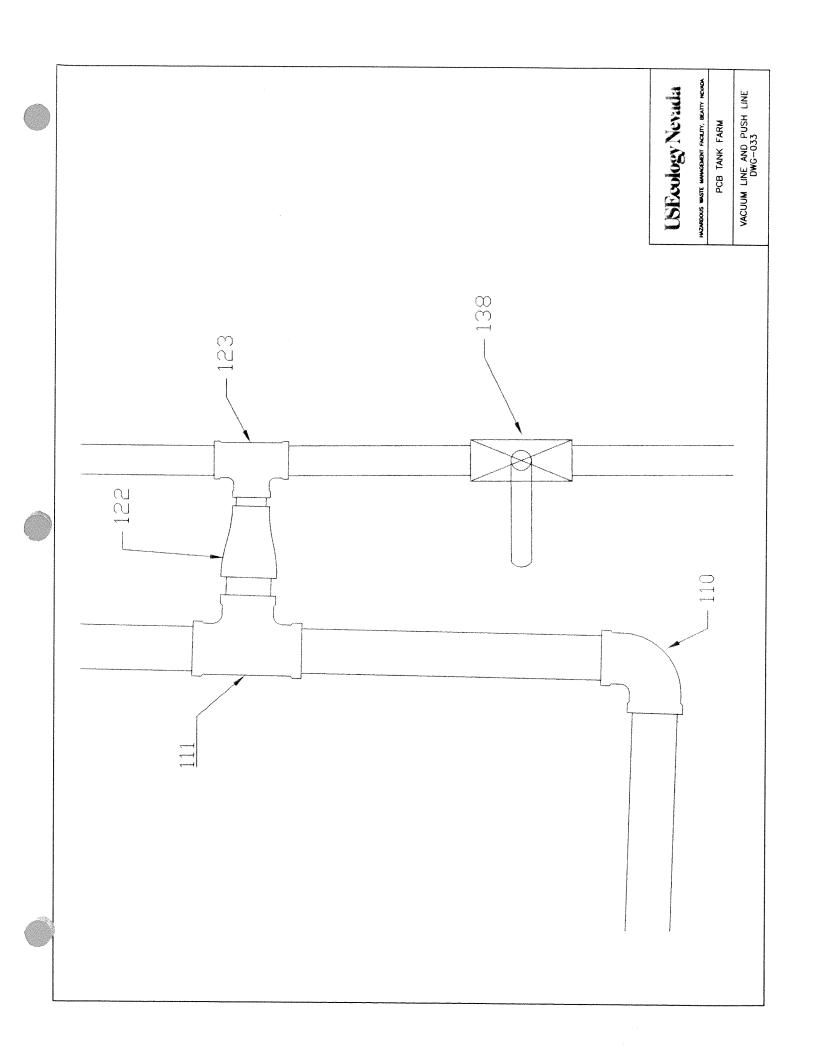


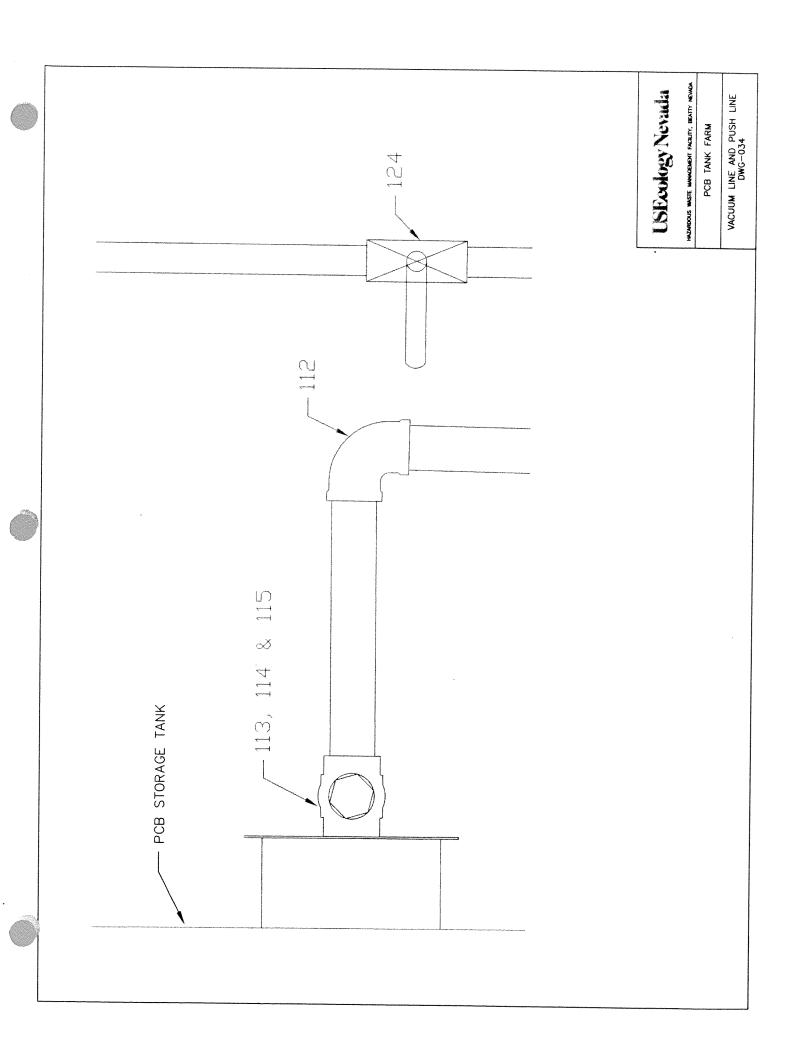




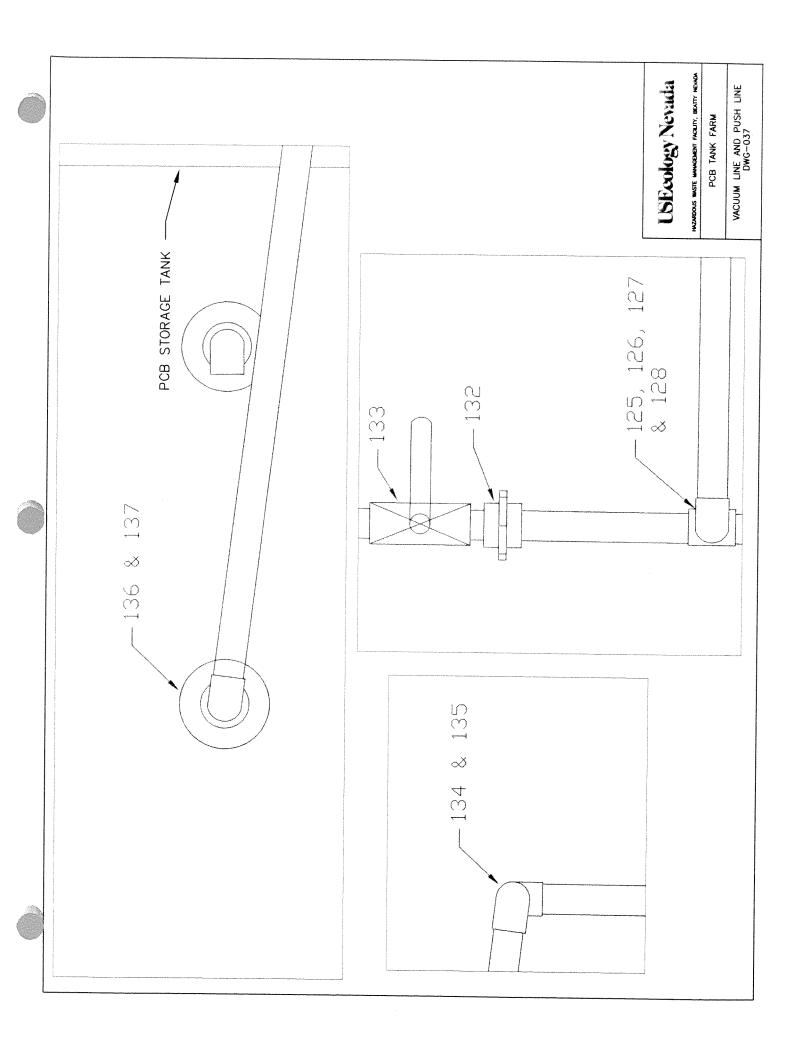


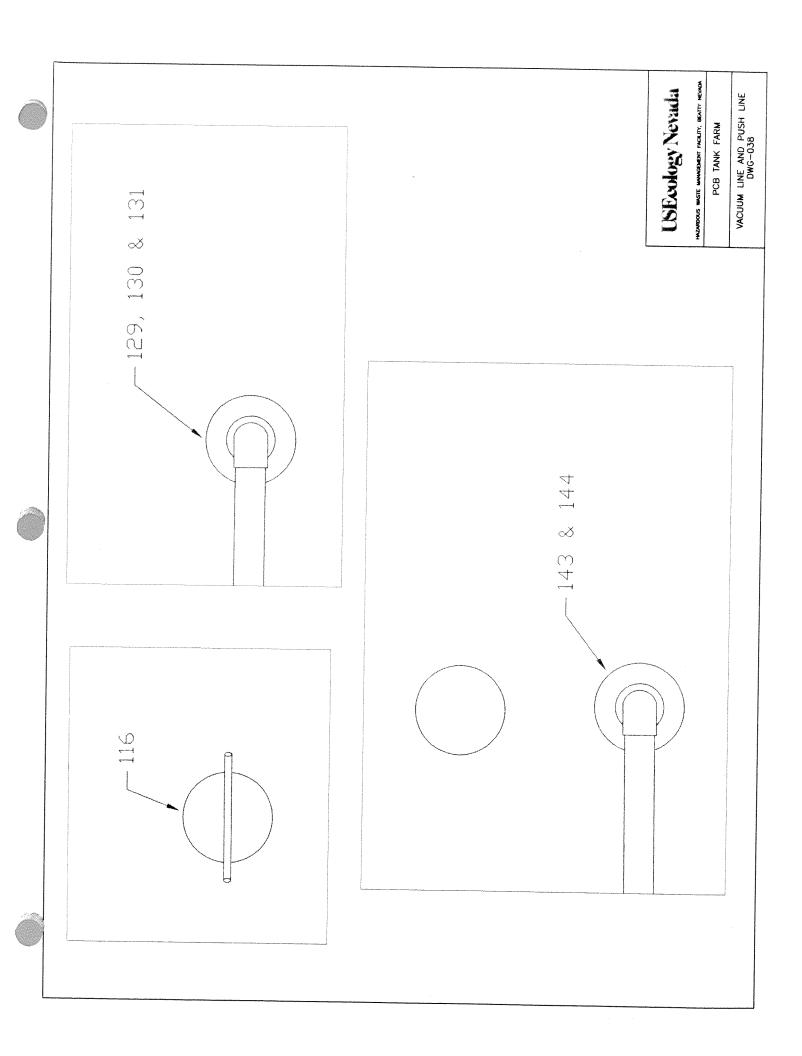


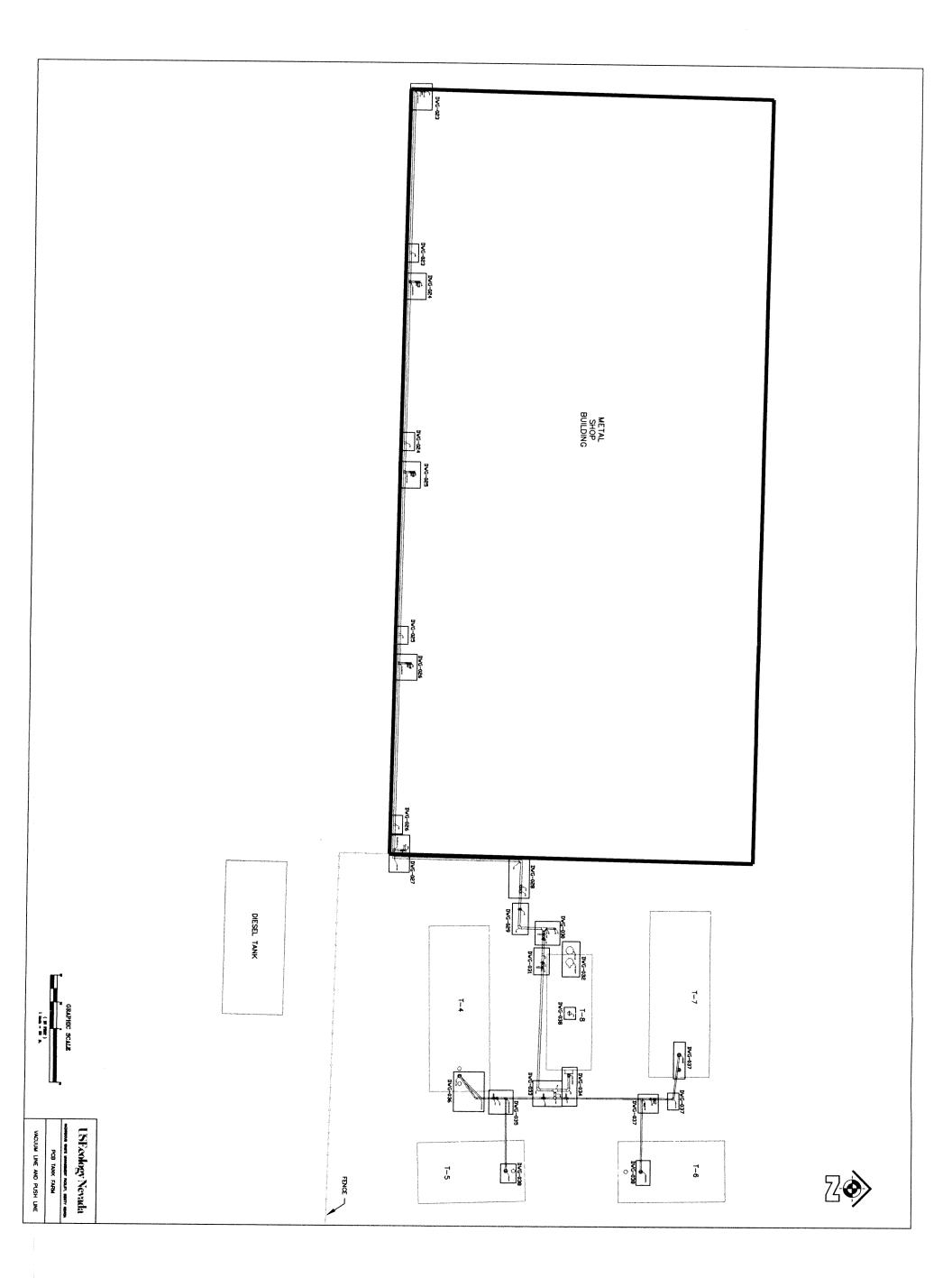


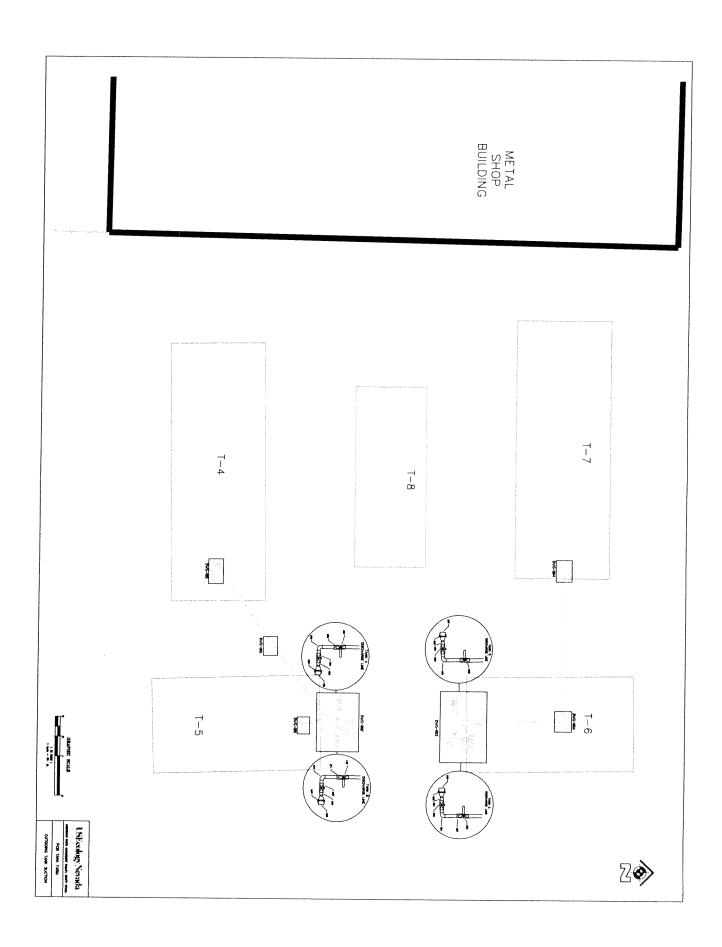


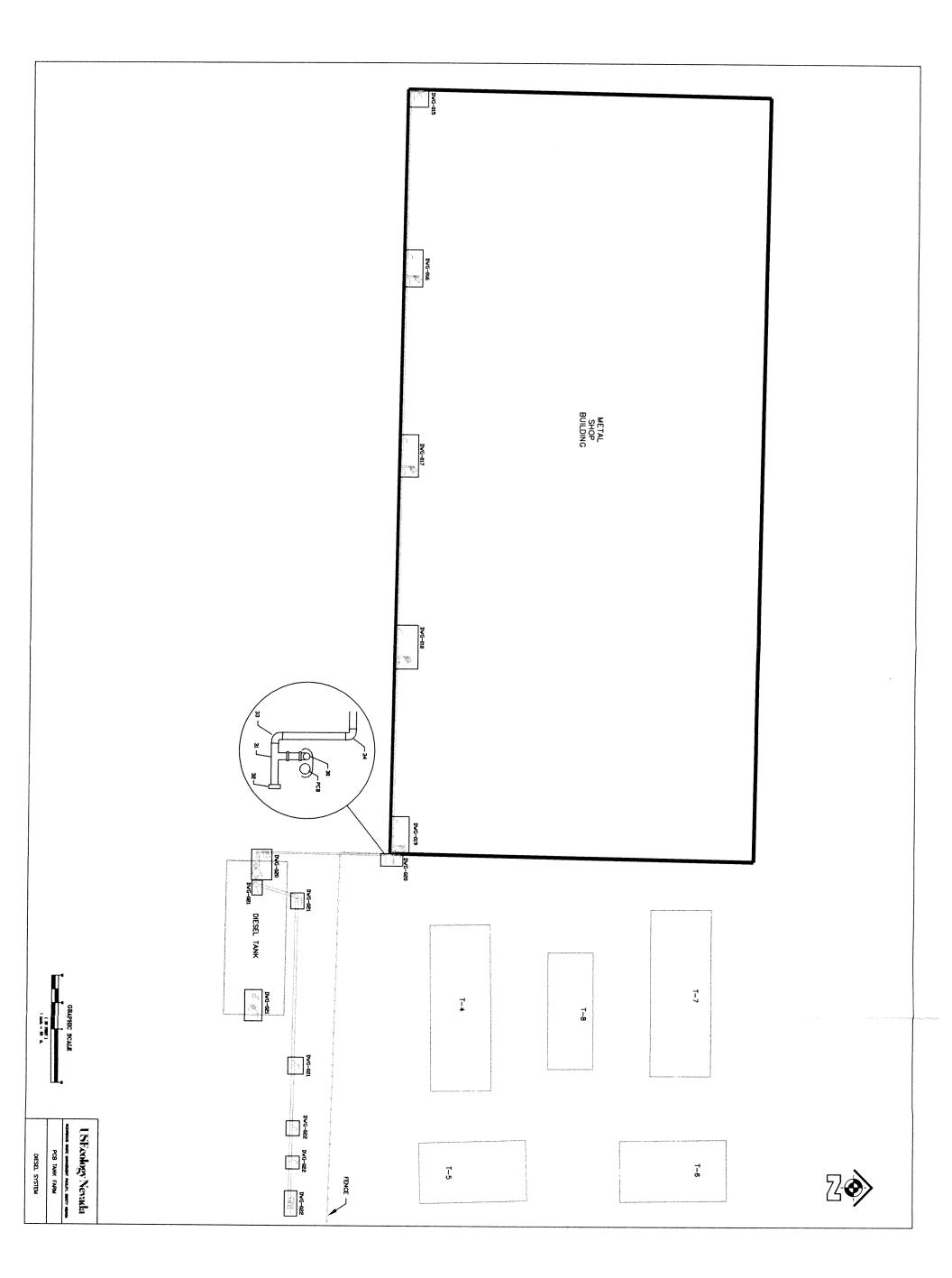
HAZARDOUS WASTE MANAGEMENT FACILITY, BEATTY NEVADA USEcology Nevada VACUUM LINE AND PUSH LINE DWG-035 PCB TANK FARM 1450 CA -139, 140, 141 & 145

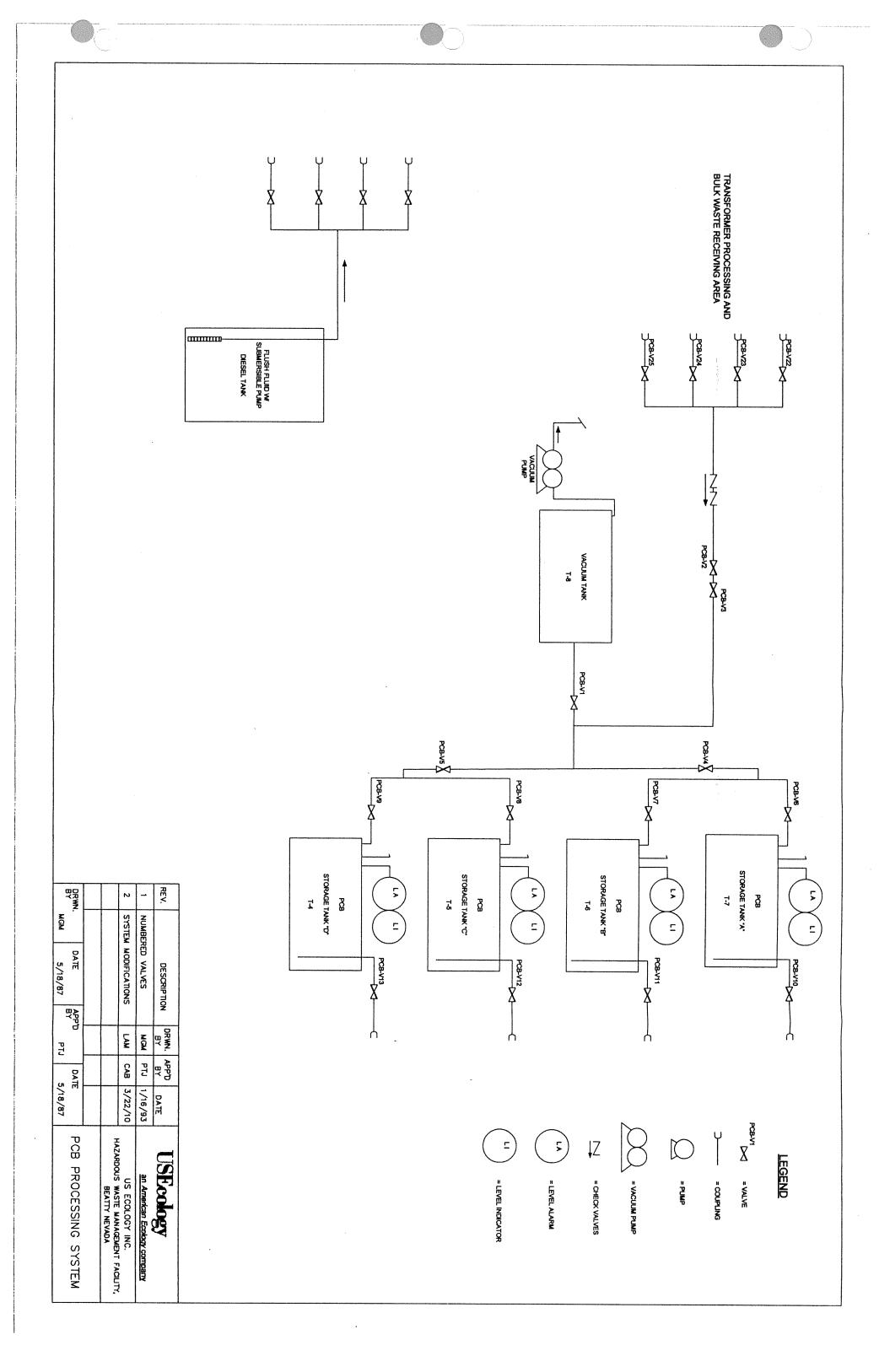


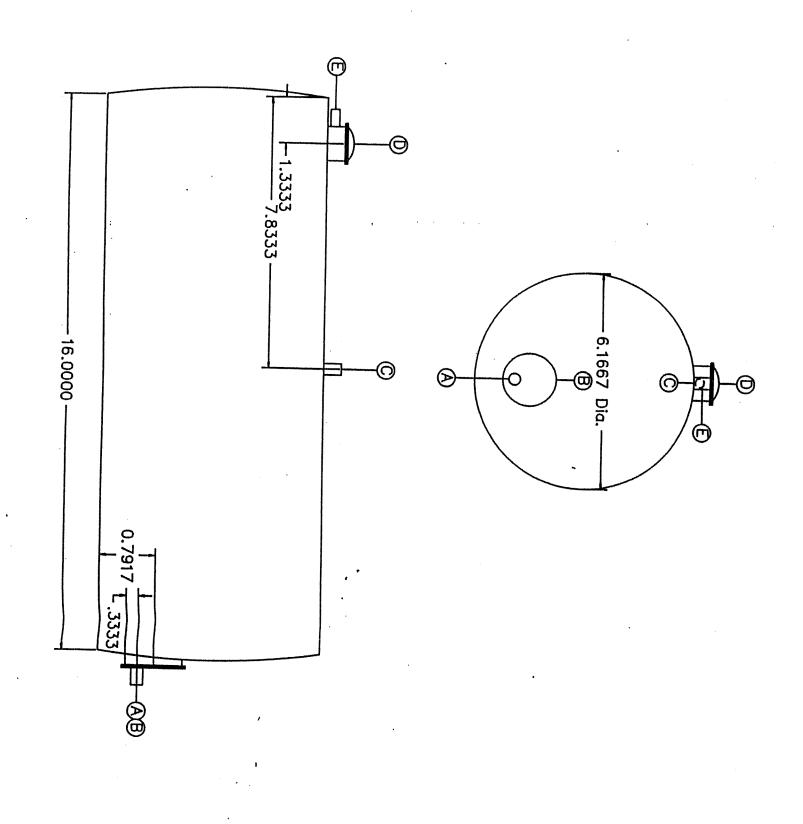






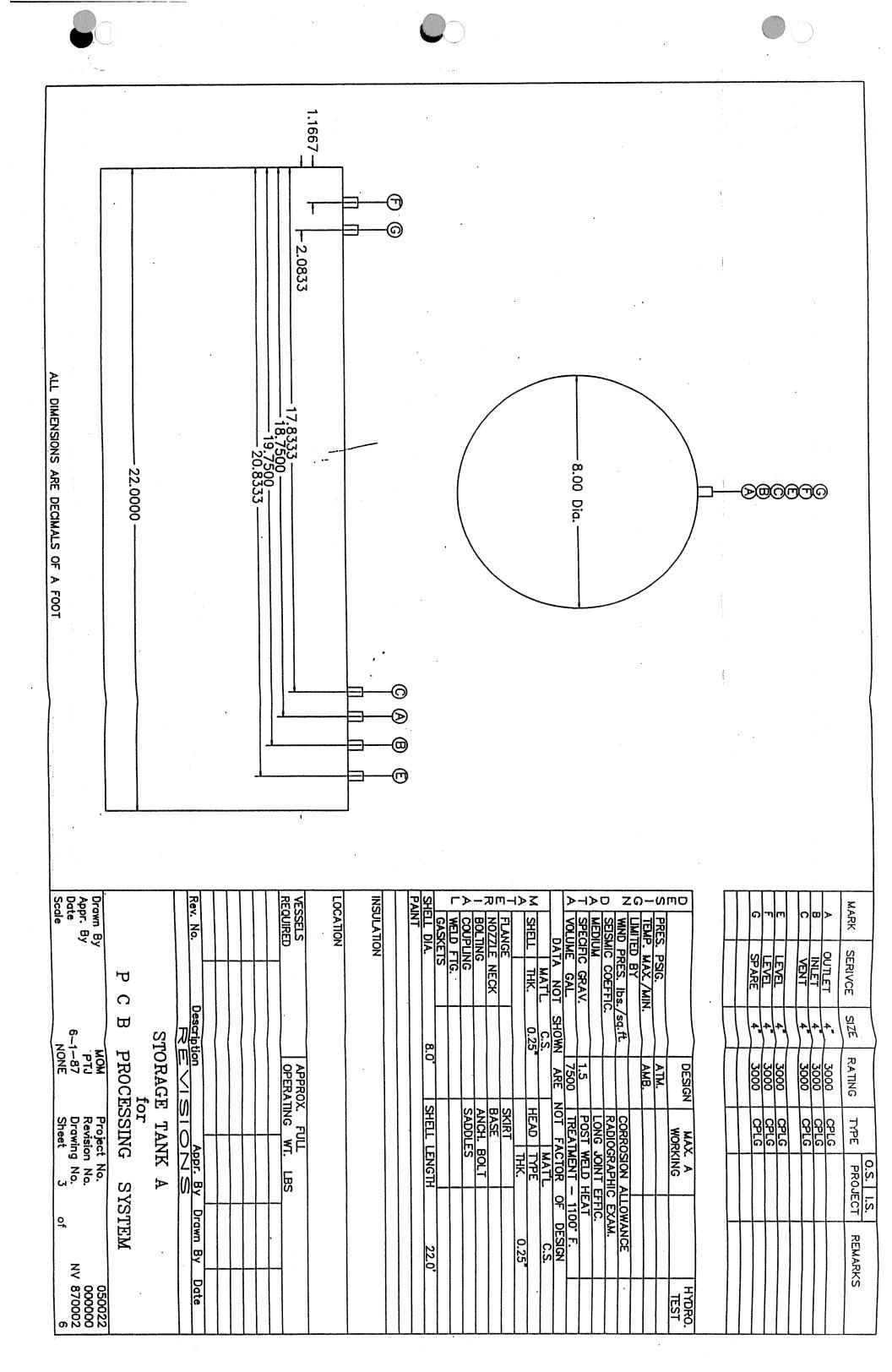


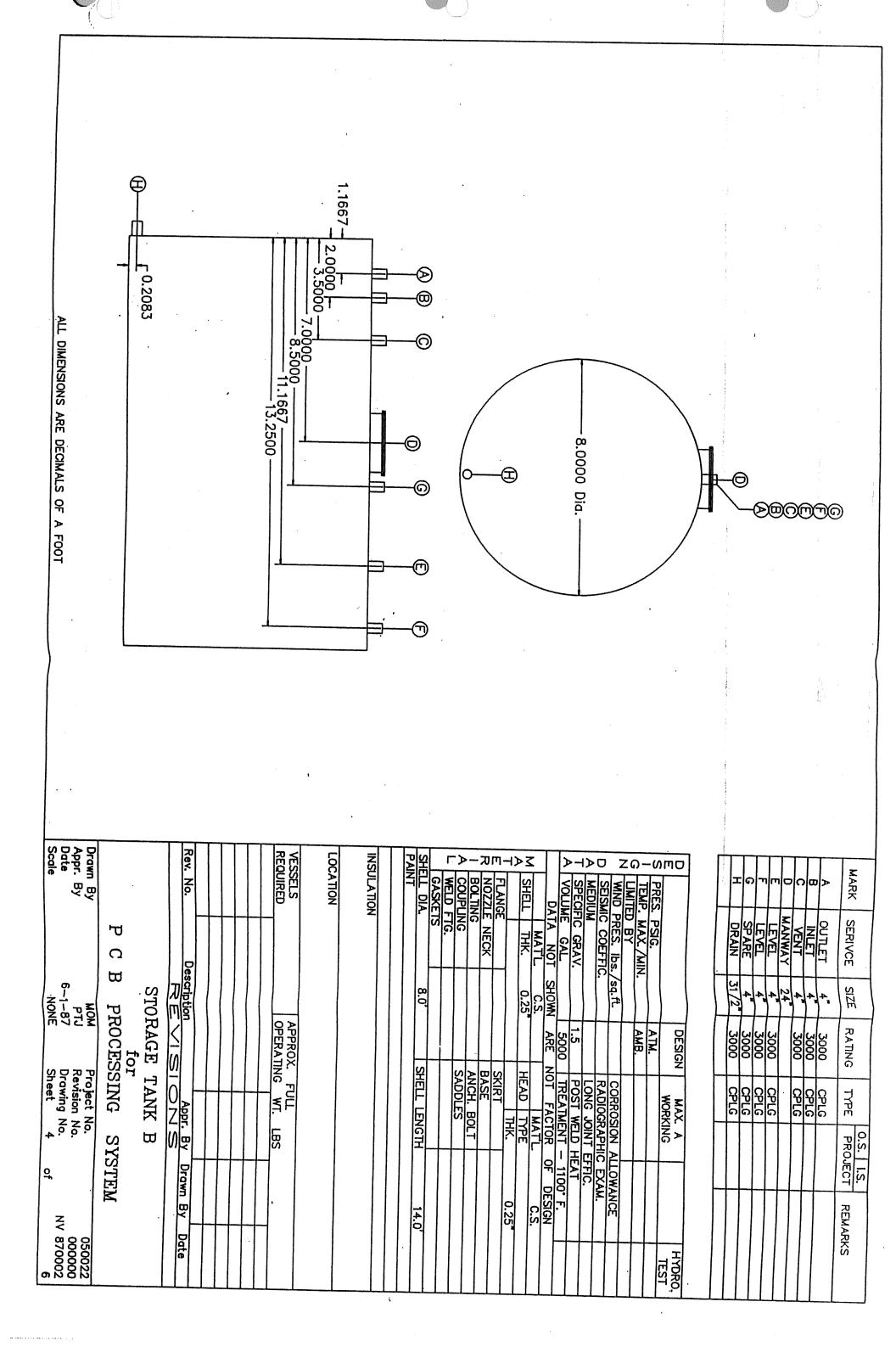


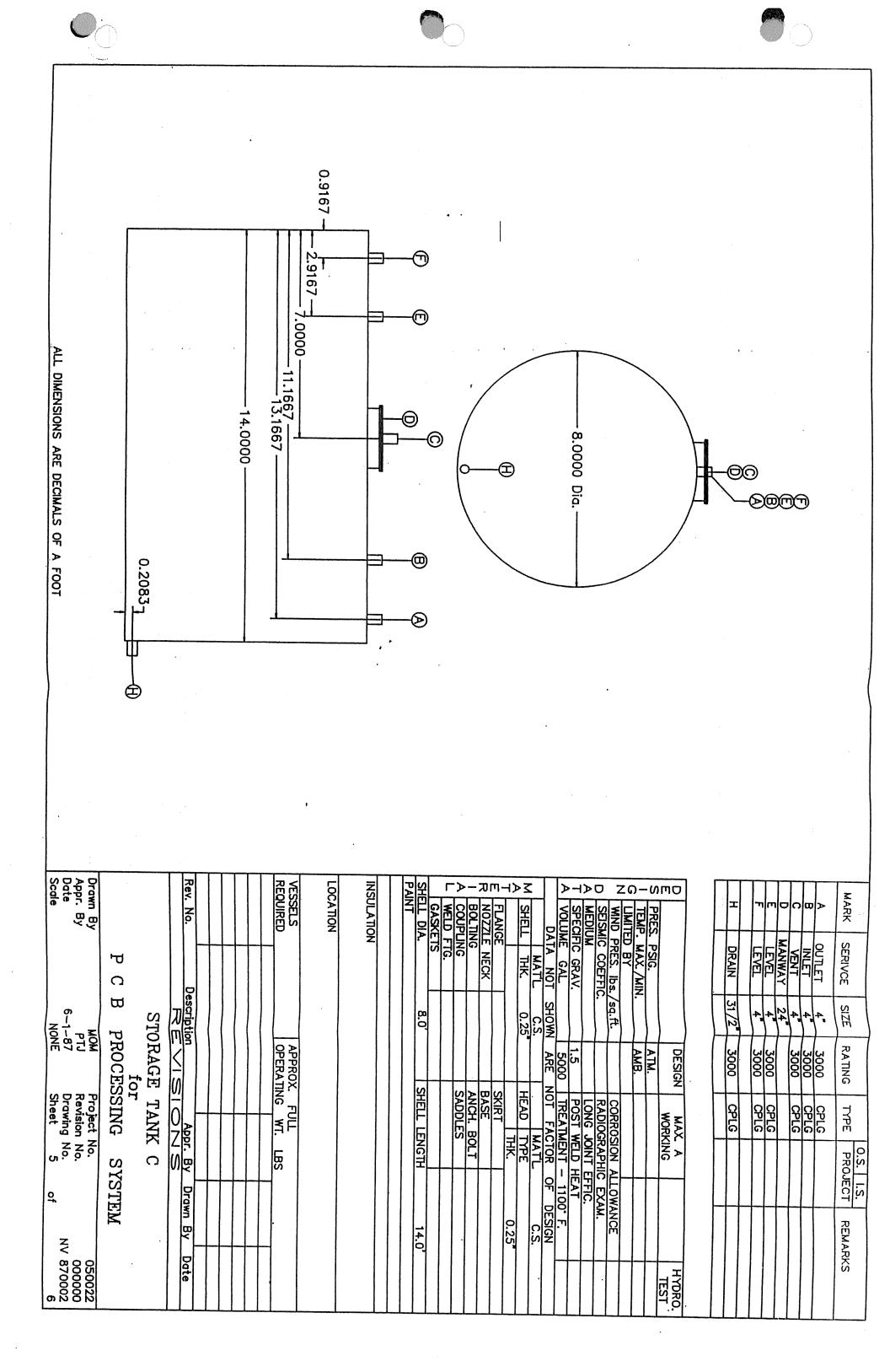


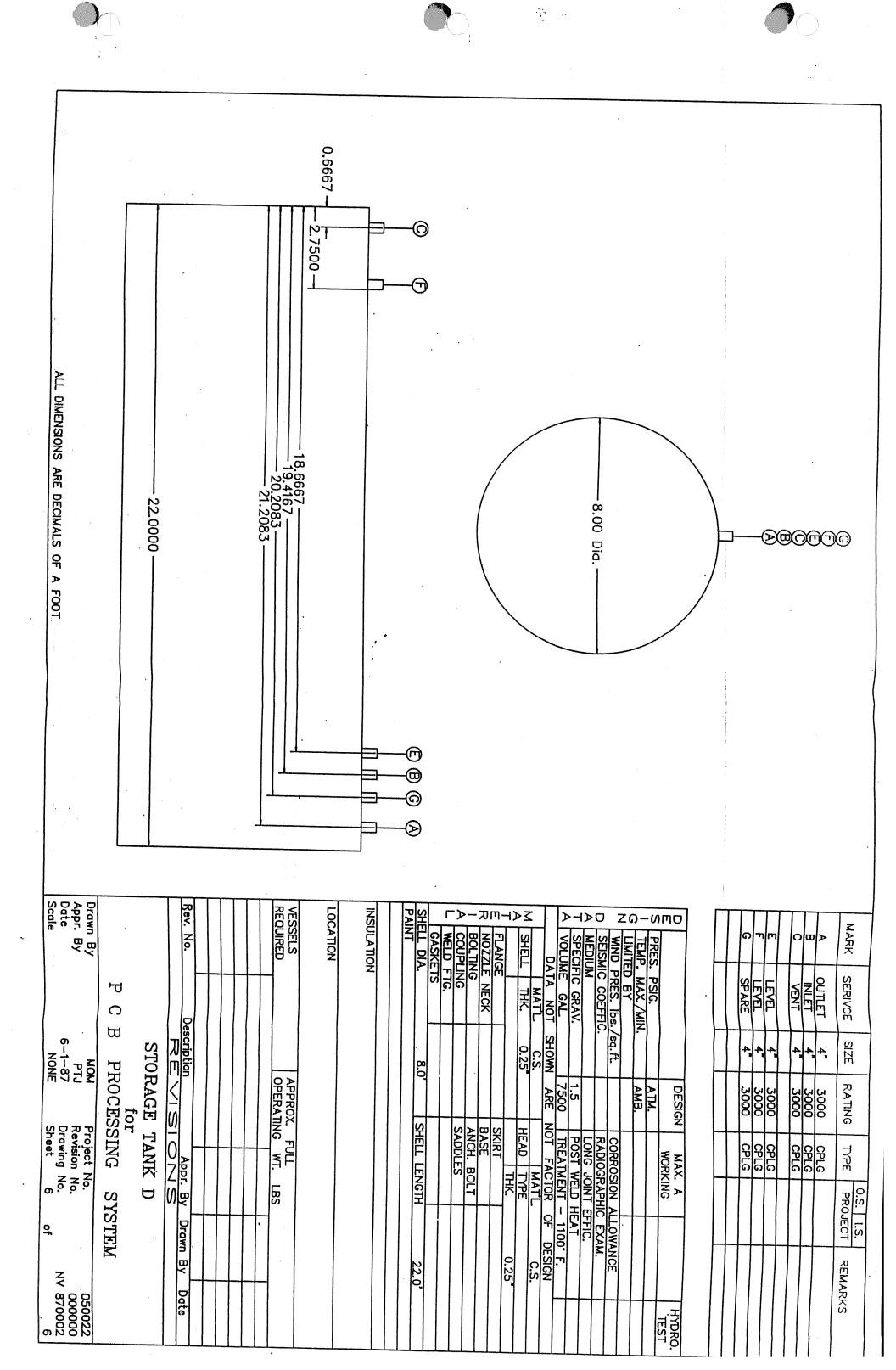
ALL DIMENSIONS ARE DECIMALS OF A FOOT

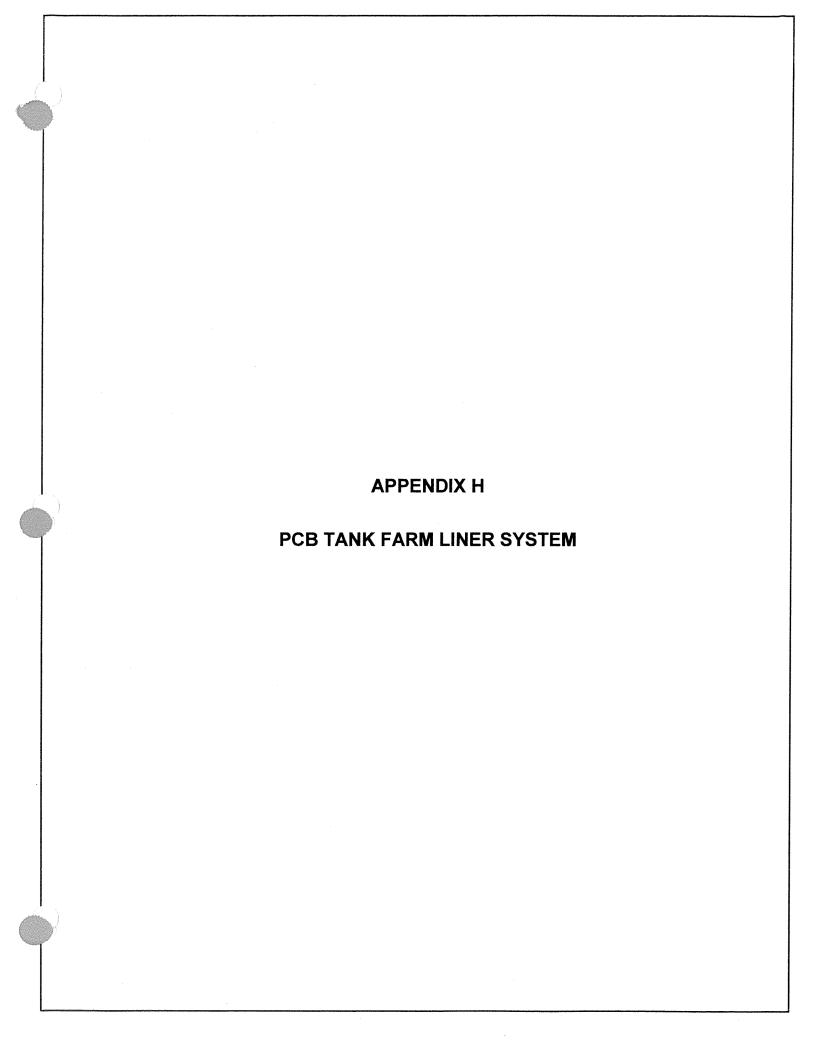
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	P C B	Des					엊 뜻	GAL NOT	S. lbs., COEFFIC	PSIG.		VACUUM	SPARE	IN/OUTLET	SERIVCE
MOM PTJ 6-1-87 NONE	VA PF	Description TX				6.1667'	0.25	SHOWN	/sq.ft			الما		4 [0	SIZE
	VACUUM TAN for PROCESSING		APPROX. F					1.5 3000 ARE		DESIGN FULL VA AMB.			3000	3000	RATING
Project No. Revision No Drawing No. Sheet	TANK SING	SI Appr. By	FULL WI.			SADDLES SHELL LEN	HEAD TYPE THK. SKIRT BASE	POST WITH TACK	CORROS	N MAX. A WORKING			CPLG	CPLG	TYPE
No. No. of	SYSTEM	. By Drawn	BS			ES ES		POST WELD HEAT TREATMENT - 1100 F. NOT FACTOR OF DESIGN	SAPHIC EXAPHIC	A ING					PROJECT
050022 000000 NV 870002 6	K.	m By Date				16.0*	0.25*	AT 1100° F. F DESIGN	ANCE	HYDRO. TEST					REMARKS

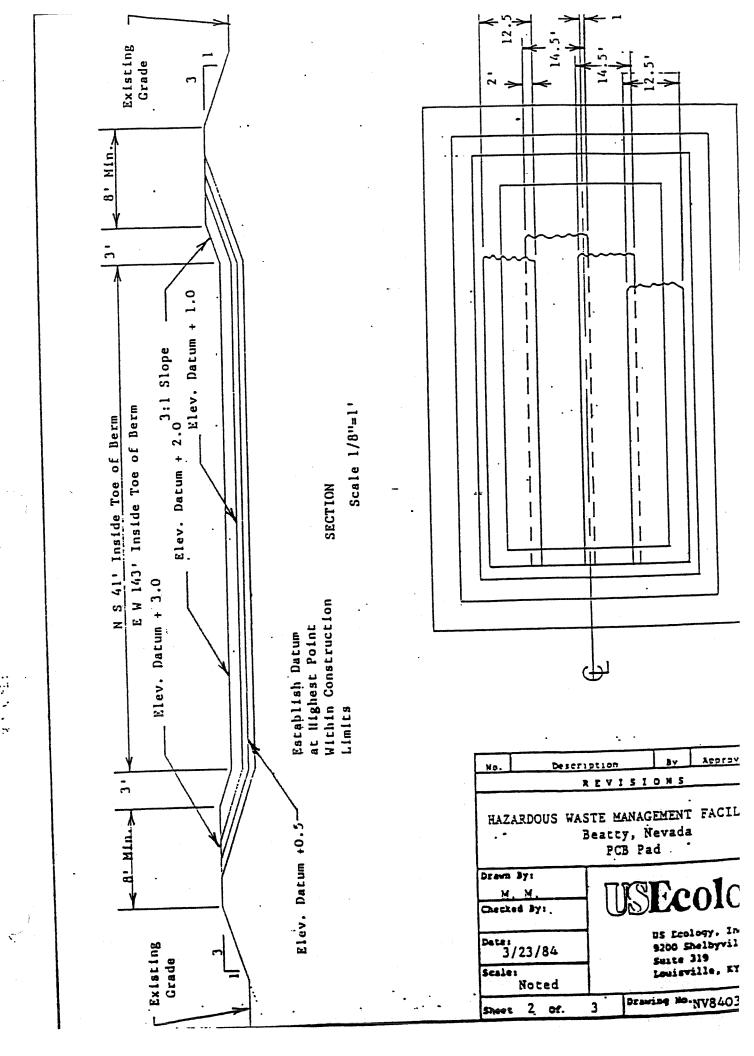


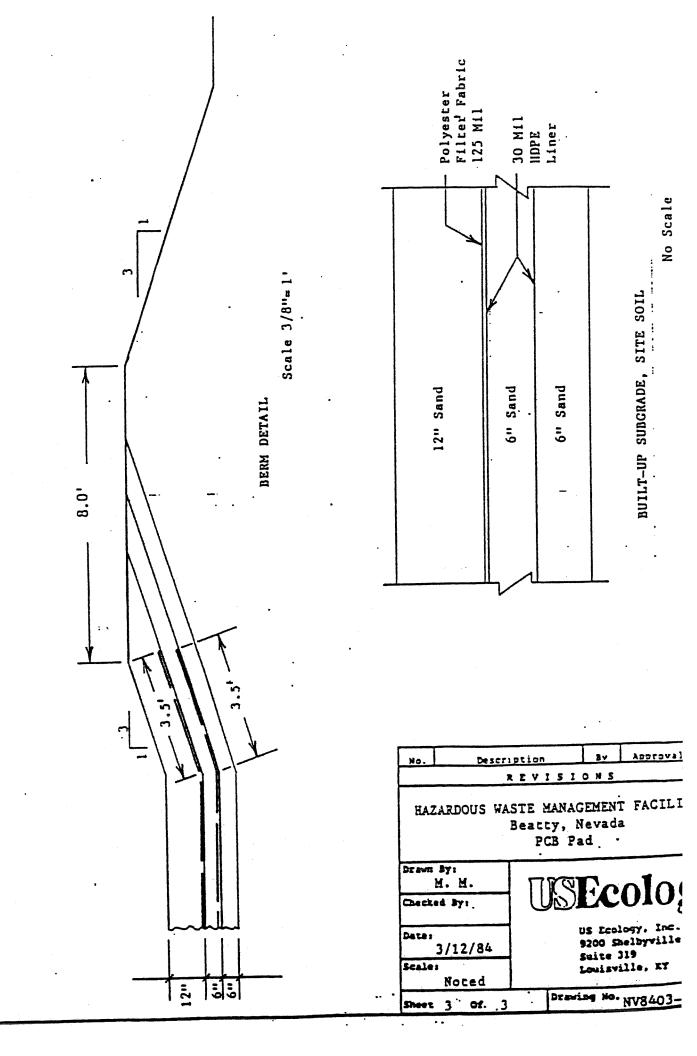


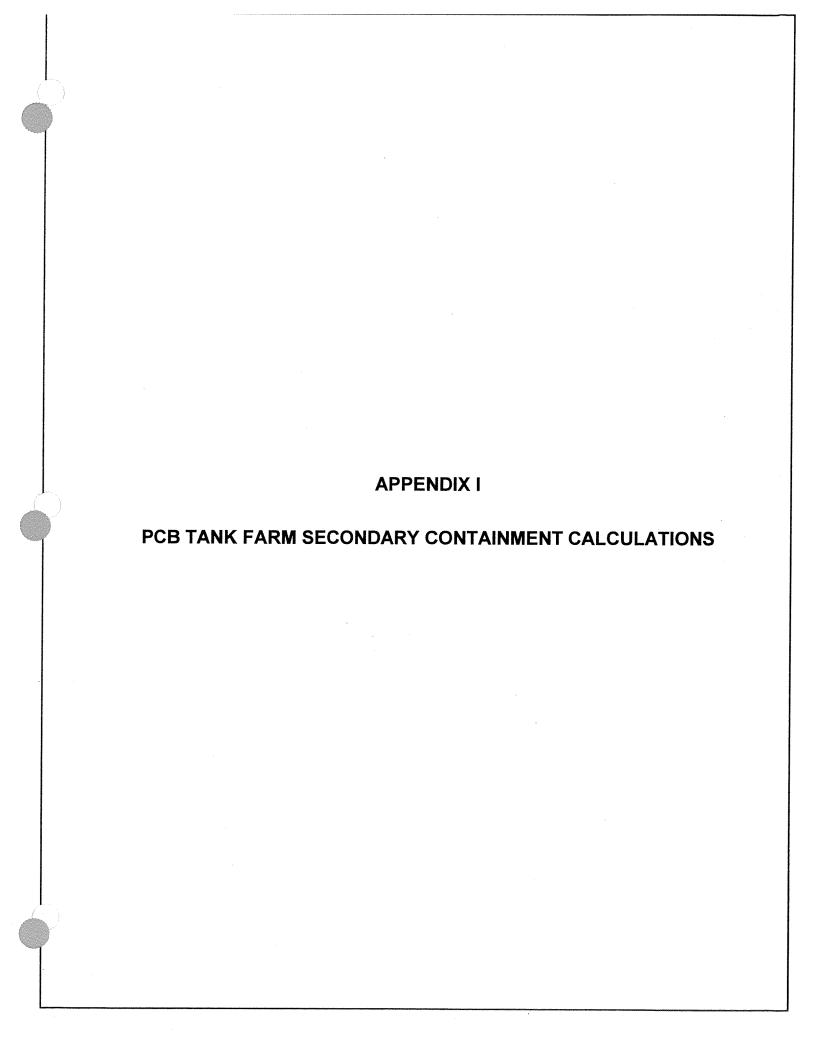












Secondary Containment Calculations

PCB Tank Farm

Tank Volumes:

T-4 = 7,500 gallons

T-5 = 7,500 gallons

T-6 = 5,000 gallons

T-7 = 5,000 gallons

T-8 = 3,000 gallons

Total = 28,000 gallons

Precipitation from 100 year storm = 3 inches

Precipitation Volume = 0.25 ft x 48ft x 48ft x 7.48gal/ft³ = 4,308 gallons

Requirement:

Containment Capacity Required = Twice the Volume of largest tank + Precipitation = 7,500(2) + 4,308 = 19,308 gallons

Containment Capacity Available = (a) volume of air + (b) volume in sand

(a) = 48ft x 48ft x 1.5ft x 7.48gal/ft³ = 25,850 gallons

(b) = 48ft x 48ft x 0.0833ft x 30% (porosity of sand) x 7.48gal/ft³ = 430 gallons (This assumes 1 inch of soil in containment area)

Tank Farm Containment = 26,280 gallons

PCB Storage Area

PCB storage area capacity = 71,816 gallons

Requirement:

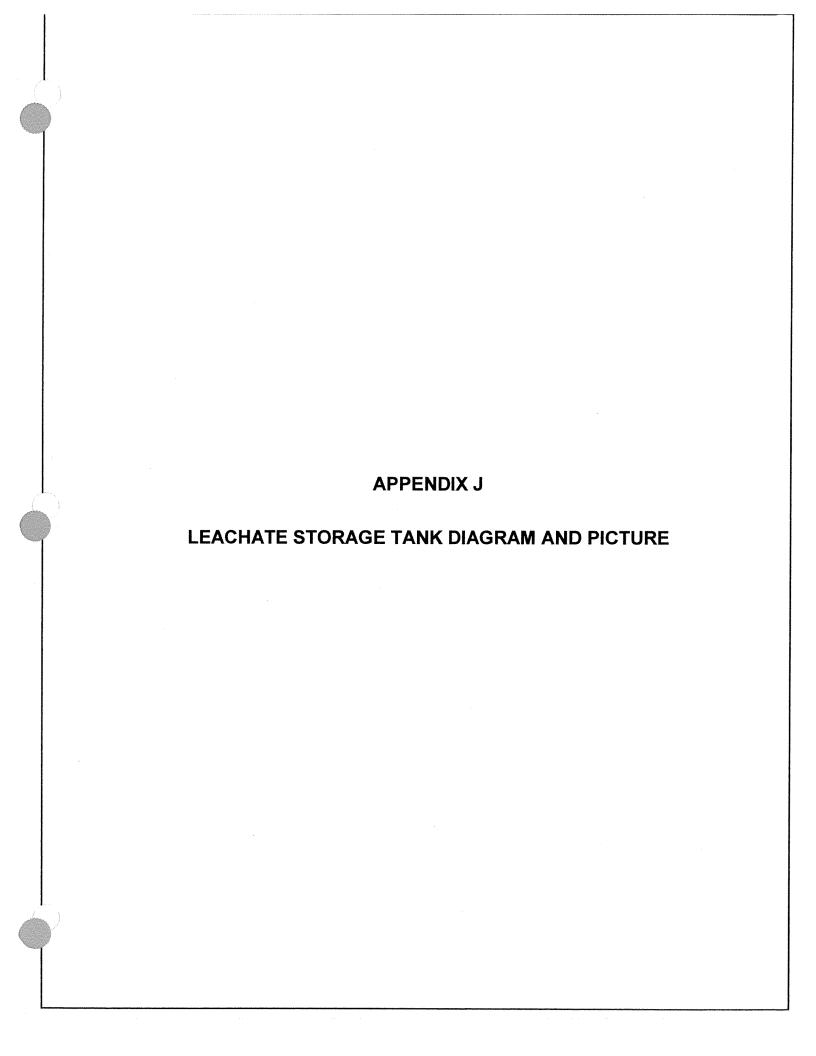
25% of the total capacity <u>or</u> twice the volume of the largest container. <u>Whichever is greater</u>. (Precipitation is not taken into consideration since the building in enclosed)

25% of the total capacity = 71,816 gallons x 0.25 = 17,954 gallons

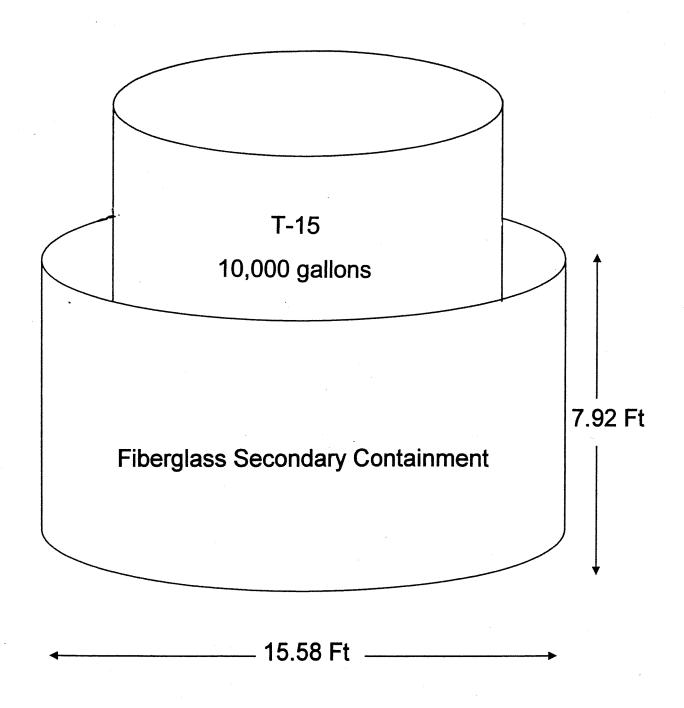
or

Vol of largest container = 115 gallons

Containment Capacity Available = $48 \text{ft} \times 100 \text{ft} \times 0.5 \text{ft} \times 7.48 \text{gal/ft}^3 = \boxed{17,954 \text{ gallons}}$

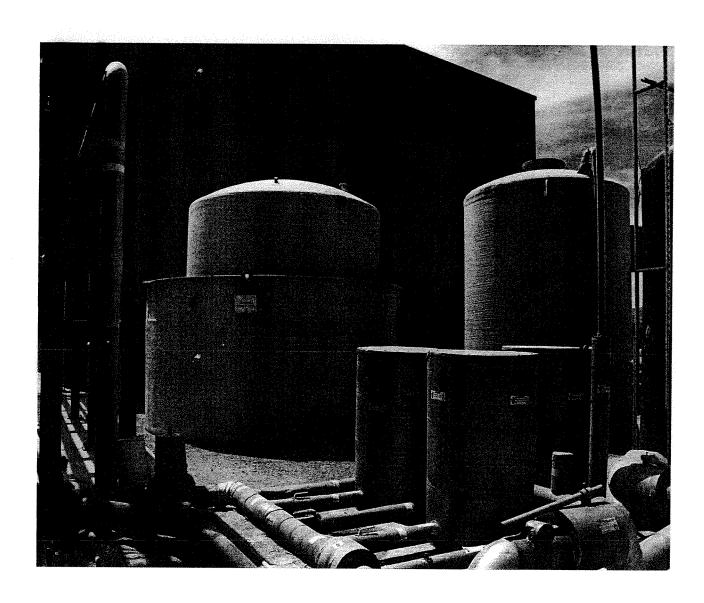


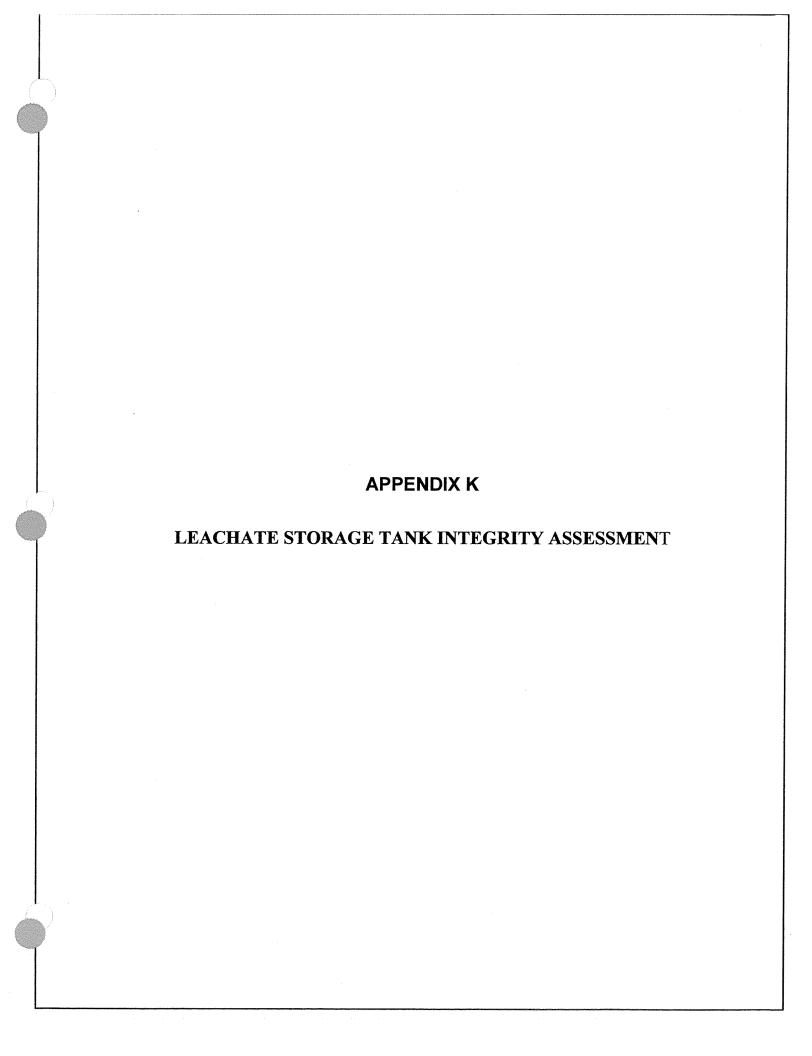
T-15 Leachate Storage



US Ecology Nevada March 2010

T-15 Leachate Storage Tank





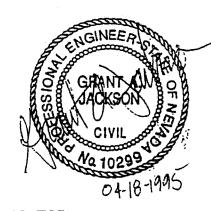
ENGINEERING CERTIFICATION

LEACHATE STORAGE TANK

U.S. ECOLOGY, INC. BEATTY, NEVADA

April 1995

Revision 0



Prepared By

NAISMITH ENGINEERING, INC. ENGINEERING • ENVIRONMENTAL • SURVEYING CORPUS CHRISTI, TEXAS

NEI PROJECT NO. 4383

TABLE OF CONTENTS

1.	1.1.	ERAL							 						• •	٠	- 1 - 1
	1.2.	Facility Desc															•
-2	INTE	GRITY ASS															- 2
	2.1.	Design Stan	dards						 							•	- 2
	2.2.	Structural St	rength/Ir	tegrity	·				 							•	- 2
•~	2.3.	Compatibilit	y With V	Wastes					 								- 2
	2.4.	Corrosion P	rotection						 								- 3
	2.5.	Inspection/T	esting .						 							•	- 3
3.	CER	TIFICATION	Ī						 	••	.	••		٠.			- 3
REF	EREN	CES				•••	• • •		 			••	• •			. . .	- 5
APP	ENDIC	ES															
	APP APP	ENDIX A ENDIX B ENDIX C	STOI	LOCARAGE	TAN MENI	K DA	ATA STE	M		ME	CA	TC	:U	$\mathbf{L}A$	·ΤΙ	101	NS

1. GENERAL:

man man territoria

- 1.1. Introduction: Naismith Engineering, Inc., (NEI) was retained by U.S. Ecology, Inc., (USE) to provide an integrity assessment for the Leachate Storage Tank located at the U.S. Ecology, Inc., facility near Beatty, Nevada. Facility operations are governed by two (2) separate authorizations. The facility is authorized to manage hazardous wastes regulated by the Resource Conservation and Recovery Act (RCRA) under a permit (Permit No. NEV-HW002) issued by the Nevada Department of Conservation and Natural Resources, Division of Environmental Protection (NDEP). The facility is also authorized to manage toxic-substances regulated by the Toxic Substances Control Act (TSCA) under an approval issued by the U.S. Environmental Protection Agency, (EPA) Region IX. This assessment conforms with the requirements of the EPA as outlined in Title 40, Code of Federal Regulations (CFR), Part 264, Subpart J, "Tank Systems".
- 1..2. Facility Description: The hazardous waste storage tank being assessed is a ten thousand (10,000) gallon aboveground fiber reinforced plastic (FRP) tank. The tank will be used to store leachate gathered from the hazardous waste landfill at the facility. The tank is installed inside a FRP secondary containment tank unit. The tank system is supported on a reinforced concrete foundation. The location of the storage tank within the facility is illustrated on the location map in Appendix A.
 - 1..2..1. Storage Tank: The Leachate Storage Tank has a diameter of approximately twelve (12) feet and a shell height of approximately twelve (12) feet. An adequate number of fittings are installed on the tank to allow it to be properly operated and monitored. The tank is furnished with one (1) twenty-two (22) inch diameter manhole on the roof. Design information for the tank is included in Appendix B.

In order to prevent accidental overfill, the Leachate Storage Tank is furnished with a high level sensor connected to a visible alarm located adjacent to the tank fill connection. The alarm is set to turn on when liquid in the tank reaches a level of eleven (11) feet (approximately ninety two percent [92%] of its maximum volume). The level in the tank is also measured using a portable liquid level indicator prior to placing any material into the tank. The liquid level in the tank is monitored by plant personnel during the filling operation.

The controlling specification for the fabrication of this tank is ASTM D3299 for filament wound FRP tanks.

1..2..2. Secondary Containment: The storage tank is located within a circular secondary containment open-top tank approximately sixteen (16) feet in diameter and eight (8) feet in height. The FRP secondary containment unit was

movement anticipated during earthquake conditions. The tank was designed and constructed with adequate bracing and anchoring to withstand the expected seismic loads. The tank and support structure were designed using a liquid waste specific gravity of 1.0. Structural calculations are included in Appendix D.

- 2..3. Compatibility With Wastes: The Leachate Storage Tank could potentially be exposed to any of the waste streams which the facility is permitted to handle. However, these compounds will not be in concentrated form. Tests previously performed on the leachate from the landfill collection system indicate that it has a pH of approximately 6.1 to 6.8. This indicates that the material will not be reactive. Additional data on the leachate indicates that the conductivity ranges from 74,000 to 110,600 micromhos per centimeter (µmho/cm). The corrosion resistant properties of FRP ensure that substances with a pH near 7 will not effect the integrity of the system. In addition, liquids having a conductivity of greater than 75,000 µmho/cm, will not affect these materials. Based on the chemical resistance properties of FRP and the dilute nature of the wastes potentially present, the materials from which the tank and secondary containment were constructed are appropriate for use with the liquid to be stored in the tank. As an additional measure of protection against the failure of the tanks due to incompatibility with the wastes, the tanks will be inspected routinely, and repaired if necessary, as outlined below.
- 2..4. Corrosion Protection: Both the primary containment tank and the secondary containment tank were constructed entirely from corrosion resistant materials. In addition, the tank will be inspected prior to being placed into service, or prior to a change in service, to ensure that it does not fail due to corrosion. To prevent damage caused by incompatible wastes, the tank will be decommissioned and cleaned prior to a change in service. Any problems detected will be corrected prior to placing the tank into service.
- 2...5. Inspection/Testing: The storage tank and the associated containment system have been inspected or tested as required to demonstrate compliance with 40 CFR Part 264, Subpart J. The tank was successfully hydrotested on March 24, 1995. A data sheet for this test has been included in Appendix B.

3. CERTIFICATION: This constitutes certification of the proper design and construction of the Leachate Storage Tank at the U.S. Ecology facility in Beatty, Nevada, in compliance with the requirements of 40 CFR Part 264, Subpart J.

I certify under penalty of law that this document and all attachments were prepared under my direction or supervision in accordance with a system designed to assure that qualified personnel properly gather and evaluate the information submitted. Based on my inquiry of the person or persons who manage the system, or those persons directly responsible for gathering the information, the information submitted is, to the best of my knowledge and belief, true, accurate, and complete. I am aware that there are significant penalties for submitting false information, including the possibility of fine and imprisonment for knowing violations.

NAISMITH ENGINEERING, INC.

Grant A. Jackson, P.E.

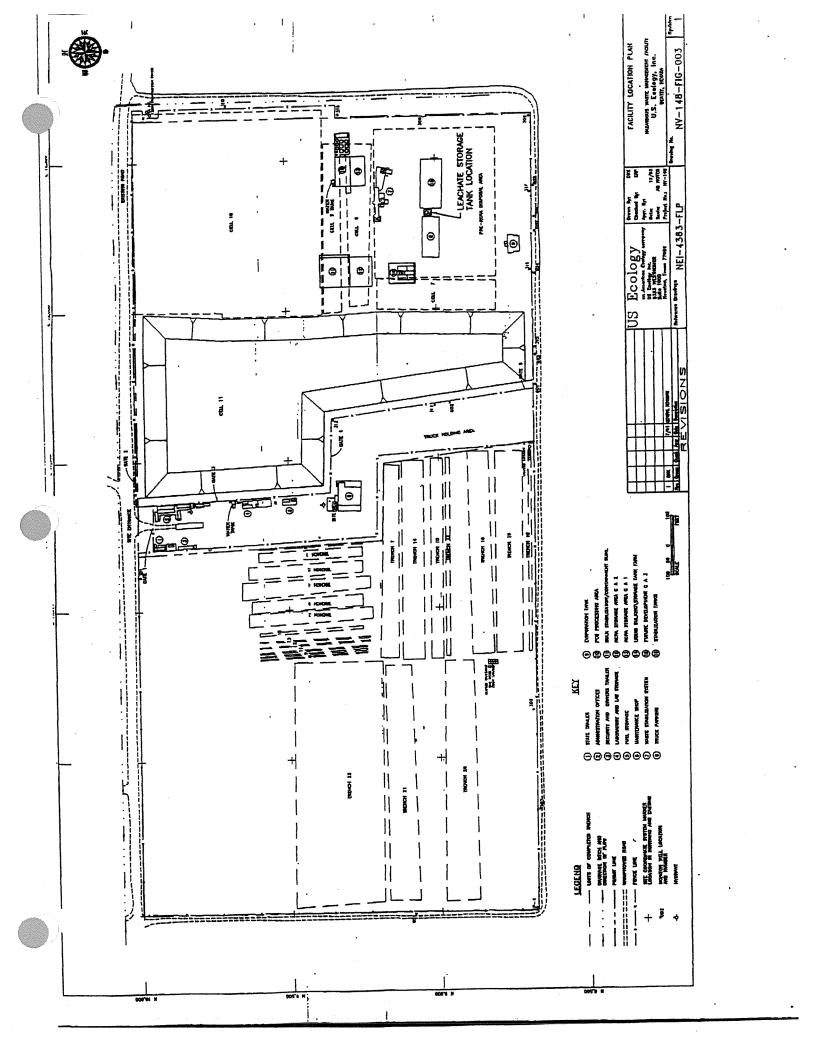
GRANT AND CIVIL CIVIL ON 10299

REFERENCES

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- ACI 318-89 and ACI 318R-89 (revised 1992), <u>Building Code Requirements for</u> <u>Reinforced Concrete and Commentary</u>, American Concrete Institute Publications.
- 3. "Investigation of the Geotechnical Conditions for Planned Containment Building, Stabilization Building, and Tank Farm", Grant Environmental, Englewood, Colorado, June 15, 1994.
- 4. Perry, Robert H., and Chilton, Cecil H. (1973), Chemical Engineers' Handbook, 5th Edition, McGraw-Hill Book Company, New York.
- 5. Rainfall Frequency Atlas of the United States, U.S. Department of Commerce Weather Bureau, May 1961.
- 6. Ringo, B. C., and Anderson, R. B. (1992), <u>Designing Floor Slabs on Grade</u>, The Aberdeen Group, Addison, Illinois.

D:\4383\REPORT.0

APPENDIX A
Site Location Map



APPENDIX B Storage Tank Data

0.25010 MIN. 0.25010 MIN.

DESIGN CONDITIONS

TEMP: AHB CONC; TOP: DISHED CAPACITY: LOCOODGO! NON BPEC GRAV: BERVICE: VASTE VATER
PREDEURE: ATMOSPHERIC. STATIC HEAD E-GLASS BURFACE MOVATANK GREY GELCDA! LINER ISOPHTHALIC X/ C-VEI HE KONT: BOLTE: ZINC PLATED STEEL STANDARD: ASIH 113299 STTMCTURE [SOPHTHAL GASKETS: NEUPRENE DIAMETER: 12ft III BOTTOM FLAI

LINGS OF SCHEDULE

QUANTITY: [1]

BIZE DEBCRIPTION

KEY TO FITTINGS.
BRV - BOLTED MANYAY
FTC - FULL THREADED COUPLING
THC - THREADED HALF-COUPLING
VGN - GODSENECK YENT

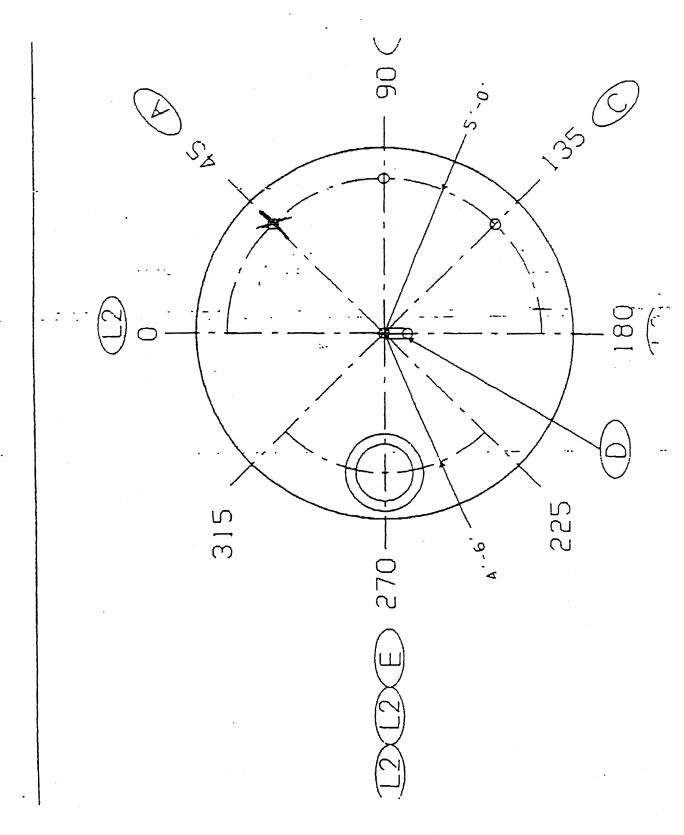
ACCESSORIES

CARBON STE MA TEFUAL POTON QTY 8 YM

CHOP 27% E-GLASS REINFORCEMENT 0.043
HOOP VOUND 50% E-GLASS REINFORCEMENT 0.023
1.502 RANDOM STRAND HAT 0.043
2402 VOVEN ROVING 0.033
C-VEIL 0.010 OIE~>

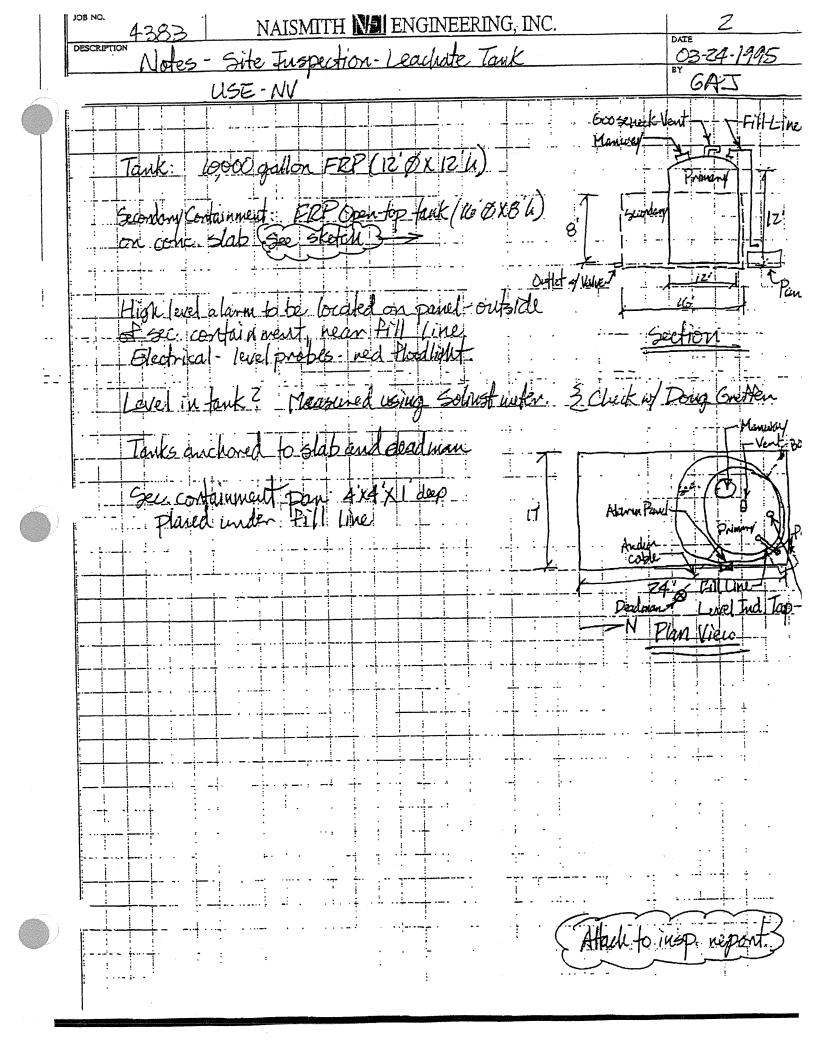
STRUCTURE

15. - 4" The experient 12...-0.



NAISMITH ENGINEERING, INC. PROJECT INSPECTION REPORT

Project Title: Leachate Tank Certification					
Owner: U.S. Ecology, Inc. Beat	V. NV (American Ecology)				
Owner's Project No.: NV-	NEI Project No.: 4383				
	•				
Date: March 24, 1995 Time: 6	915 to 1800 (PST) Page <u>i</u> of <u>Z</u>				
Contractor: N/A	Type of inspection: ☐ daily ☐ periodid				
Inspector(s): 6AJ	Persons contacted on-site: Dave Toltent, Dava Gurten Bill Marchind				
Weather. Cold which to over cast	Testing in progress:				
Contractor: working delayed (weather delayed due to					
Work in progress: Tustallution of high	h level alarm by site personnel.				
Work completed since last inspection: N/	4				
Equipment/materials received on-site since last inspection: NA High level alarm					
Summary: 0915 - Arrived at site 1030 - Instructed Installation of high level abarm. 1100 - Began Filling with water 1000 - Made initial measurements (Primary touk - 3.i0") (See attached sheet for summary of notes made during inspection)					
The state of the state of the	(Attach additional sheets as required)				
Signature of inspector(s):	Salpo				
	Eudony, Dave Tolbert-U.S. Ecology				



NAISMITH ENGINEERING, INC. PROJECT INSPECTION REPORT

Project Title: Leachate Tank Certification						
Owner: U.S. Eiology, Inc., Beatty, NY (American Ecology)						
Owner's Project No.:	NEI Project No.: 4383					
Date: 03-25-1905 Time: (0830 - 1000 P57 Page 1 of 1					
Contractor: N/A	Type of inspection: ☐ daily ☒ periodid					
Inspector(s): 6AJ	Persons contacted on-site:					
Weather: Cold (45°) wind to clear Contractor: ☐ working ☐ delayed (weather ☐ delayed due to ☐ N/A	Testing in progress: Wydrostatic alarm					
Work in progress: None						
Work completed since last inspection: Tustallation of High level alarm						
Equipment/materials received on-site since last inspection: Nove						
Summary: Visual observations: no visible leaks; no bubbles, etc.						
Liquid level measurements (0920): Primary 3.10' Secondary 8.60"						
High level alarm checked: ok						
	(Attach additional sheets as required)					
Signature of inspector(s):	Jalho					
Distribution: Steve Del Homme-American	. Ecology, Dave Tolbert- U.S. Ecology					

E:\PROJMANNSP.FRM

REVISED 08-30-94

APPENDIX C
Containment System Volume Calculations

April 18, 1995

JOB NO. 4383

NAISMITH ENGINEERING, INC.

SHEET NO. 1

DESCRIPTION:

LEACHATE STORAGE TANK

DATE: 03-23-1995

SECONDARY CONTAINMENT VOLUME CALCULATIONS

OBJECTIVE:

Compute the required height for the secondary containment Part 1. walls for the Leachate Storage Tank.

Compute the required height for the secondary containment Part 2. walls for the pan under the piping.

PART 1

APPROACH:

Determine the required volume of containment according to 40 CFR §264.193, which requires that the secondary containment be able to contain one hundred percent (100%) of the capacity of the largest tank within its boundary, plus the precipitation resulting from a 25-year, 24-hour rainfall event.

ASSUMPTIONS:

- The storage tank has a nominal storage capacity of 10,000 gallons. 1.
- The secondary containment is a circular open-top tank, sixteen (16) 2. feet in diameter and eight (8) feet in height.
- The secondary containment unit is sized to also hold a 100-year, 24-hour rainfall event. In the vicinity of Beatty, Nevada, a 100year, 24-hour rainfall event produces 2.60 inches of rain water.
- Since the secondary containment unit only contains one tank, a leak 4. in this tank will equalize levels inside the tank and the secondary containment unit. Therefore, no containment volume will be lost to the tank. Calculations will be based on the gross area of the secondary containment unit.

CALCULATIONS:

Calculate the area of the secondary containment unit, A. Step 1

$$A = \pi \times r^2 = 3.14159 \times (8)^2 = 201.1 \text{ ft}^2$$

This is equivalent to 201.1 ft3 per foot of height

Calculate the volume of liquid to be contained, V. Step 2

 $V = 10,000 \text{ gal/}(7.48 \text{ gal/ft}^3) = 1,336.9 \text{ ft}^3$

JOB NO. 4383 DESCRIPTION:

NAISMITH ENGINEERING, INC.

SHEET NO. 2

LEACHATE STORAGE TANK

DATE: 03-23-1995

SECONDARY CONTAINMENT VOLUME CALCULATIONS

Step 3 Calculate the required containment wall height, h, based on tank volume (V) alone.

 $h = V/A = 1,336.9 \text{ ft}^3/201.1 \text{ ft}^2 = 6.65 \text{ ft}$

Step 4 Calculate the total required containment wall height, h, based on V_{PCB} and a 100-year rainfall event.

 $h_t = 6.65 \text{ ft} + 2.6 \text{ in/(12 in/ft)} = 6.86 \text{ ft}$

Using 8.0 feet provides 1.1 feet of freeboard indicating that this design is adequate.

PART 2

APPROACH:

Determine the required volume of containment according to 40 CFR §264.193. This will include the volume of the piping, plus the precipitation resulting from a 25-year, 24-hour rainfall event.

ASSUMPTIONS:

- 1. The fill piping has a diameter of two (2) inches.
- 2. The fill piping is approximately seventeen (17) feet in length.
- 3. The dimensions of the secondary containment pan are four (4) feet by four (4) feet by one (1) foot high.
- 4. An air-gap is provided between the tank fill entrance and the highest level in the tank. This will prevent siphoning the contents of the tank back into the pan.
- 5. The secondary containment pan is sized to also hold a 100-year, 24-hour rainfall event (2.60 inches).

CALCULATIONS:

Step 1 Calculate the volume of liquid contained in the piping, V.

 $V = \pi \times r^2 = 3.14159 \times (2/12)^2 \times 17 = 0.37 \text{ ft}^3$

JOB NO. 4383 DESCRIPTION: NAISMITH ENGINEERING, INC.

LEACHATE STORAGE TANK

SHEET NO. 3

DATE: 03-23-1995

SECONDARY CONTAINMENT VOLUME CALCULATIONS

Step 2 Calculate the wall height required.

 $h = 0.37 \text{ ft}^3 / (4 \times 4) \text{ ft}^2 = 0.023 \text{ ft } \times 12 \text{ in/ft} = 0.28 \text{ in.}$

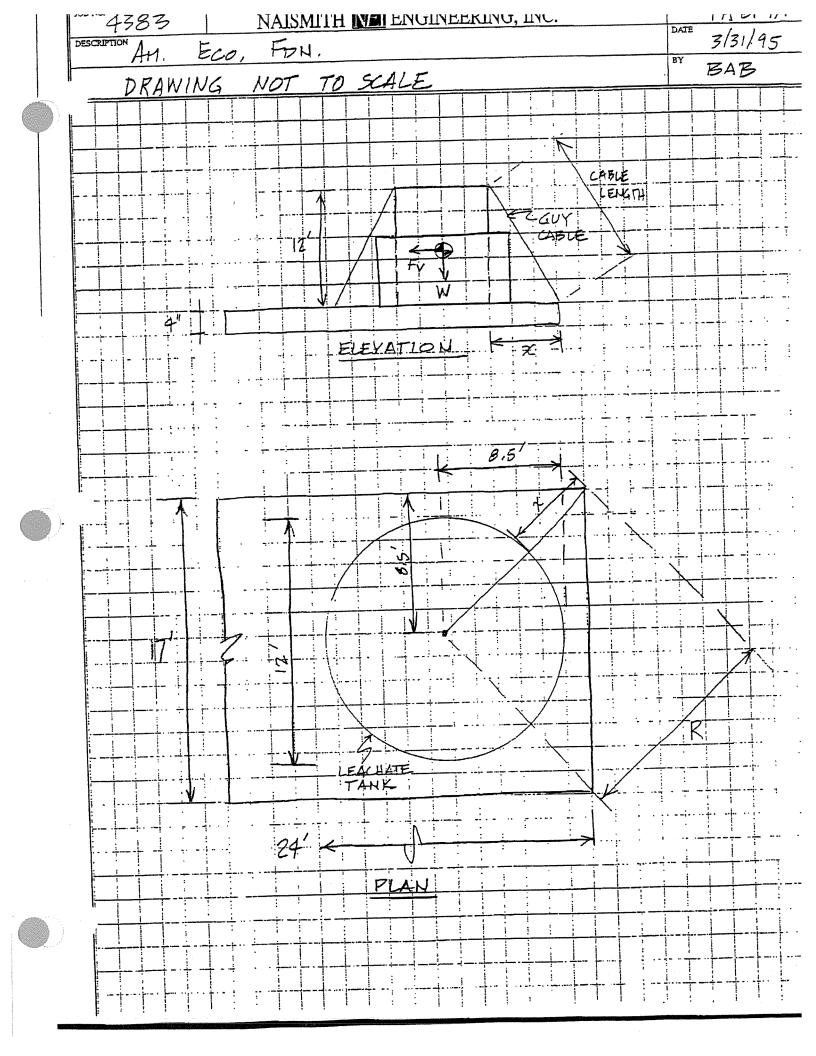
With a precipitation allowance of 2.6 inches, this gives a total height of:

h = 2.60 in + 0.28 in = 2.88 in.

Using 12 inches provides 9.12 inches of freeboard indicating that this design is adequate.

D:4383/2NDCONT.CAL

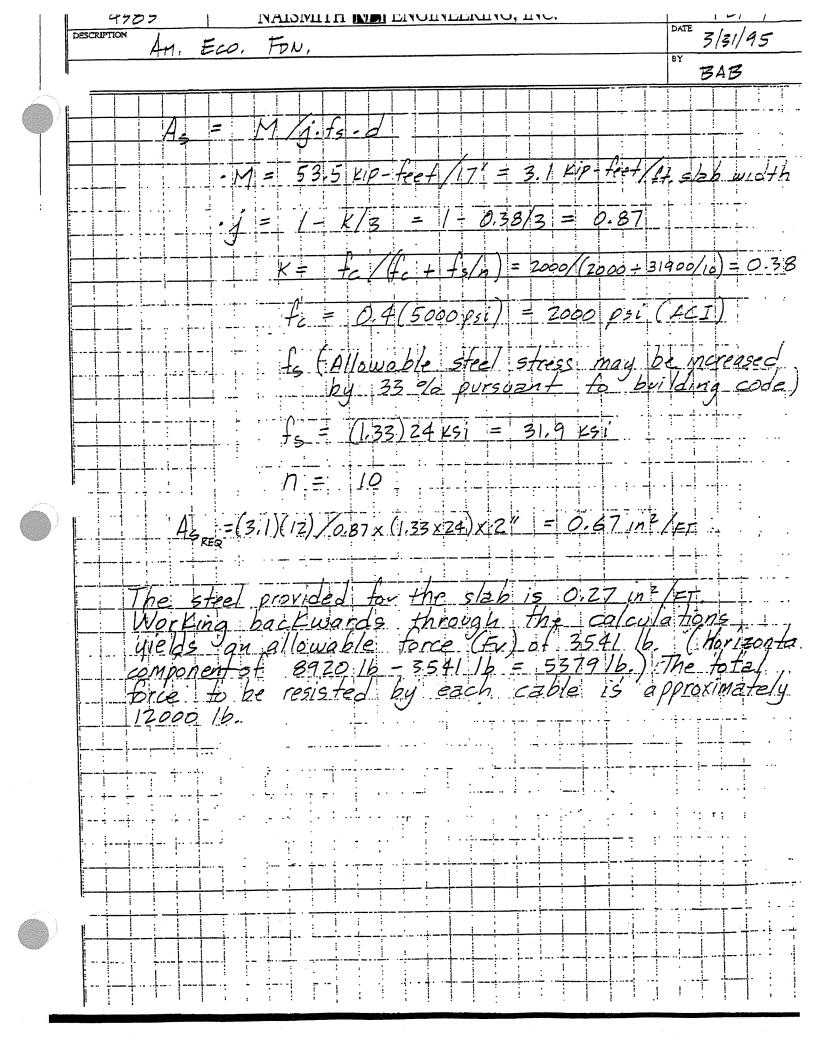
APPENDIX D
Structural Calculations

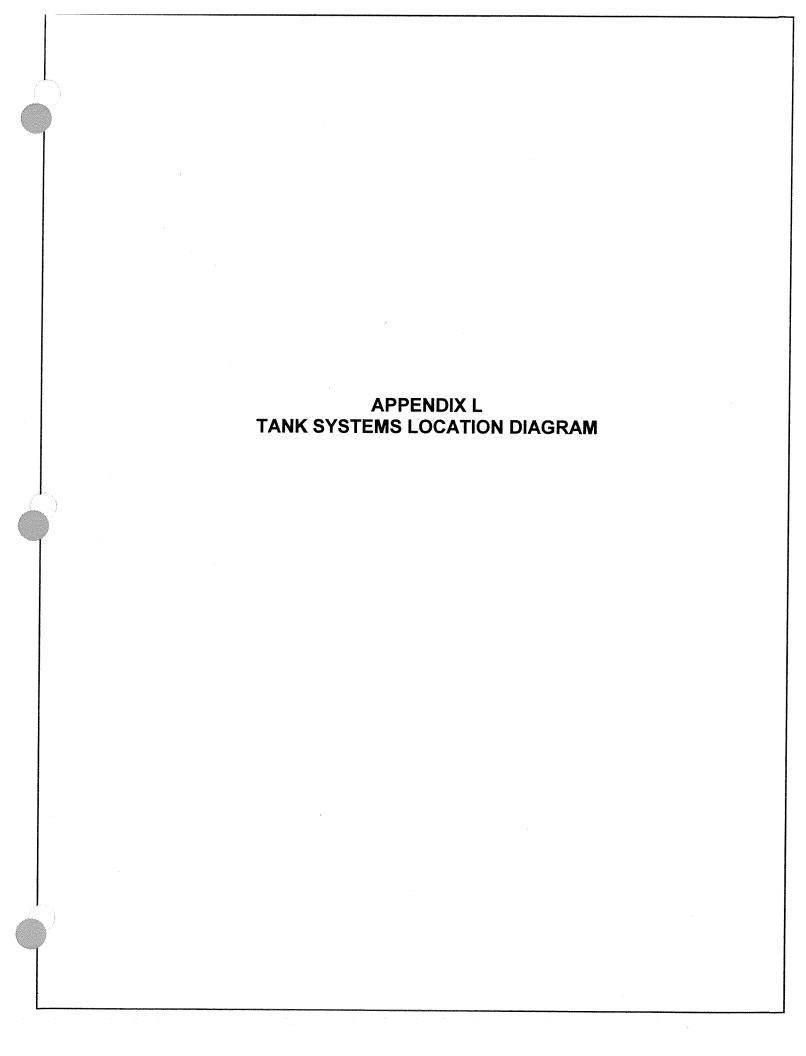


4383	NAISMITH NEI ENGINEEKING, INC.	DATE /
CRIPTION AM.	ECO. FOUNDATION CHECK	3/31/95
		BAB
	NAISMITH ENCINEEDING INC.	
	CALCULATIONS - LEACHATE STORAGE TANK	
	REINFORCED CONCRETE SLAB-ON-GRAD	
OBU SCTIVE	: To perform a check of the structural	adequocy
	of an existing slab-on-grade.	
Approach	tstablish soil pressure limits.	
· · · · · · · · · · · · · · · · · · ·	2. Perform analysis of sha based on	estadional
j -	engineering standards and the 199	1 Unitorn
	Building Code	
· · · · · · · · · · · · · · · · · · ·		
	3. Consider all loading conditions to why	<u> </u>
	dab may be subjected	
	↓ · +	
GIVEN :	1. The site is located of the edge Zone 3 seismic loading.	0t-+-
	Cone 3 seismic loading	···
	2 Previous soils report by Grant &	numan Montin
	recommended soil pressures not	10
	exceed 5 tsf	
	3 Plan dimensions of slap, thick	mess of
	slab and reinforcing steel with	hin the
	Sab	
	4. GUY WIRES (4) PROVIDED TO CREATE DAM	PING EFFEC
	FROM SEISMIC LOAPING	·
CALCULA		letermine
		and size
	adequacy of slab thickness	CALLED
	W = WTANK + WLIDURD	
	Worney (includes primary containment	6nK = 4500
	Witnes (tank full) = 84,700 /bs.	

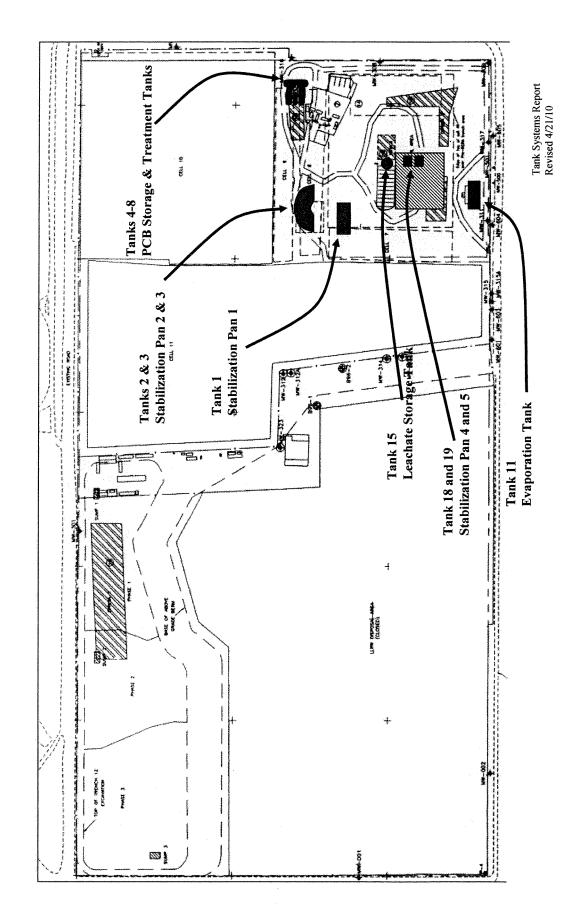
	4585 NAISMITH NOI ENGINEERING, INC.	DATE , /
	DESCRIPTION AM, EGO, FON.	3/31/95
		BAB
'n,		
	W = 4500 + 84700 = 89,200 /6	
	7 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	
	SEISMIC FORCES GOVERN OVERTURNING BASEL	
	OF THE WEIGHT (W) IS APPLED TO THE BAS	
	OF THE TANK (S) AND 15 ASSUMED TO ACT IT	4 ROUGH
	THE CENTER OF GRAYITY (C.G.) OF THE TANK	4
	CONTAINING LIQUIDS	
<u>-</u> .	FY (SEISMIC SHEAR FORCE) = 0.10(89, 200	= 89201b.
	M (OVERTURNING MOMENT) = (8920 16)6.0	FL)
	M = 53,520 lb-FT. (53.5 KIP-feet)	
:	Mr (resisting moment) = (17/x 24/x t) 0.150 x/c	U.FT 17/2
	GET ME (resisting moment) M (overturning moi	neut) XF. J.
	520t. = 53.5(1.4)	
	+ = 0.14 feet < 0.33 f	pet O.K.
	Stop No. 2 Check of soil bearing press	2/1/0
	TYPICAL LOADING	
	Since tank is not resting on the c	enter of
	the slab, assume majority of loading	9 15
		1 = 616 DO. F1
	Soil Bearing (SB)= (89,20016, + slob weig	ht)/272
	5B = 189200 + (24/17/10.3)	31 150 1/272
	5B = 402 PSF << 5 TSF	

l	4383 NAISMITH NEI ENGINEERING, INC.	70+ 7
	DESCRIPTION AM. ECO. FDN.	3/31/95
		"BAB
$\langle \hat{\Delta} \rangle$		
	· FEISHIC LOADING (FOR PURPOSES OF SOIL BESKING	PEESSURE,
	THE DAMPING EFFECTS OF THE GUY WIEES (CABLE	5) WILL:
	BE CONSERVATIVELY NEGLECTED.	
	GOIL BEARING = W/A ± MY/T	
		1 1 1
	: Y = Distance from edge of slob to ce	nter of 510p.
	1 = 8.5 feet	
- ·	I = Moment of inentia of slab foot	2 right
	$T = bh^2/12 = (16)(17)^2/12 = 385$	4
:	GOIL BEARING(3B) = 402 + 53,520(8.5)/385 =	
$(\tilde{\ })$	5B = 402 + 1182 = 1584 psf < 2000	PSE U.A.
	Step No. 3 Check sliding	
•		
	\$ (Provided) = 28° \(\tan^- (\frac{t}{V}/W) \)	
	D(actual) = tan-(8920/89200) = 5.7	° < 0 28° O.K
	4 (actual)	- 1 - 1 - 4
	Step No. 4 PUNCHING SHEAR	
	O.K. By inspection	
	step No. 5 Reinforcing	
		he slab
	The maximum moment is induced in to	and 15
	there fore equivalent to the overturning	y moment

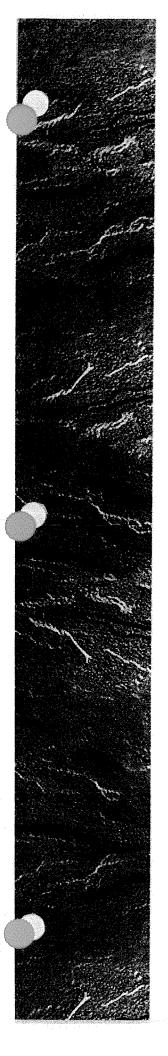




Tank Systems Location Diagram US Ecology Nevada, Inc.



APPENDIX M CONTAINER MANAGEMENT BUILDING TANK SYSTEMS 18 AND 19 (STABILIZATION PANS 4 AND 5)



INSTALLATION CERTIFICATION REPORT

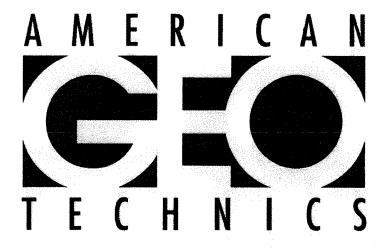
Stabilization Facility - Mixing Tanks Beatty, Nevada

Project No. 06B-G1263.1

Prepared for

US Ecology Nevada

May 4, 2007



Prepared for

US Ecology Nevada PO Box 578 Beatty, NV 89003

Attention: Bob Marchand, Facilities Manager



INSTALLATION CERTIFICATION REPORT

Stabilization Facility - Mixing Tanks Beatty, Nevada

American Geotechnics Project No. 06B-G1263.1

Prepared by

American Geotechnics

XP 6-30-10

VAUGHN J. THURGOOD

CIVIL

Vaughn Thurgood, PE

CQA Manager

Rex W. Hansen, PE Haho

Principal Engineer

May 4, 2007 Page i



TABLE OF CONTENTS

			PAGE
1.0	INTRODUCTION		1
	1.1	Purpose and Scope of Work	1
	1.2	Description of Operations	1
	1.3	Description of Tanks	2
	1.4	Description of Tanks	3
	1.5	Corrosion	3
2.0	CONSTRUCTION 4		
	2.1	Construction Sequence	4
3.0	CONTAINMENT TESTS		5
	3.1	Secondary Containment Test	5
	3.2	Primary Containment Test	5
4.0	CER	TIFICATION	6

APPENDICES

Tank Construction Drawings A

Sheet M101

Sheet S101

Sheet S102

Sheet C204

Sheet C207

Sheet C211

- B Tank Construction Photos
- \mathbf{C} Hydrostatic Test Reports





1.0 INTRODUCTION

1.1 Purpose and Scope of Work

American Geotechnics was retained to provide construction quality assurance (CQA) services during the erection of the Stabilization Facility at the US Ecology Nevada (USEN) site. This report has been prepared for the purpose of certifying the installation of two mixing tanks in conformance with Title 40 CFR Part 264 Subpart J. The tanks were constructed as part of a new stabilization facility. The site is located in Nye County approximately 11 miles south of Beatty, Nevada along Highway 95.

1.2 Description of Operations

The subject tanks will serve as mixing pans, used to facilitate the solidification or stabilization of waste materials. Waste materials will typically be transferred into the mixing tanks from either end-dump trucks or tankers. The waste materials may consist of liquid, sludge, or solid waste debris with hazardous characteristics. Waste stabilization will be accomplished by mixing hazardous waste materials with reagents (cement, lime, kiln dust, etc.). A hydraulic excavator will be used to provide the necessary mixing forces and to remove the stabilized waste materials from the tank upon completion. The stabilized materials will then transported and placed in a permanent landfill repository at the site.

We understand the permitted operational procedures at the facility require daily inspection of the secondary containment of the mixing tanks to check for leakage through the primary containment. We also understand that as a matter of practice, USEN will not allow waste materials to be stored in the mixing tanks for extended periods of time (i.e. the materials are treated and removed within a shift period).



May 4, 2007 Page 2

1.3 Description of Tanks

The subject mixing tanks are similar in design to the existing mixing pans currently used at the USEN facility. The mixing tanks consist of a steel plate primary containment vessel and an epoxy coated concrete structure that provides secondary containment. The tanks were designed to withstand the static weight of the waste materials in addition to the anticipated dynamic loads from the loading, mixing and unloading activities.

1.3.1 Primary Containment

Structural design of the steel vessel was performed by Samuel Engineering of Greenwood Village, Colorado. The steel vessel consists of the following components, as illustrated on Sheets S101 and S102:

- An external ¾-inch steel wear plate;
- a ½-inch steel structural plate; and
- wide flange (W6x15) structural framing members.

1.3.2 Secondary Containment

Structural design of the secondary containment concrete structure was provided by SECOR of Tualatin, Oregon. The mixing tank secondary containment consists of an epoxy coated, reinforced concrete structure, as illustrated on sheet C204. The concrete mat foundation is 24 inches thick and reinforced with two sets of #6 rebar spaced at 6 inches on-center in both directions, located near the top and bottom of the mat. The 12-inch thick walls are reinforced with a set of #6 vertical rebar at 6 inches on-center and a set of #5 horizontal rebar at 12 inches on-center.

The concrete mixing tank floors include a system of longitudinal drain channels that slope toward a collection box, as illustrated on Sheets C207 and C211. Inspection of the collection box is provided with a 4-inch diameter steel pipe that allows access through the primary steel vessel.



May 4, 2007 Page 3

1.4 Compatibility with Waste

The mixing tanks could potentially be exposed to any of the waste streams handled by the USEN facility. Reactive materials and materials with high pH or low pH values represent the greatest potential for incompatibility with the steel tanks. We understand that routine maintenance inspections will be performed to evaluate the condition of the ¾-inch wear plate, and that replacement wear plates will be installed as needed.

The epoxy coating on the concrete structure will inhibit the effects of hazardous materials that may come into contact with the secondary containment.

1.5 Corrosion

The mixing tanks have no external metal components in contact with the soil or water. All reinforcement steel within the concrete secondary containment structures was constructed with the specified 3 inches of cover.







2.0 CONSTRUCTION

2.1 Construction Sequence

Record Steel Construction Inc. (RSCI) of Meridian, Idaho performed construction of the new Stabilization Facility and the subject mixing tanks. Tank construction began with excavation of the subgrade materials. The subgrade materials at the site were prepared and inspected prior to placement of tank foundations, which were observed to consist of Poorly Graded Sand with Silt and Gravel (SP-SM). The subgrade materials were moisture conditioned and compacted to 95 percent of standard proctor (ASTM D 698), in accordance with the construction specifications. Steel reinforcement bars for the tank mat foundations and walls were erected and cast, as shown in the enclosed photos (Appendix B). Structural fill, consisting of the native SP-SM materials, was placed around the exterior of the concrete structure in controlled lifts, moisture conditioned, and compacted to 95% of standard proctor. Multiple epoxy coatings were applied to the interior surfaces of the concrete tanks.

The primary containment steel vessels were fabricated by Rule Steel in Middleton, Idaho. Each tank vessel was fabricated and transported to the site in two halves. The vessels were lowered into position at the site using a 30-ton crane and then joined together along a common seam weld. The integrity of the primary and secondary containment was tested, as described in the following section.



May 4, 2007 Page 5

3.0 CONTAINMENT TESTS

3.1 Secondary Containment Test

The integrity of the secondary containment structures for mixing tank #1 and #2 were tested as described in this section. Each concrete structure was filled with 12 inches of water and inspected after a minimum of 24 hours to record any loss of liquid. The water was exposed to the atmosphere during the test and thus was subject to evaporation. An open-ended control barrel was located on the floor of the concrete tank and monitored to account for the effects of evaporation during the testing periods. The hydrostatic tests performed on the concrete secondary containment structures indicated no net loss of liquid during the test periods.

3.2 Primary Containment Test

The integrity of the steel primary containment vessels for mixing tank #1 and #2 were tested as described in this section. Each steel vessel was filled to capacity with water and monitored for leakage over a 24-hour period. No water was observed to leak into the secondary containment during the test periods.

May 4, 2007

Page 6



4.0 CERTIFICATION

"I hereby certify under penalty of law that this document and attached test results were prepared and conducted under my direct supervision. The information submitted, to the best of my knowledge and belief is true, accurate, and complete. The signature and seal provided below is a declaration by the Professional Engineer that, in his professional judgment, the subject mixing tanks were designed, constructed and tested in a manner consistent with the referenced design document and applicable state and federal regulations."

American Geotechnics

Vaughn Thurgood, PE

VAUGHN J.
THURGOOD
SSUN CIVIL
NO. 18380



APPENDIX A

TANK CONSTRUCTION DRAWINGS

M101

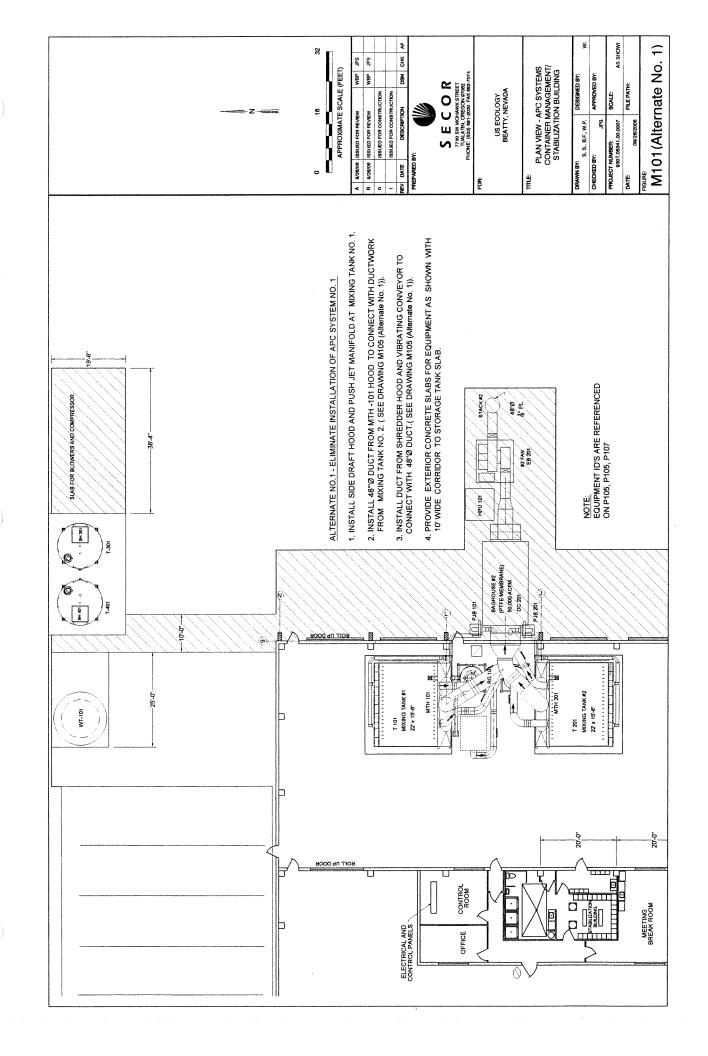
S101

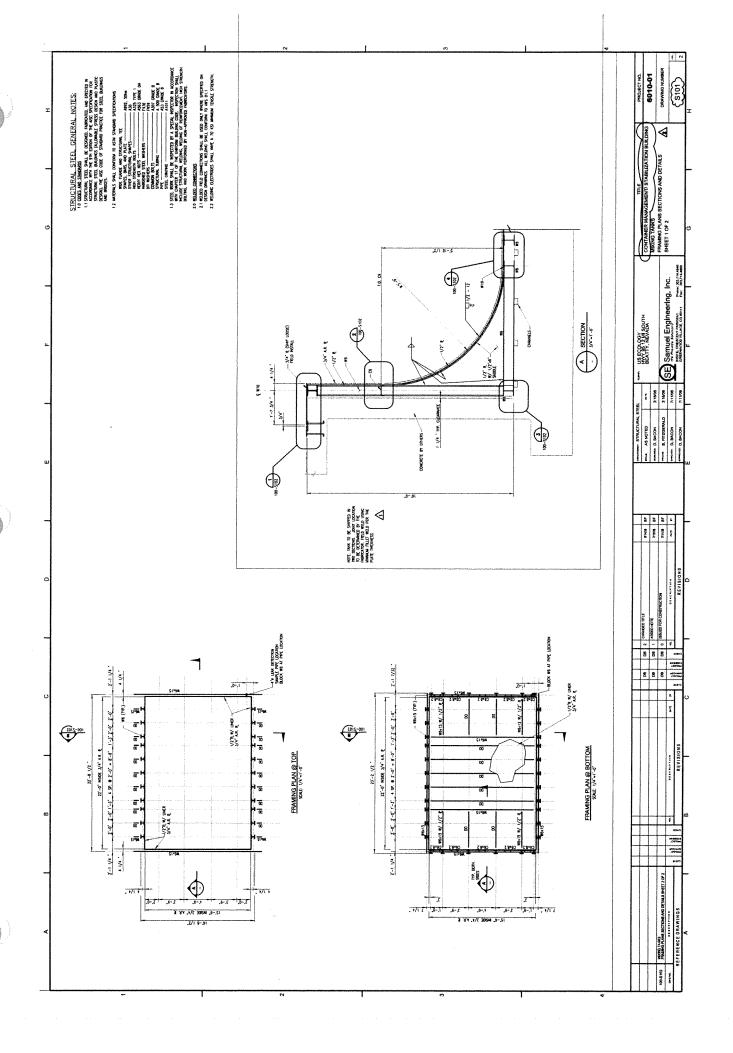
S102

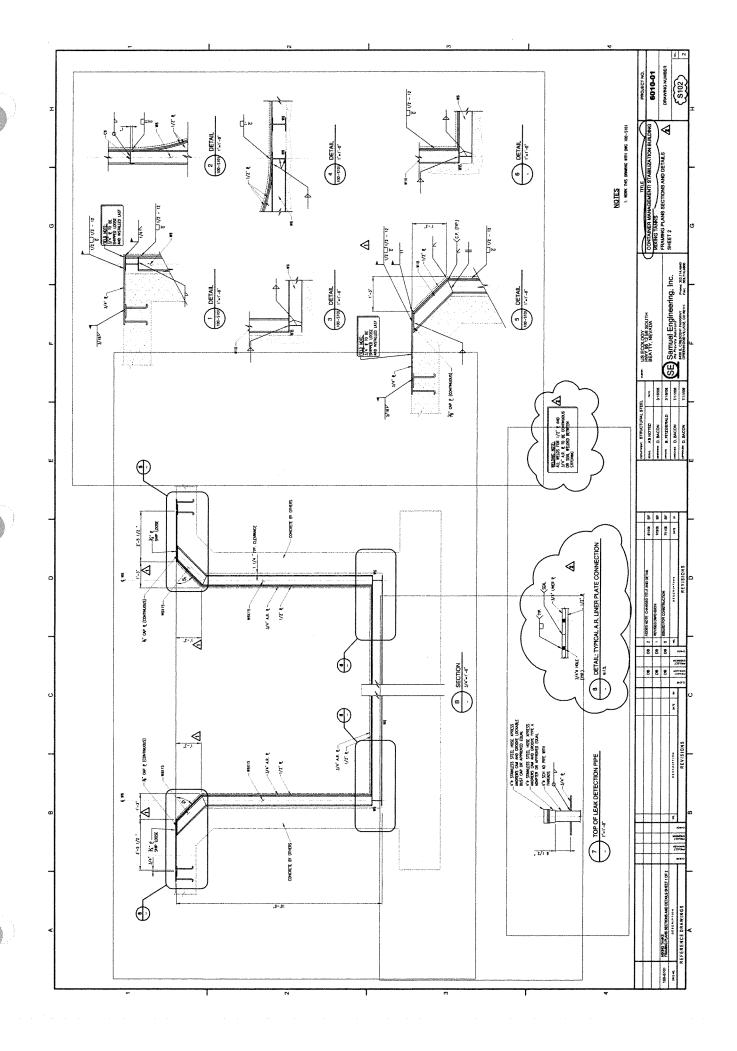
C204

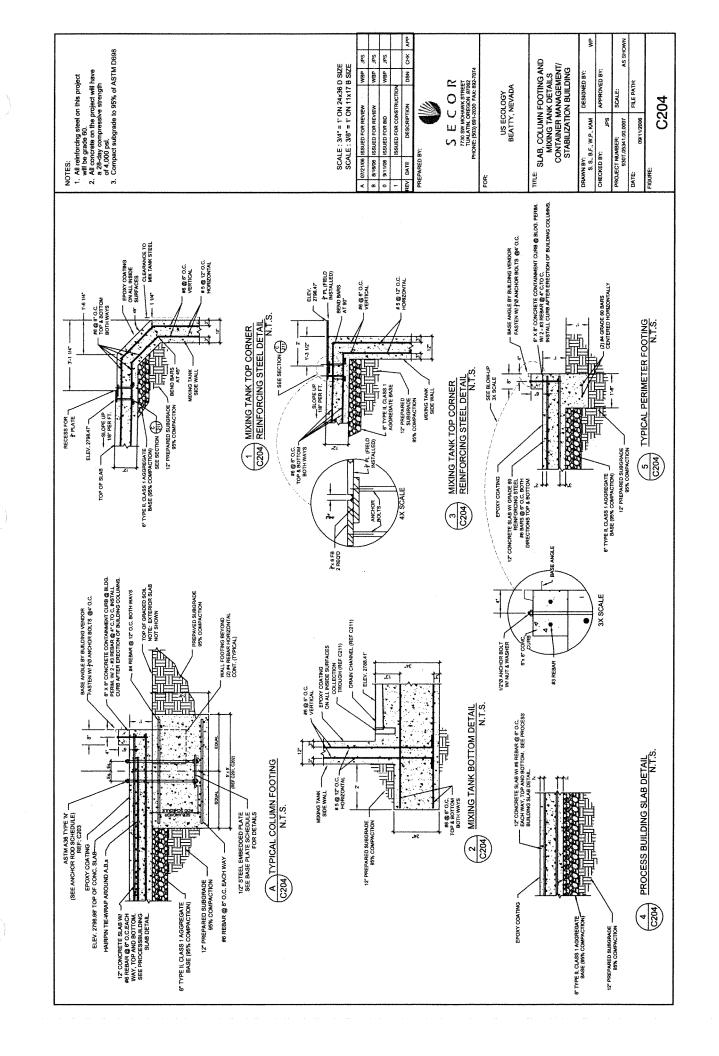
C207

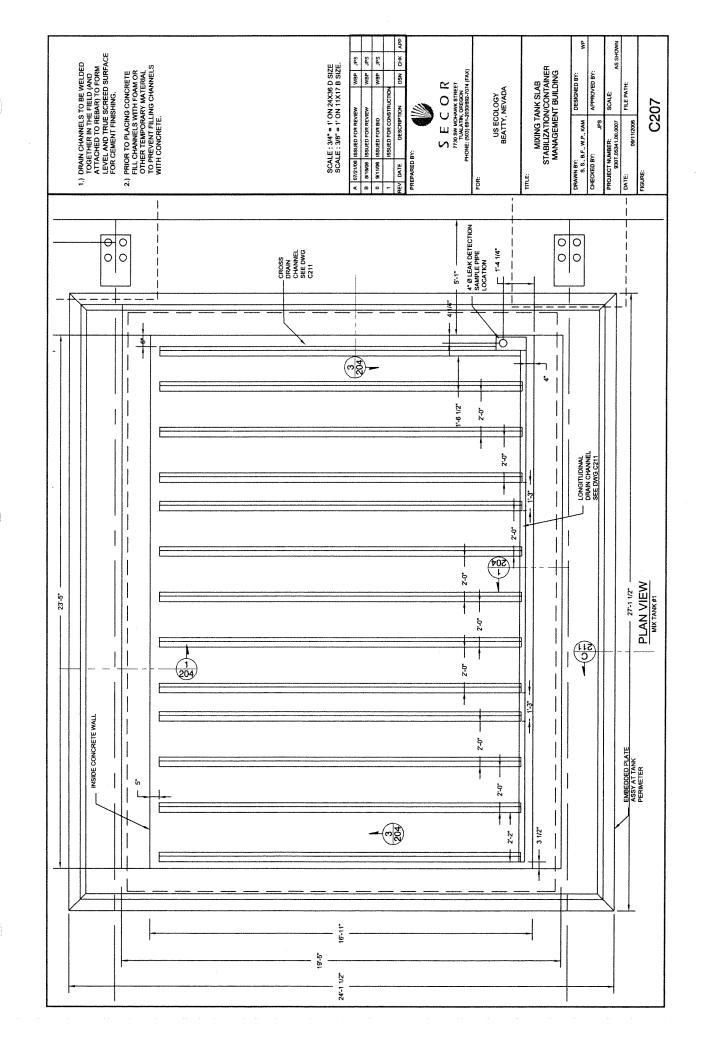
C211

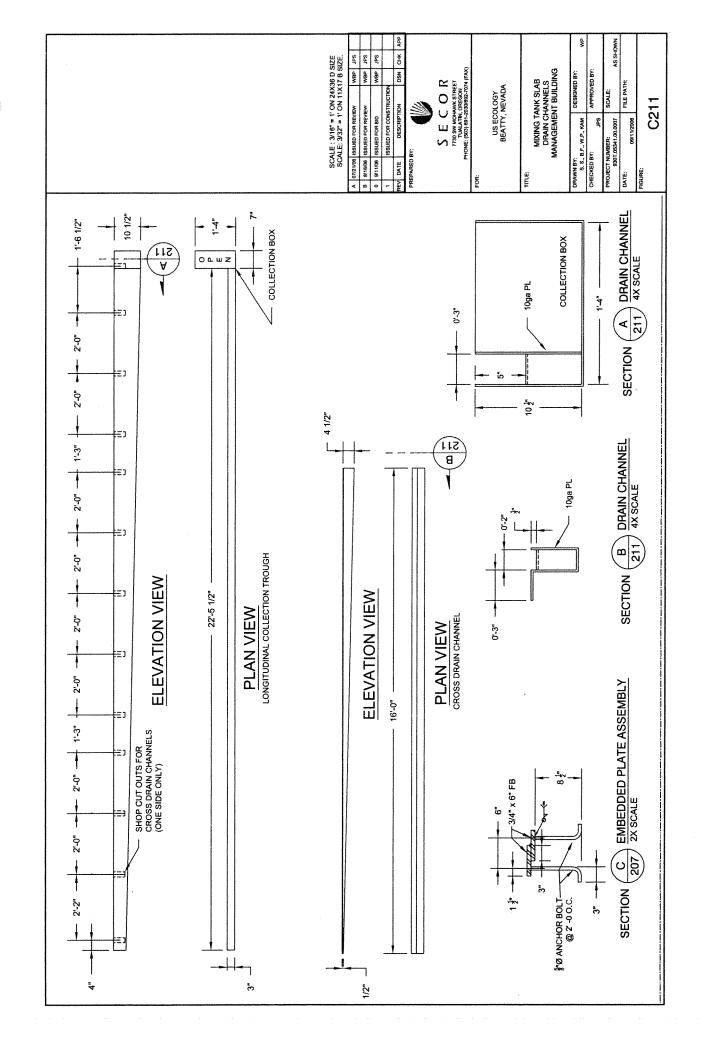














APPENDIX B

TANK CONSTRUCTION PHOTOS



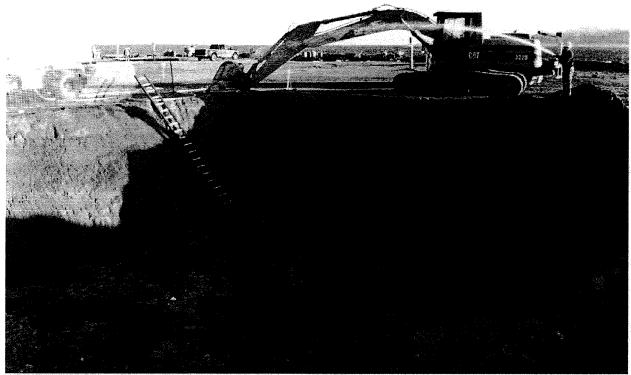


Photo — 1 The sand and gravel subgrade materials are moisture conditioned and compacted following excavation.



Photo – 2 Survey control for the foundation of mixing tank #1 is established while excavation continues for mixing tank #2.





 $\overline{Photo} = 3$ View of the #6 rebar installation prior to pouring the tank mat foundations.

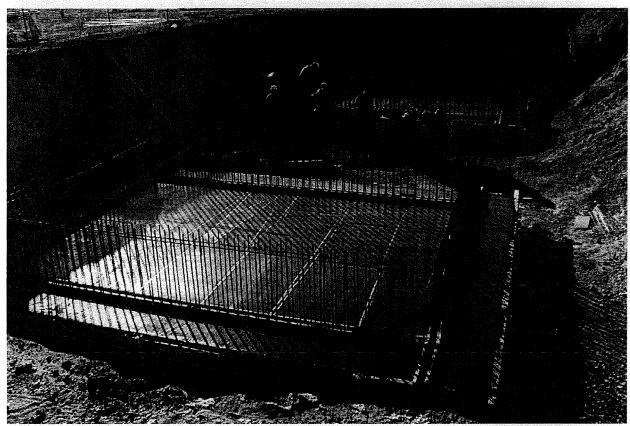


Photo -4 View of the freshly poured tank foundations.



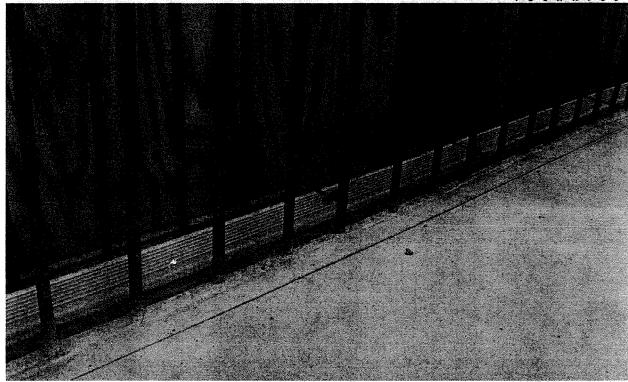


Photo - 5 View of a water stop installed along the construction joint located between the walls and the foundation of the tanks.

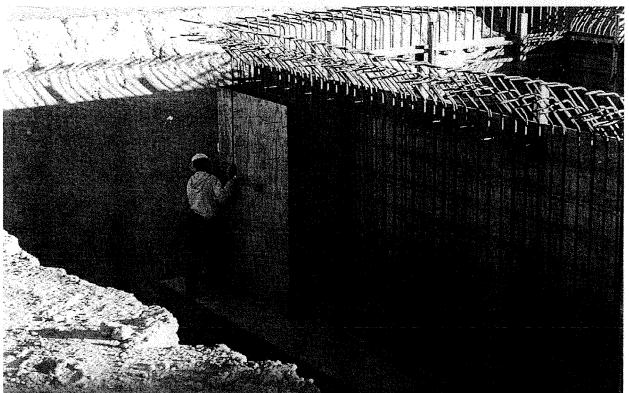


Photo -6 Typical view of the vertical and horizontal reinforcement in the walls of the tanks.



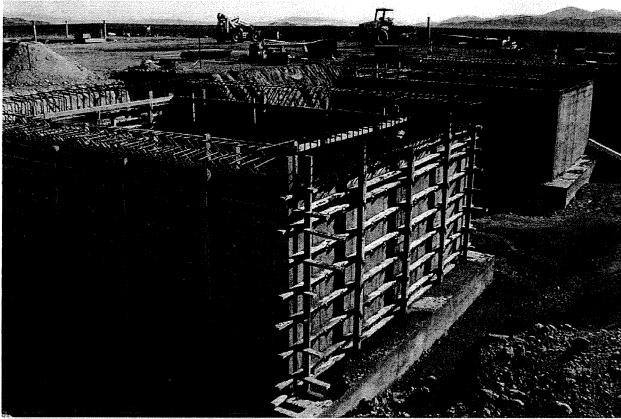


Photo -7 View of the completed formwork and concrete placement.

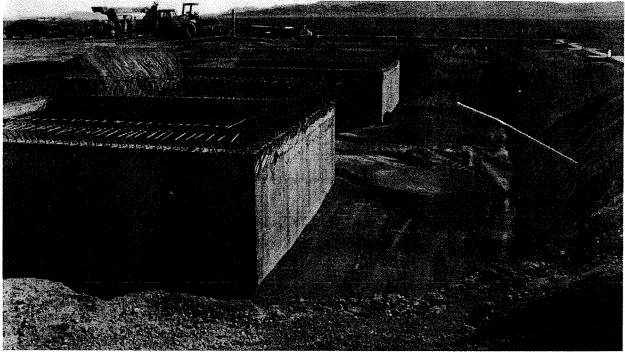
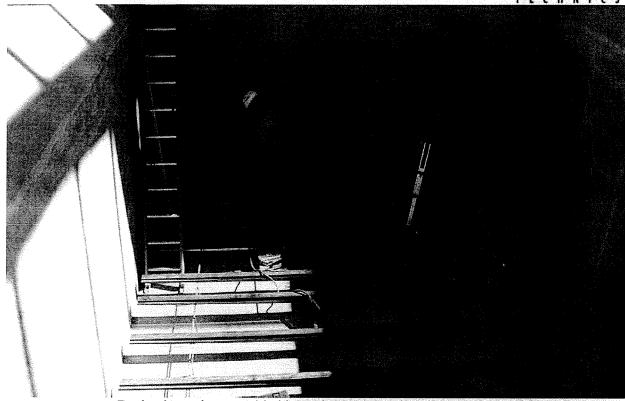


Photo - 8 Structural fill is place around the exterior perimeter of the concrete tanks in uniform lifts and compacted.





Drain channels are welded into place prior to pouring the floor of the concrete Photo - 9tank.

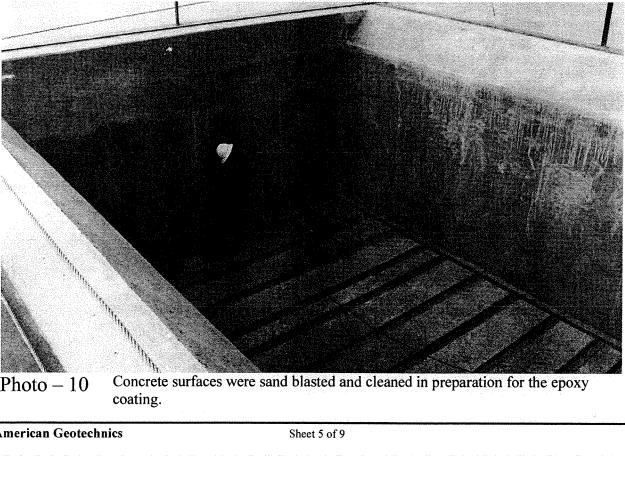


Photo - 10

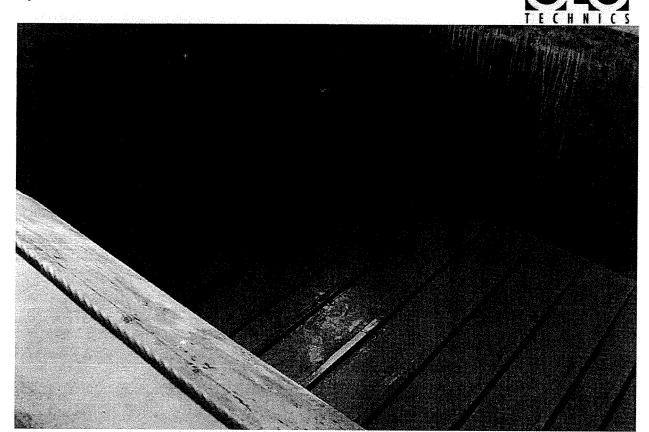


Photo - 11 Primer coat of epoxy is applied to the prepared concrete floor and walls.

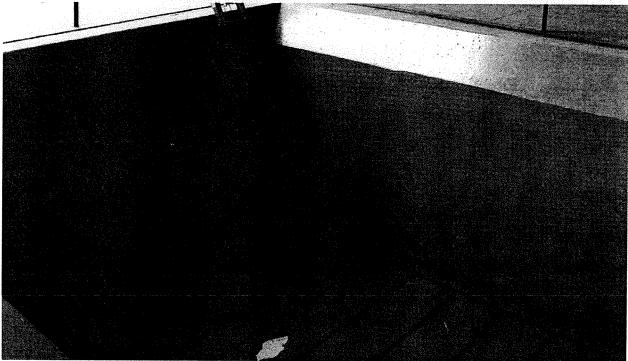


Photo - 12 Hydrostatic test is performed on the secondary containment; the control barrel is visible near the base of the ladder.



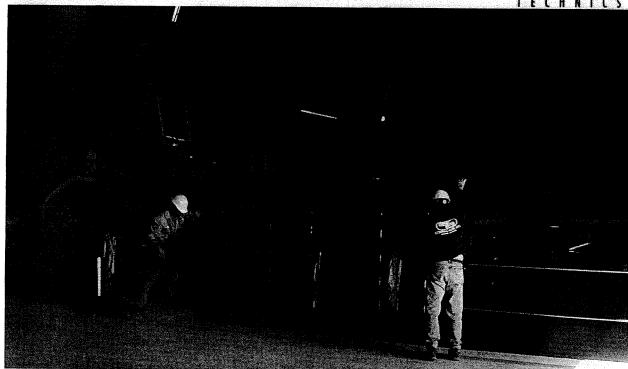


Photo-13 The steel vessels were constructed off-site in two halves and then transported to the site and lowered into position.



Photo -14 View of the steel vessel after placement of both halves into the mixing tank.



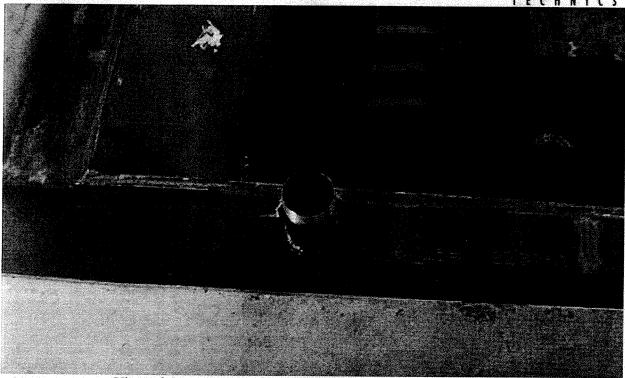


Photo-15 View of the 4-inch diameter access port that allows inspection of the secondary containment. Note the perimeter plates are not yet installed.

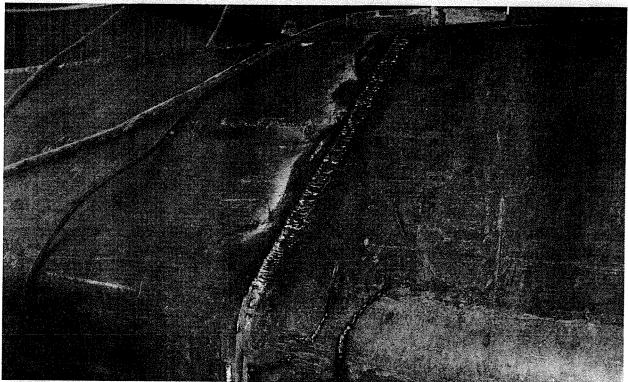


Photo – 16 The two halves of the steel vessel are joined along a common seam with multiple passes of welding rod.



Photo – 17 The steel mixing tanks were filled with water to test the integrity of the primary containment.

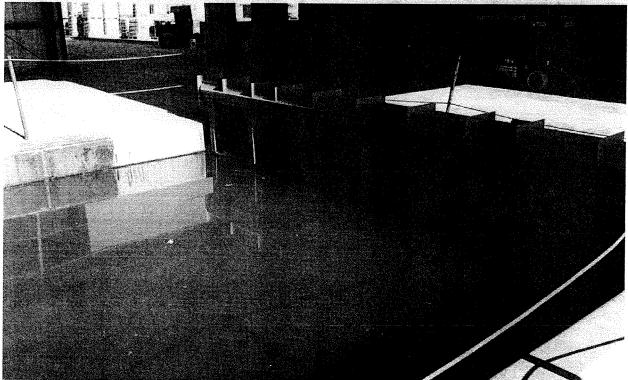


Photo-18 No leakage was observed into the secondary containment during the test period. A push jet manifold is visible on the far edge of the mixing tank.



APPENDIX C

HYDROSTATIC TEST REPORTS



March 23, 2007

Mr. Vaughn Thurgood, P.E. American Geotechnics 5260 Chinden Blvd. Boise, ID 83714

RE: US Ecology Nevada, Inc. - Stabilization Building Treatment Tank Containment Leak Testing

Mr. Thurgood;

This letter presents the results of the hydrostatic leak tests performed on the Stabilization Treatment Pan Secondary Containment Vaults located within the new Stabilization Building. The following test procedure was followed, as directed in your previous communications.

- The containment structures were cleaned and dried and allowed to stand for 24 hours.
- A second application of epoxy was installed and a 24 hour cure time was allowed.
- About 12 inches of water was placed in each of the containment structures.
- A thirteen inch tall drum (control drum) of known integrity was placed on the floor of the containment and filled to a
 level slightly above that of the water in the containment.
- Upon initialization of each test the water depth measurements were recorded from specific locations in the containment and control drum (See tables).
- Water levels were also measured after a 24 hour period or, in the case of the North Pan on March 21, when weather conditions permitted.

Date/Time	North Pan	Control Drum
3/19/07 16:30	12.0"	11 3/16"
3/20/07 16:30	*	11"
3/21/07 07:30	11 11/16"	10 7/8"
Delta @ 36 hours	5/16"	5/16"

Date/Time	South Pan	Control Drum
3/22/07 16:30	11 3/4"	11 5/8"
3/23/07 16:30	11 5/8"	11 1/2"
Delta @ 24 hours	1/8"	1/8"

^{*} Windy conditions inhibited accurate measurement.

Should you have questions regarding this information, please contact either myself (extension 104) or Mr. Mark John (extension 103) at 800-239-3943.

Sincerely,

Robert Marchand General Manager

Enclosure

cc: Mr. Mark John, Operations Manager - US Ecology Nevada

www.americanecology.com



May 4, 2007

Mr. Vaughn Thurgood, P.E. American Geotechnics 5260 Chinden Blvd. Boise, ID 83714

RE:

Stabilization Building Treatment Tank
Steel Vessel Primary Containment Leak Testing
US Ecology Nevada, Inc.

Mr. Thurgood;

This letter presents the results of the hydrostatic leak tests performed on the primary containment steel vessels associated with the treatment tanks located within the new Stabilization Building. The following test procedure was followed, as directed in your previous communications.

- Each treatment tank was filled to capacity with clean water.
- While the steel tanks were being filled with water, we noted that water spilled on the building floor was running into the void space between the top of the primary tank liner and the secondary containment. This gap will be closed when the epoxy coatings are applied to the building floor, fully isolating the building floor surface and the primary tank liner from the secondary containment. Upon initialization of each test, the depth of water within the secondary containment sump was observed and recorded.
- Water levels in each secondary containment sump were measured after a 24 hour period as follows.

Date/Time	North Pan Secondary Containment
4/30/07 14:00	5 1/8 "
5/1/07 14:00	5 1/8 "
Delta @ 24 hours	0"

Date/Time	South Pan Secondary Containment
5/3/07 08:00	2 7/8"
5/4/07 08:00	2 7/8"
Delta @ 24 hours	0"

Should you have questions regarding this information, please contact either myself (extension 104) or Mr. Mark John (extension 103) at 800-239-3943.

Sincerely,

Robert Marchand General Manager

Enclosure

201

Mr. Mark John, Operations Manager - US Ecology Nevada